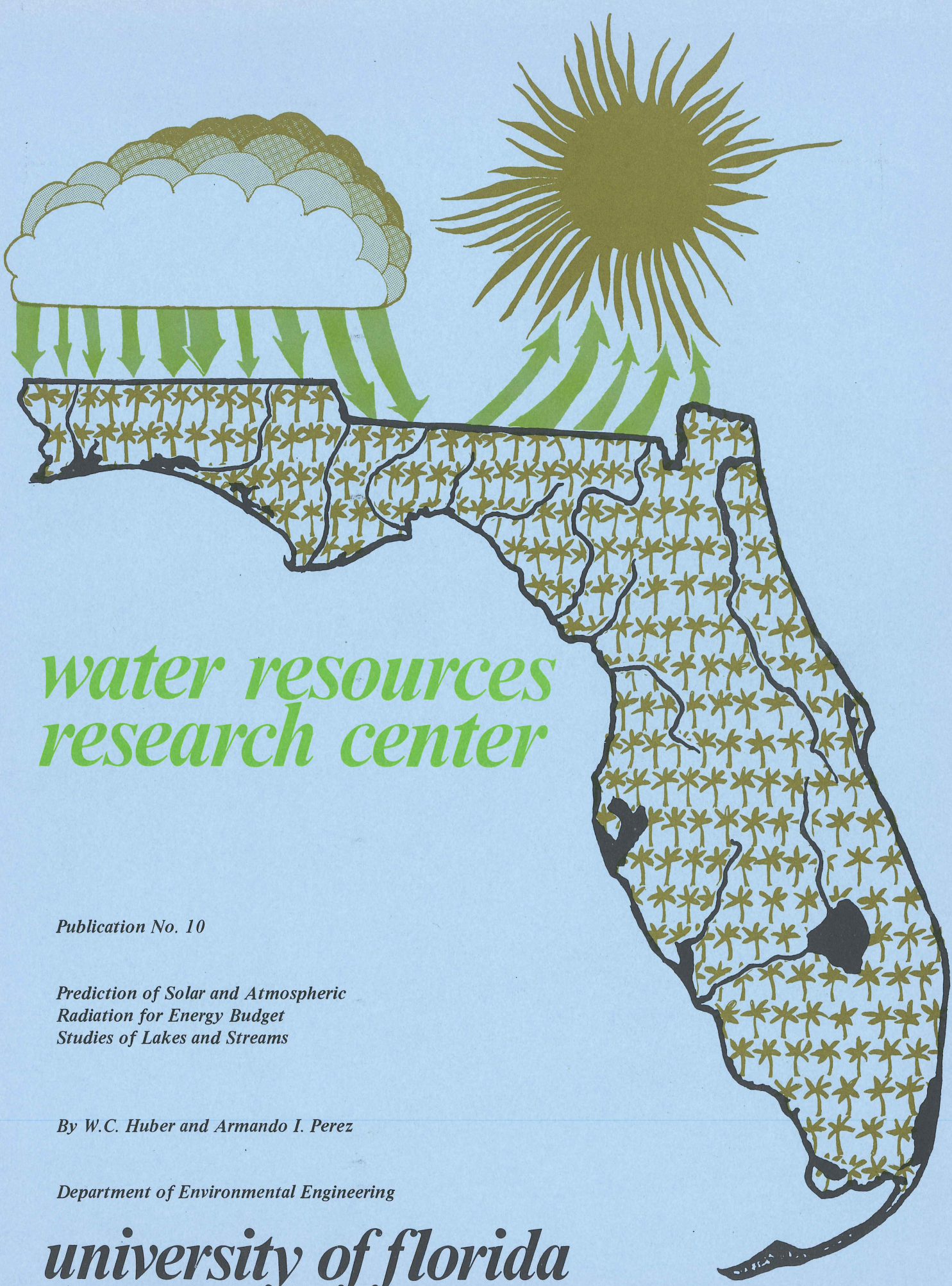

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Prediction of Solar and Atmospheric Radiation for Energy Budget Studies of Lakes and Streams

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FLORIDA WATER RESOURCES RESEARCH CENTER

Errata

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a. Appendix II: Listing of data. Shortwave measurements tabulated for day 105 are in error. The correct values should be one-half those tabulated.

b. It is important to note that all wave radiation measurements contain errors due to a defective radiometer. The longwave values derived from them should be used in subsequent analyses only with considerable caution.

ABSTRACT

PREDICTION OF SOLAR AND ATMOSPHERIC RADIATION FOR ENERGY BUDGET STUDIES OF LAKES AND STREAMS

Evaluation of terms in the energy budget is an integral part of the prediction of thermal changes in natural water bodies. These lakes, reservoirs, streams, and tidal waters receive heat from shortwave solar radiation, longwave atmospheric radiation, and advectively from surface water inflows. The net advective heat flux is often zero, in which case the radiation components are the dominant causes of temperature changes. Predictive methods for the two radiation components have been developed as a function of meteorological parameters alone, (e.g. temperature, humidity, cloudiness, opaqueness). These predictive methods can be used in areas where there are no records of radiation measurements since the required meteorological variables are commonly measured at weather stations and airports. A better predictive equation was found for shortwave radiation than for longwave radiation, due possibly to local climatic conditions and possible errors in portions of the longwave radiation measurements. Use of the shortwave equations in evaluating temporal temperature changes in a Florida lake resulted in good agreement with measured values. A tabulation of 148 days of hourly radiation and meteorological values is included in the report.

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1. INTRODUCTION

1.1 The Energy Budget

In the study of pollution problems in natural waters, knowledge of the temperature distribution is usually a prerequisite to a quantitative formulation of the pollutant distribution. In addition, the water temperature affects aquatic life and the stability of various chemical agents that may be found in the water. Finally, the water temperature plays an important role in the determination of the ability of a given water course to assimilate waste heat, from a thermal power plant for example. As a result, there has been considerable interest in predicting temperature distributions in rivers and estuaries (16, 17), lakes (7), reservoirs (8, 15), and the coastal environment (24).

All studies of temperature distributions must include an analysis of the sources and sinks of heat associated with the particular body of water. The systematic catalogue of these sources and sinks is called the energy budget. For a typical natural waterway, this can be expressed as:

$$\rho c_p \forall \frac{dT}{dt} = Q_s + Q_a + Q_v - Q_L \qquad (1\text{-}1)$$

where Q_s = net influx of short wave solar radiation (incident minus reflected),

Q_a = net influx of long wave atmospheric radiation,

Q_v = net energy advected into the water body (due to stream inflows, spillway outflows, etc.),

Q_L = net losses due to evaporation, conduction, and back radiation.

The term on the left hand side of equation 1-1 represents the change of energy stored in the body of water, where

T = average temperature,
t = time,
$\forall$ = volume of the water body,
c_p = specific heat,
ρ = density.

The units of the equation (and of the Q's) are energy/time, (e.g. cal/sec or Btu/hour).

Equation 1-1 may be used to compute the temporal variation of the average temperature of a water body (17). An example is shown in Appendix I. However, spatial variations of temperature within the water must be considered using a more sophisticated theory (8, 15).

1.2 Objectives

In a natural body of water, the net advective heat flux is commonly near zero, unless heat is added by a thermal power plant for instance. Consequently, the principle heating mechanisms are solar and atmospheric radiation, and mathematical models designed to predict temperature distributions must have these two quantities as input data. When the model is to be applied to a specific location, it is best to have a record of measured radiation values; however, these data are usually not available. Consequently, predicted values of the solar and atmospheric radiation fluxes must be used, and they are often subject to large errors. It is the objective of this report to develop methods for predicting incident solar and atmospheric radiation as a function of meteorologic variables that are commonly measured at weather stations throughout the country (e.g. temperature, humidity, cloudiness). In this manner, the energy budget equation may be used as a predictive tool for the determination of temperature distributions.

2. THEORETICAL BACKGROUND OF SOLAR AND ATMOSPHERIC RADIATION

2.1 Spectral Distribution

The source of 99.97% of all the energy used for climatologic and hydrologic processes is the sun, which radiates energy approximately as a black body, at a temperature of 6000°K. As a result of this high radiating temperature, 98% of the solar radiation received at the outer edge of the atmosphere lies between 0.25 and 3.0 μ*. The spectral distribution of this energy may be seen in Figure 2-1. The total short wave radiation incident upon the earth, (often called insolation), consists of the direct solar beam and diffuse radiation scattered from the sky.

The atmosphere and land mass of the earth radiate at a much lower temperature, approximately 287°K (14°C). As a result, the spectral distribution of this radiation is shifted as may also be seen in Figure 2-1. The atmosphere does not radiate as a black body, however, and the emissivity is a function of the meteorologic conditions.

*1 μ = 1 micron = 10^{-6} meters = 10^{4} Å

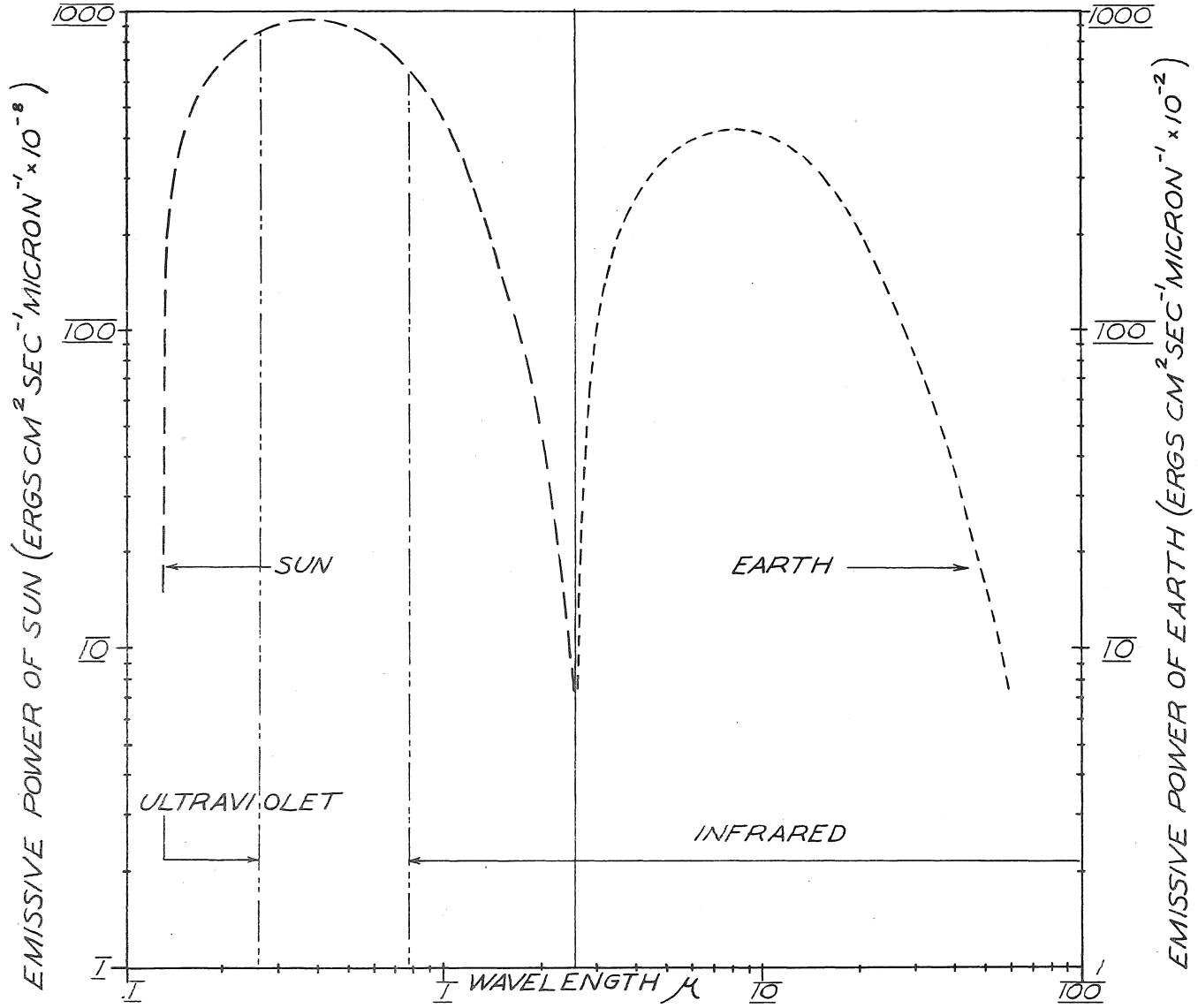

Figure 2-1. Spectral distributions of solar and atmospheric radiation (Note: change of scale of ordinates).

Due to the shortwave nature of the solar radiation, very little is absorbed by the atmosphere. However, the long wave radiation emitted by the earth is strongly absorbed by H_2O, CO_2 and O_3 in various wavelength bands (21). The atmospheric emissivity is consequently a function of the concentration of these quantities, since the absorbed terrestrial radiation is subsequently re-radiated.

2.2 Solar Radiation Received on a Horizontal Surface at the Top of the Atmosphere

The flux of solar radiation normal to the sun's rays received at the outer edge of the earth's atmosphere is known as the solar constant, I_{sc}. Although the solar constant is subject to some variation (20), it is commonly accepted to have the value

$$I_{sc} = 2.0 \text{ cal/cm}^2\text{-min} = 2.0 \text{ ly/min}^* \qquad (2\text{-}1)$$

at the mean distance of the earth from the sun. The intensity actually received will vary slightly with the square of the normalized earth-sun radius, r. The normalized radius, r, is the actual radius divided by the mean radius. Its variation may be found in meteorological tables (14) or given approximately as (25):

$$r = 1 + 0.017 \cos \left[\frac{2\pi}{365} (186\text{-}D)\right] \qquad (2\text{-}2)$$

where D is the number of the day of the year, (e.g. on February 1, D=32), and the extra day of leap years is ignored. The flux of radiation normal to the sun's rays, I_{sc_n}, is then

$$I_{sc_n} = \frac{I_{sc}}{r^2} \quad . \qquad (2\text{-}3)$$

The flux on a horizontal surface at the edge of the atmosphere is given by

$$I_o = I_{sc_n} \sin \alpha = \frac{I_{sc}}{r^2} \sin \alpha \qquad (2\text{-}4)$$

where α is known as the solar altitude and is the angle between the sun's rays and the plane tangent to the earth's surface at the point of observation. This is illustrated in Figure 2-2. The complement of α is known as the zenith angle, Z, and is the angle made between the sun's rays and the local vertical. The solar altitude can be determined from

*1 langley = 1 ly=1 cal/cm^2

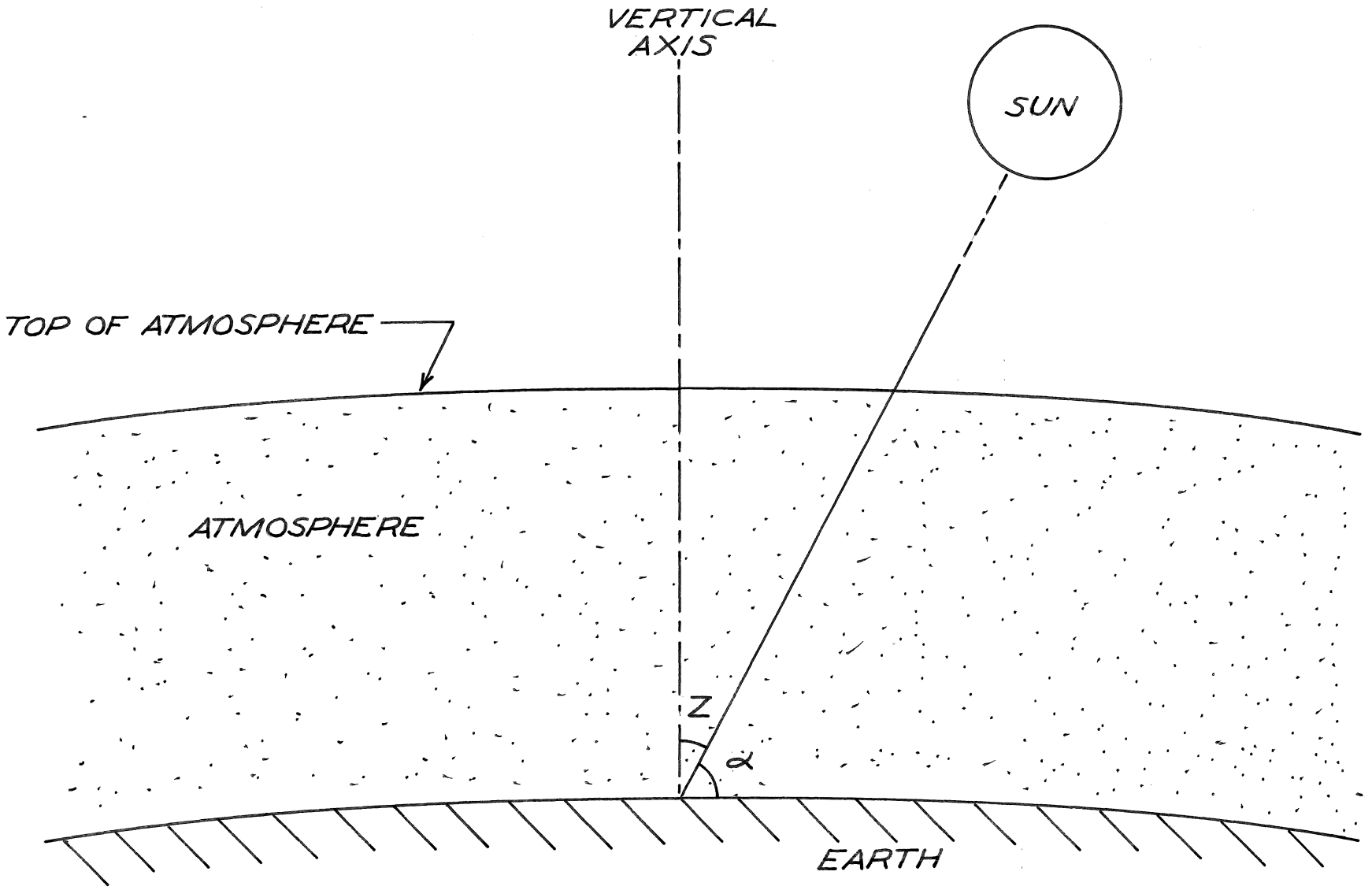

Figure 2-2. Illustration of solar altitude and zenith angle.

considerations of spherical trigonometry (21) and is given by

$$\sin \alpha = \sin \delta \sin \phi + \cos \delta \cos \phi \cos h \qquad (2\text{-}5)$$

where δ = declination of the earth,
ϕ = latitude of observer,
h = sun's hour angle.

The declination, δ, varies seasonally and may be found in meteorological tables (14) or given approximately as (25):

$$\delta = 23.45 \frac{\pi}{180} \cos \left[\frac{2\pi}{365} (172\text{-}D) \right] \qquad (2\text{-}6)$$

where δ is in radians, and D is the number of the day of the year defined in the same manner as for equation 2-2.

The hour angle of the sun is the angular distance measured westward around the axis of the earth between the meridian of the observer and the meridian of the sun. At true solar noon (when the solar altitude is at a maximum for that day), h=0. In the mornings, h is negative and in the afternoons h is positive. The value of h depends on three factors: (1) the local standard time (zone time); (2) the distance between the meridian of the observer and the standard meridian for that time zone; and (3) the variations in the length of a day due to seasonal variations in the orbital velocity of the earth. The third factor is accounted for by the so-called "equation of time" which gives the difference between "true solar time" and that computed on the basis of a yearly average.

Table 2-1 gives values of the equation of time taken from a more complete table given by List (14).

To compute h, the true solar time, t_s, is first computed thusly:

a. To the local standard time (zone time) add four minutes for each degree of longitude the point of observation is east of the standard meridian or subtract four minutes for each degree west of the standard meridian to get the local mean solar time.

b. To the local mean solar time add algebraically the equation of time obtained from Table 2-1 to obtain the true solar time.

TABLE 2-1

THE EQUATION OF TIME (After List)

Date		Equation of Time (min - sec)		Date		Equation of Time (min - sec)	
Jan.	1	-3	14	July	1	-3	31
	9	-6	50		9	-4	56
	17	-9	54		17	-5	57
	25	-12	14		25	-6	24
Feb.	1	-13	34	Aug.	1	-6	17
	9	-14	17		9	-5	33
	17	-14	10		17	-4	12
	25	-13	19		25	-2	18
Mar.	1	-12	38	Sept.	1	-0	15
	9	-10	51		9	+2	22
	17	-8	42		17	+5	10
	25	-6	20		25	+8	00
Apr.	1	-4	12	Oct.	1	+10	01
	9	-1	52		9	+12	27
	17	+0	13		17	+14	25
	25	+1	53		25	+15	46
May	1	+2	50	Nov.	1	+16	21
	9	+3	35		9	+16	12
	17	+3	44		17	+15	10
	25	+3	16		25	+13	15
June	1	+2	27	Dec.	1	+11	16
	9	+1	06		9	+8	01
	17	-0	33		17	+4	17
	25	-2	17		25	+0	20

For example on March 1 at a point at 80°W longitude in the eastern time zone, the true solar time at 11:00 A.M. Eastern Standard Time is

$$t_s = 11{:}00 - (80° - 75°) \times 4 \frac{\text{minutes}}{\text{degree}} - 12 \text{ min } 38 \text{ sec}$$

$$= 10{:}27{:}22 \text{ A.M.} \qquad (2\text{-}7)$$

The hour angle is then given in radians as

$$h = \frac{\pi}{12} (t_s - 12) \qquad (2\text{-}8)$$

with t_s in hours.

2.3 Effect of the Atmosphere on Clear-Sky Solar Radiation

The solar radiation received at the edge of the atmosphere I_o, is attenuated as it passes through the atmosphere by scattering and absorption. The extinction of the solar beam through scattering by air molecules can be described by Rayleigh scattering, whereas for larger particles, a more complicated theory results (20). In all cases, the scattering is dependent upon wavelength, and can be described for monochromatic radiation as:

$$I(\lambda)_s = I_o(\lambda)\ e^{-\sigma(\lambda)m} \qquad (2\text{-}9)$$

where $I(\lambda)_s$ = intensity of the monochromatic solar beam after scattering,
$I_o(\lambda)$ = intensity of radiation at edge of atmosphere of wavelength λ,
$\sigma(\lambda)$ = scattering coefficient at wavelength λ,
m = relative path length through the atmosphere, called the "optical air mass."

The optical air mass is the ratio of the path length of the solar rays at a given solar altitude to the path length through the zenith angle. It can be seen from Figure 2-1 that m is given approximately by:

$$m = \csc \alpha \qquad (2\text{-}10)$$

for angles greater than 10°. At a solar altitude less than 10°, refraction of the rays by the atmosphere creates a maximum value of m of about 36 at $\alpha = 0$. The variation of the optical air mass with solar altitude has been given as (9):

$$m = \frac{1}{\sin \alpha + 0.15\ (\alpha+3.885)^{-1.253}} \qquad (2\text{-}11)$$

with α in degrees. This must be modified for the local barometric pressure since m decreases at high altitudes. This can be done using the barometric formula (14):

$$m(z) = m(z=0)\ \frac{p}{p_o} = m(z=0)\ \left(\frac{288 - 0.0065\ z}{288}\right)^{5.256} \qquad (2\text{-}12)$$

where z is the elevation above sea level in meters, p is the local barometric pressure, p_o is the sea level barometric pressure, and m at sea level (z=0) is given by equation 2-11.

Absorption of the solar beam may be described in a form similar to equation 2-9:

$$I(\lambda)_a = I_o(\lambda)\ e^{-\Gamma(\lambda)\ m} \qquad (2\text{-}13)$$

where $I(\lambda)_a$ = intensity of monochromatic solar beam after absorption,

$I_o(\lambda)$ = intensity of radiation at edge of atmosphere of wavelength λ,

$\Gamma(\lambda)$ = absorption coefficient at wavelength λ,

m = optical air mass.

The direct solar radiation received at the ground includes all wavelengths, and is the result of both absorption and scattering by air molecules and particles of vapor and dust. The total intensity of the attenuated direct solar beam is then

$$I = \int_o^\infty I_o(\lambda)\ e^{-[\sigma(\lambda) + \Gamma(\lambda)]m}\ d\lambda. \qquad (2\text{-}14)$$

This equation may be used to define an average transmission coefficient, a, such that

$$I = I_o a^m = a^m \int_0^\infty I_o(\lambda)\, d\lambda. \qquad (2\text{-}15)$$

The intensity at the outer edge of the atmosphere, I_o, is given by equation 2-4. The transmission coefficient will be a function of the turbidity of the atmosphere as indicated by moisture and dust content. However, because of the fact that the extinction coefficients, $\sigma(\lambda)$ and $\Gamma(\lambda)$ are functions of wavelength, the value of a will vary with the optical air mass, m, even if the turbidity of the atmosphere does not change (20). Consequently, if values of a are computed from measured radiation at the ground surface, I,

$$a = a(m) = \left(\frac{I}{I_o}\right)^{\frac{1}{m}} \qquad (2\text{-}16)$$

then a will not be a constant over the day, but rather decrease with decreasing air mass, m. This has been borne out by experiments as will be shown in Chapter 4.

One method of accounting for this variation with air mass is to determine the variation in transmission coefficient if it were due to scattering alone (20). This transmission coefficient, $a_s(m)$, will vary with m and can be found from a numerical integration of

$$I_o\, a_s(m)^m = \int_0^\infty I_o(\lambda)\; e^{-\sigma(\lambda)m}\, d\lambda \qquad (2\text{-}17)$$

since the functional relationship of $\sigma(\lambda)$ is known for Rayleigh scattering. Knowing $a_s(m)$, a turbidity factor, T, is defined by

$$I(m) = I_o a_s(m)^{mT} \qquad (2\text{-}18)$$

where it is hoped that the variation with air mass will be mostly accounted for in $a_s(m)$ and not appear in T. It is then possible to solve for the turbidity factor,

$$T = \frac{1}{-m\log_{10} a_s(m)}\; \log_{10}\frac{I}{I(m)} = \frac{1}{P(m)}\log_{10}\frac{I_o}{I(m)} \qquad (2\text{-}19)$$

where

$$P(m) \equiv -\frac{1}{m\log_{10} a_s(m)}\,. \qquad (2\text{-}20)$$

The parameter P(m) has been tabulated (20) and can be approximated by the polynomial relationship

$$P(m) = 23.0\ m^{-.783} \ . \qquad (2\text{-}21)$$

Unfortunately, values of the turbidity factor found from equation 2-19 still exhibit some variation with m because scattering and absorption from vapor and dust are also wavelength dependent. Analysis of data using the turbidity factor is shown in Chapter 4.

The preceding discussion has dealt with atmospheric effects on the direct solar beam. However, the total or global short wave radiation as measured by a pyranometer will include the diffuse radiation contributed by the sky as a result of scattering and reflection from the earth's surface. These effects may be treated separately in the manner of Klein (11) who determined separate transmission coefficients for scattering and absorption and totaled the various scattered and reflected components into one general equation with several parameters. A method in which his approach is used is shown by Wunderlich (25).

However, since the scattered and reflected radiation is attenuated in a similar manner to the direct solar beam, and since the radiation received at the edge of the atmosphere is the primary source of all global radiation components, a simpler method due to Kennedy (10) is to lump all effects into one atmospheric transmission coefficient, a_t. This parameter is defined in the manner of equation 2-15:

$$I = I_o a_t^m \qquad (2\text{-}22)$$

where it is expected from prior discussions that a_t will vary with m. However, for a given range of air mass, a_t will be expected to vary with parameters describing the moisture and dust content of the atmosphere. Data are analyzed in this manner in Chapter 4.

2.4 The Effect of Clouds on Solar Radiation

It is obvious that solar radiation is diminished by clouds; however, the quantification of this effect is one of the most difficult to determine. Most investigations have concluded that it is better to modify the clear sky radiation by a function of cloudiness than to include the functional relationship directly in the transmission coefficient.

Weather stations commonly measure cloudiness, C, as a fraction of the sky covered on an hourly basis (5). In addition, some determine the relative duration of sunshine, S, which is the ratio of net duration of sunshine to total possible duration of sunshine (length of day). The value of S is determined on a minimum of a daily basis. The relationship between C and S is nominally

$$S = 1-C \quad . \tag{2-23}$$

However, on the basis of a regression analysis, Wunderlich (25) suggests that

$$S = 1-C^{5/3} \tag{2-24}$$

is a better fit. In equations 2-23 and 2-24, the value of C is an average over the same time scale as S.

The functional relationship usually suggested between cloudiness and net radiation is

$$I = I_o a_t^m \quad (1-c_1 C^{c}2) \quad . \tag{2-25}$$

A parabolic relationship proposed by Wunderlich (25) has

$$c_1 = 0.65 \text{ and } c_2 = 2 \quad . \tag{2-26}$$

The values of the constants, c_1 and c_2 are considered in Chapter 4.

In addition to measurements of the fraction of sky covered by clouds, weather stations also measure opaqueness, O, which is the fraction of sky covered by clouds through which there is no visibility. In general then, $O \leq C$. The possibility of a relationship of the type given by equation 2-25 using opaqueness instead of cloudiness is also examined in a later chapter.

Other parameters that influence the amount of radiation received are cloud elevation, thickness and type. Although these parameters are measured at some weather stations, the measurements frequently require equipment that is not always available, such as balloons, ceiling lights, or radar (5). On the other hand, cloudiness and opaqueness may be estimated by ground observers with no special equipment. Since it is intended that the parameters included in the predictive methods developed in this report be readily available, the influence of clouds will be studied using only cloudiness and opaqueness.

2.5 Longwave Atmospheric Radiation from Clear Skies

The atmosphere does not radiate strictly as a black body or gray body because of the wavelength dependence of the radiation absorbed and emitted by the water vapor, H_2O, carbon dioxide, CO_2, and ozone, O_3. However, most investigations assume that the atmospheric radiation can be represented by a blackbody type relationship,

$$I_a = \varepsilon \sigma T^4 \qquad (2\text{-}27)$$

in which ε is the atmospheric emissivity and will be a function of the concentration of H_2O, CO_2, and O_3 and, perhaps, other meteorologic parameters. The absolute air temperature, T, is measured at a specified distance above the ground, and σ is the Stefan-Boltzman constant with a value

$$\sigma = 8.26 \times 10^{-11} \text{ cal/cm}^2\text{-min-}^{\circ}\text{K}^4$$

or $$\sigma = 1.713 \times 10^{-9} \text{ Btu/ft}^2\text{-hr-}^{\circ}\text{R}^4 \; . \qquad (2\text{-}28)$$

When measurements of air temperature and longwave radiation are made at a site, the value of ε can be determined and related to other meteorologic variables.

Several different relationships have been developed in the past. Examples, include a linear relationship with vapor pressure, e (1):

$$\varepsilon = a_o + b_o e \qquad (2\text{-}29)$$

or a square root relationship (6):

$$\varepsilon = a_o + b_o \sqrt{e} \qquad (2\text{-}30)$$

or an exponential relationship (3):

$$\varepsilon = a_o + b_o \exp (c_o e) \qquad (2\text{-}31)$$

or a dependence upon absolute air temperature (22):

$$\varepsilon = a_o T^2 \; . \qquad (2\text{-}32)$$

In general, the constants found for a given emissivity equation vary in different investigations because of changes in local climatic and experimental conditions. In this investigation, the constants might also be expected to be peculiar to the particular area; however, light may be shed upon the best functional form to use for the prediction of ε.

2.6 The Effect of Clouds on Longwave, Atmospheric Radiation

Atmospheric radiation is increased by the presence of clouds (because of the high concentration of emitting water particles), and is a function of the cloud amount, height, thickness, and type. In accordance with the preceding discussion of the effect of clouds on solar radiation, the effect of cloudiness, C, (and perhaps opaqueness, O), will be the only parameters considered because of their ease of measurement.

When clouds are present, the predicted clear sky atmospheric radiation may be multiplied by a function of cloudiness, C. Wunderlich (25) suggests

$$I_a = \varepsilon T^4 (1 + 0.17 C^2) . \qquad (2\text{-}33)$$

The type of functional relationship and constants will be considered in this investigation.

2.7 Summary

In this chapter, the broad theoretical basis for predicting solar and atmospheric radiation has been presented. It has been seen that many of the relationships are empirical in nature, although based upon physical laws. In the following chapters, these relationships will be examined in the light of experimental data.

Emphasis will be upon the functional type relationships just described rather than the graphical presentations of some investigators (2,23). This is because of the need for the relationships to be readily programable on digital computers, and also because many graphical presentations require parameters not readily available, (e.g. cloud thickness and type).

3. METHODS OF DATA COLLECTION

3.1 Shortwave Radiation

Instruments to measure radiation from the direct solar beam, either over all wavelengths or selectively, are called pyrheliometers. Instruments that measure the global (total direct and diffuse) radiation incident upon a horizontal surface are called pyranometers. An excellent discussion of these instruments may be found in Robinson (20) and Sellers (21).

An Eppley Model 8-48, black and white pyranometer, serial number 10,000, was used for the short wave radiation measurements of this study. It was not possible to check its factory calibration of 7.71 mv-min/ly. The instrument was mounted atop the roof of A. P. Black Hall (Environmental Engineering Building) on the University of Florida campus at Gainesville, (latitude 29° 37' N, longitude 82° 20' W). The approximate elevation of the instrument was 145 feet, M.S.L. This is approximately 67 feet above the sloping ground level at that point. The roof of the building presents a generally unobstructed view, except for a nearby instrument tower which cast a shadow for a few minutes once a day. This had a negligible effect on the readings.

The output of the pyranometer was fed into a Model 28, Servo Graphic Recorder, (Yeiser Laboratories, Costa Mesa, California 92627), serial number 800. The calibration of this millivolt strip-chart recorder was checked periodically using a standard voltage source belonging to the Environmental Engineering Department. The chart speed was set at 1 in/hr. The data were reduced manually from the strip-chart records.

3.2 Longwave Radiation

Total incoming radiation measurements were made with a thermal radiometer, model number TCH 188-01, serial number 1015, manufactured by Packard Bell. It is a ventilated radiometer of the Gier and Dunkle type and measures the total shortwave and longwave incoming radiation. Longwave radiation values are obtained by subtracting the shortwave values obtained simultaneously with the pyranometer. It was not possible to check the factory calibration of this instrument of 0.5512 ly/min-mv.

The radiometer was mounted near the pyranometer atop A. P. Black Hall at the University of Florida. Its output was fed into another Model 28 Servo Graphic Recorder, Serial Number 735, and data were again reduced by hand from the strip-chart records.

3.3 Meteorological Parameters

The meteorological variables of primary concern were air temperature, relative humidity, and cloudiness conditions. The first two variables were measured with a Kahlsico temperature and relative humidity recorder manufactured by the Kahl Scientific Instrument Corporation, El Cajon, California. The recorder was mounted in a standard meteorological instrument housing five feet above ground level near the north side of A. P. Black Hall, about 55 feet below the pyranometer and radiometer. A comparison of temperature and humidity measurements from this recorder with similar measurements made atop the roof showed negligible differences. The strip-chart records were reduced by hand to produce values of temperature and relative humidity at times corresponding to the radiation measurements.

Measurements of cloudiness and opaqueness were obtained from surface weather observations made at the Gainesville Airport, 6.1 miles northeast of A. P. Black Hall. Because of the fact that hourly readings were necessary on a 24 hour basis, it was not possible to make these measurements at the same site as the radiation measurements. When averaged on an hourly basis, it was expected that there would be no difference between airport and campus readings. Cloudiness and opaqueness are both measured as tenths of the sky covered; (e.g. C=10 indicates total overcast).

In addition to measurements of cloudiness at the airport, measurements of sunshine duration were made for a few weeks with a Campbell-Stokes type sunshine recorder, (Casella and Co., Ltd., London), Serial Number 7554-MK 111.B, mounted near the pyranometer and radiometer atop A. P. Black Hall. This instrument records the presence of direct sunshine from a trace burned on a specially labeled card by a spherical glass ball. These measurements were discontinued because the cloudiness measurements are standard, whereas sunshine recorders of this type are not. In addition, the trace burned on the card is often more difficult to interpret than are the cloudiness records.

It was not possible to make quantitative determinations of the dust content of the atmosphere. However, the climatic conditions of Gainesville are relatively clear and dust free because of the lack of industry in the area, and because the humid, forested area is not conducive to dust being erroded from the ground. Consequently, the lack of data on dust content should not adversely affect the analysis of data from this site.

3.4 Data Reduction

Hourly averages were used as the basis of analysis of all data. Data read from strip-charts were averaged by eye as the records were analyzed. Solar radiation values were frequently highly fluctuating as scattered clouds passed overhead. Although the hourly averages were determined carefully, integrated values would have been more accurate. Unfortunately, an integrating voltmeter was not available, and integration by planimeter was not feasible.

All reduced data were punched on cards for computerized analysis. A list of all data gathered and used in the analysis is given in Appendix II, along with corresponding parameters such as solar altitude and optical air mass that were derived from equations presented in Chapter 2.

4. ANALYSIS OF DATA

4.1 Introduction

The data gathered as described in Chapter 3 were analyzed in accordance with the developments of Chapter 2. The objective has been to use the data to develop predictive relationships for both shortwave and longwave radiation. Due to considerable delays in obtaining some of the equipment, only 135 days of hourly data were used in the analysis, corresponding to the record from March 18, 1970 to July 31, 1970. Data for August, 1970 are included in Appendix II but were not gathered in time to be included in the analysis. Efforts were made to secure data from other geographical locations, but such data were not available on an hourly basis, and daily or weekly averages (4, 18) were deemed insufficient for much of the analysis.

In order to separate the effects of clouds, clear sky radiation data were analyzed separately. The resulting prediction equations were then used to determine the potential incident radiation on cloudy days so that cloudiness effects could be studied.

4.2 Clear Sky Shortwave Radiation

The primary factor in changing the atmospheric transmission coefficient, a_t, of equation 2-22 should be the amount of water vapor present in the atmosphere. This is in the absence of appreciable dust content, as discussed previously. The amount of water vapor in the atmosphere is indicated by the "depth of precipitable water vapor," w, which is an integration of the specific humidity, q_h, over given pressure intervals moving vertically through the atmosphere (13):

$$w = 0.004 \int_{p_1}^{p_o} q_h \, d_p \qquad (4\text{-}1)$$

where w = depth of precipitable water vapor in inches,
q_h = specific humidity, in grams/kilogram,
p_o, p_1 = total atmospheric pressure at the lower and upper bounds, respectively, in mb.

The number 0.004 is a conversion constant.

The specific humidity is the mass of water vapor per unit mass of moist air and is given by

$$q_h = 622 \frac{e}{p_a - 0.378e} \simeq \frac{622\ e}{p_a} \qquad (4\text{-}2)$$

where q_h has units of grams/kilogram, and e and p_a are the vapor pressure and total atmospheric pressure, respectively. The pressures, p_a and e must have identical units when used in equation 4-2.

The preceding equations indicate that the depth of precipitable water vapor should be proportional to vapor pressure, e. Empirical formulas have also related it to the dew point (19). If r_h is the relative humidity in percent, then

$$r_h = 100 \frac{e}{e_s} \qquad (4\text{-}3)$$

where e_s is the saturation vapor pressure and is a function of temperature. Values may be found in meteorological tables (14) or approximated by the parabolic relationship:

$$e_s = 0.0418\ T^2 - 0.6216T + 13.0068 \qquad (4\text{-}4)$$

for the temperature range $15 \leq T \leq 40$ with e_s in mm Hg and T in °C.

When e_s and r_h are known, e may be found from equation 4-3.

It was expected that the value of a_t would be proportional to e. Values of a_t were found for clear days by solving equation 2-22, thus:

$$a_t = \left(\frac{I}{I_o}\right)^{\frac{1}{m}} . \qquad (4\text{-}5)$$

However, when values of transmission coefficient are plotted versus vapor pressure in Figure 4-1 for all air masses, m, there is no discernable trend. The expected trend would be decreasing a_t for increasing e.

The scatter in Figure 4-1 is due in part to the effect of air mass discussed in Section 2.3. When the air mass changes, the transmission coefficient can be expected to change slightly because the scattering and absorption are functions of wavelength. This effect is shown in Figure 4-2 in which data shown in Figure 4-1 are segregated within certain air mass ranges. Even within a given range of air mass however, the trend is still toward a constant value of transmission coefficients over all vapor contents. Correlations with other parameters such as temperature or absolute humidity showed no better results. The only variable that significantly affected the values of a_t was the optical air mass, m. The correlation of a_t with m is good, as shown in Figure 4-3.

In an effort to eliminate the effect of air mass and include the effect of vapor content, the atmospheric turbidity factor, T, of Section 2.3 was introduced. Values of T were computed using equation 2-19 and plotted versus vapor pressure as shown in Figure 4-4. The correlation was no better, unfortunately.

The conclusion to be drawn from the data of Figures 4-1 to 4-4 is that atmospheric vapor content has a negligible effect on shortwave radiation at the locality of these measurements. Values of the atmospheric transmission coefficient may thus be predicted for the north-central Florida region from Figure 4-3 alone. Because of the fact that vapor content has no effect, these values must depend to some degree upon local climatic conditions, hence they probably should not be transposed to other geographical locations. The relationship shown in Figure 4-3 may be represented by

$$a_t = 0.74m^{0.0882} \quad . \qquad (4\text{-}6)$$

4.3 Cloudy Sky Shortwave Radiation

In order to evaluate the effect of clouds on transmission of shortwave radiation, a prediction of the clear sky radiation was first made using equation 2-22 and Figure 4-3. The ratio of measured cloudy sky radiation to predicted clear sky radiation was then plotted versus cloudiness and opaqueness as shown in Figures 4-5 and 4-6.

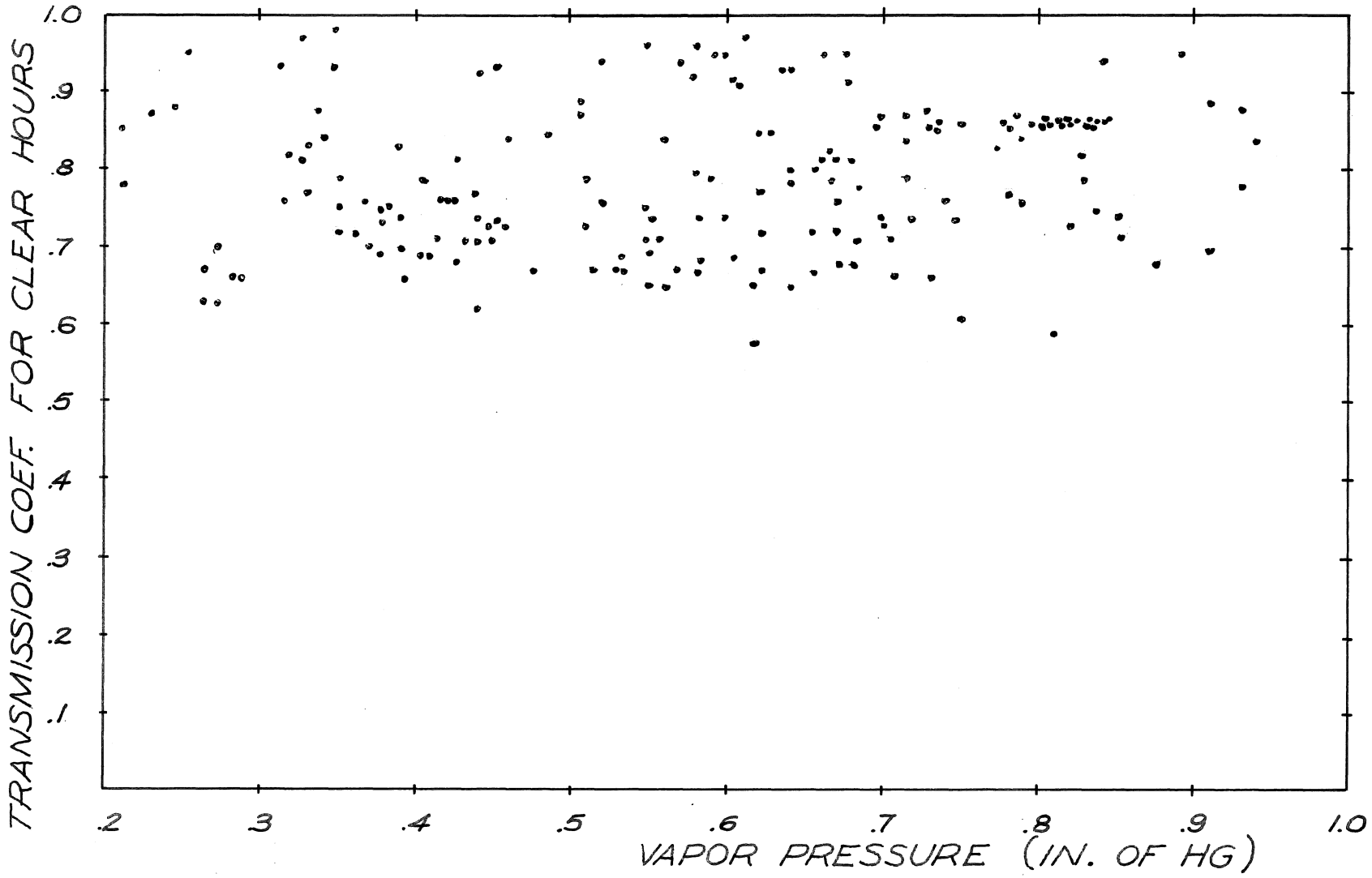

Figure 4-1. Clear sky atmospheric transmission coefficient as a function of vapor pressure.

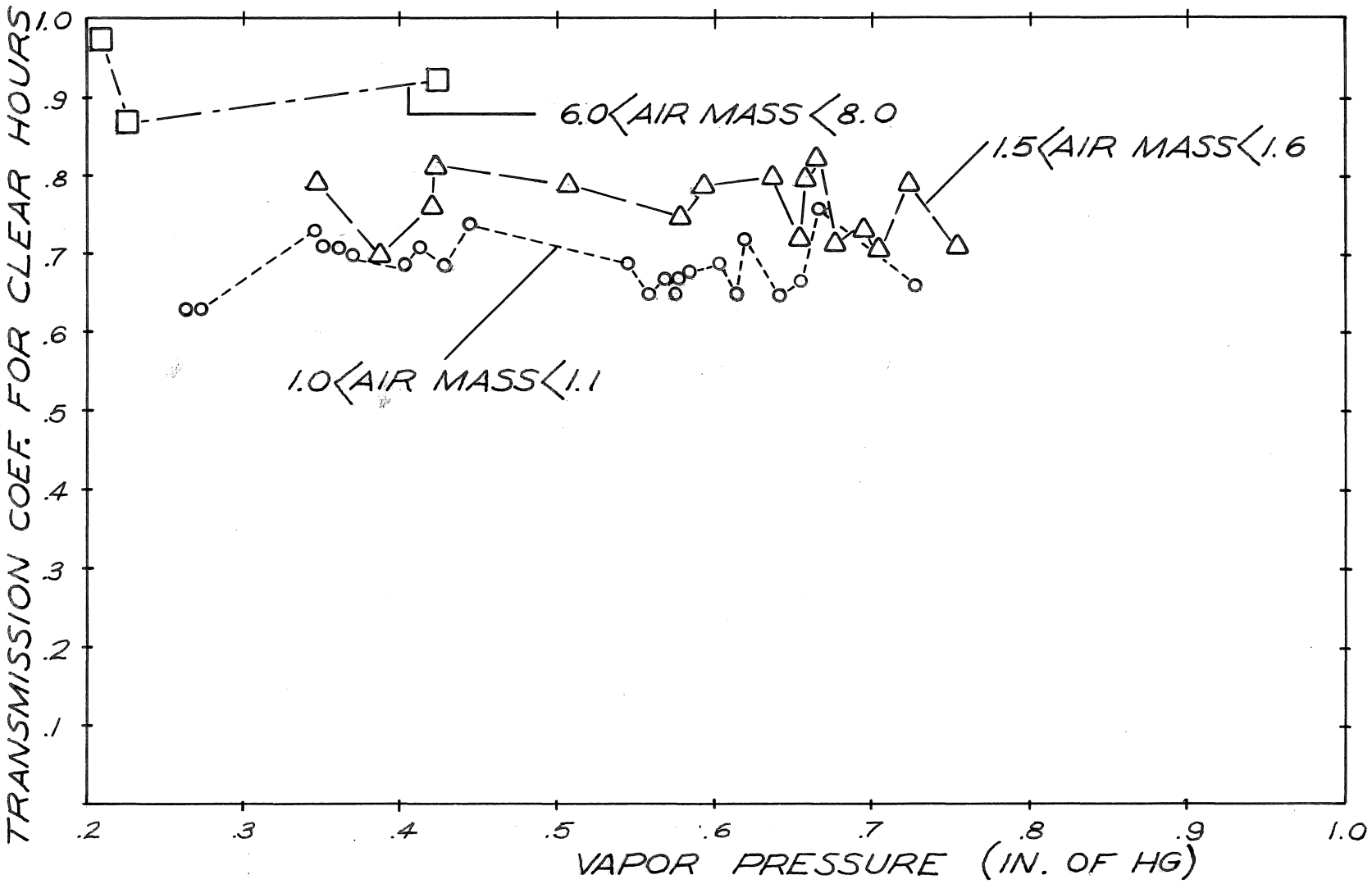

Figure 4-2. Effect of air mass on transmission coefficient - vapor pressure relationship.

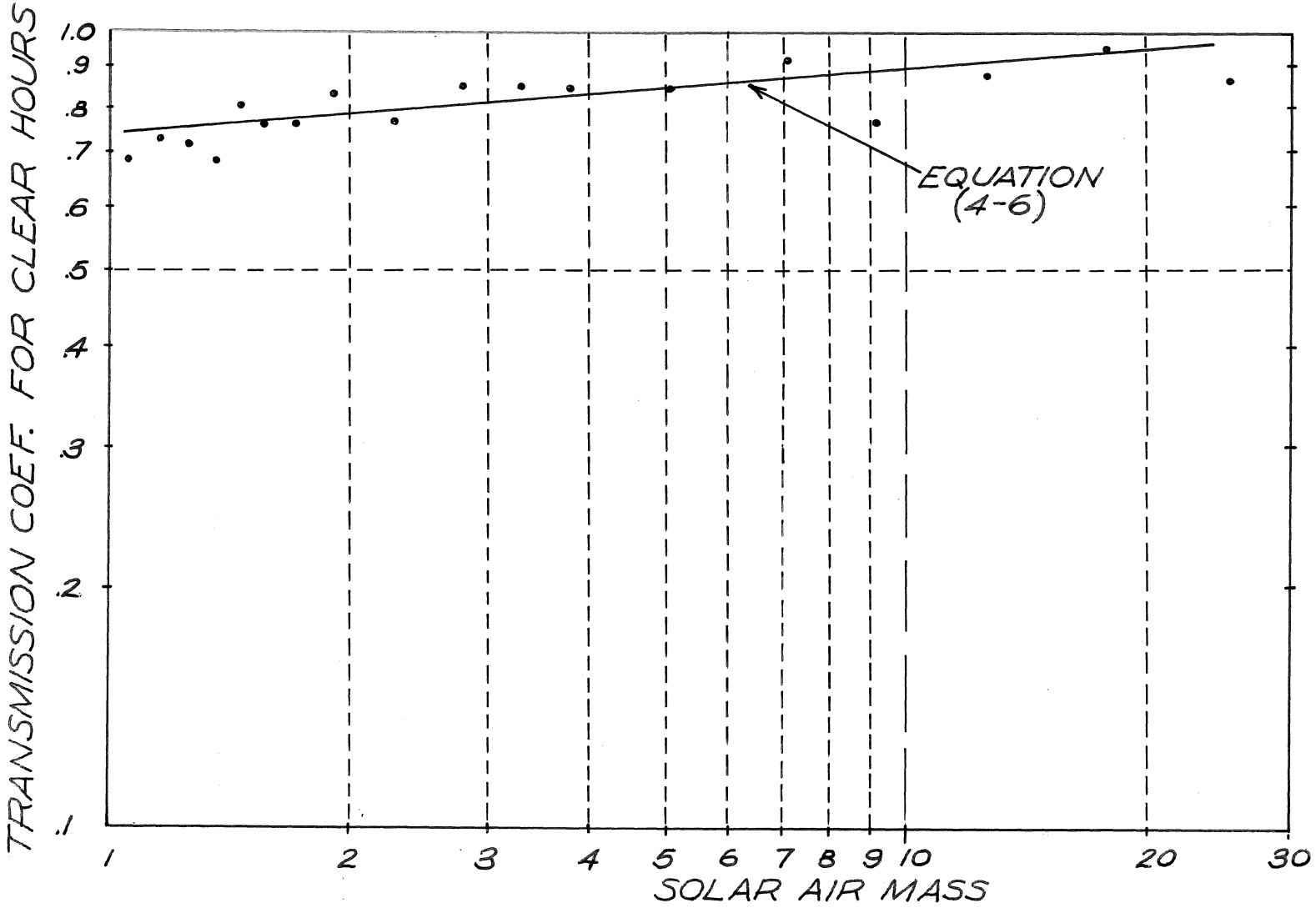

Figure 4-3. Atmospheric transmission coefficient as a function of optical air mass.

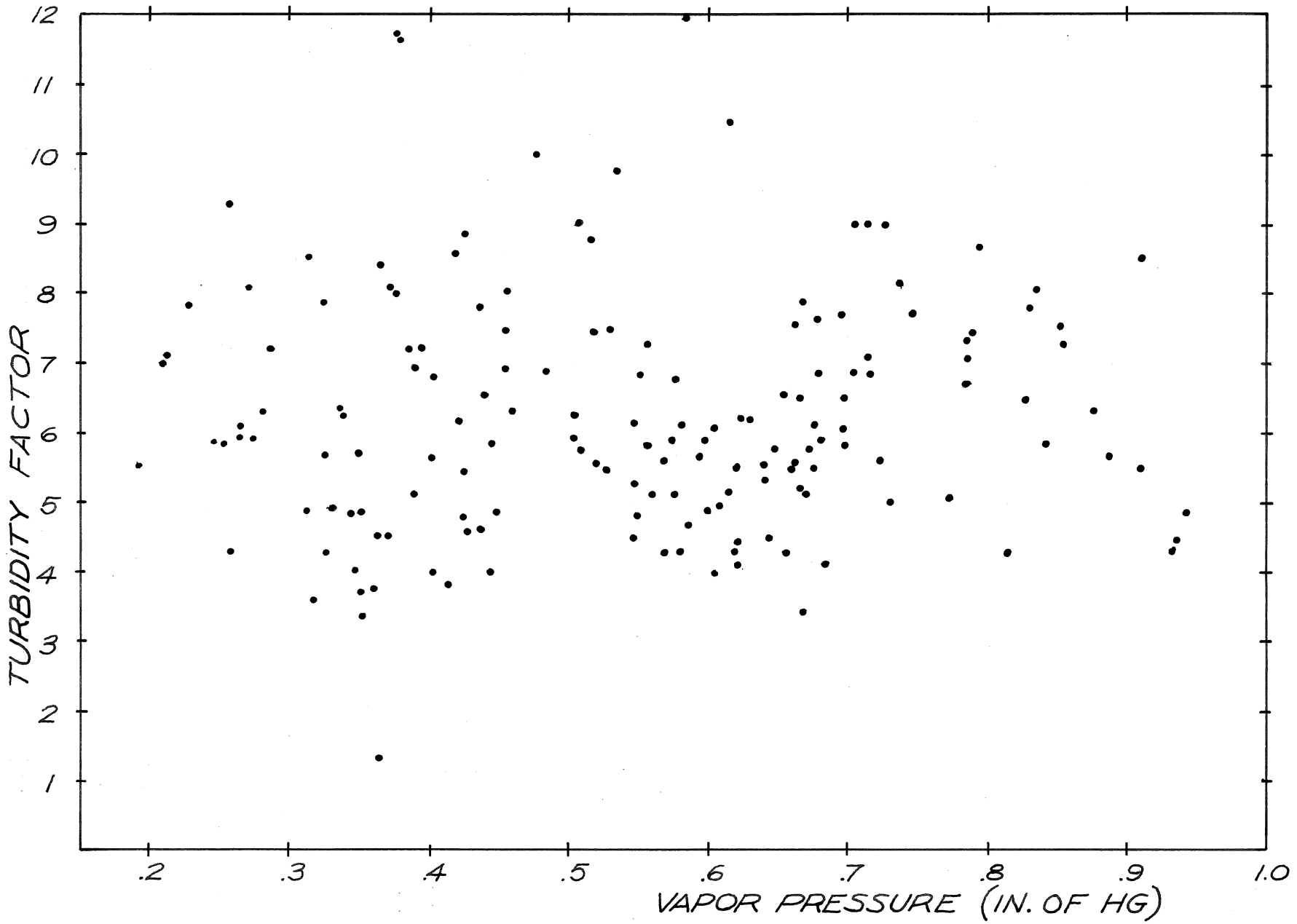

Figure 4-4. Turbidity factor as a function of vapor pressure.

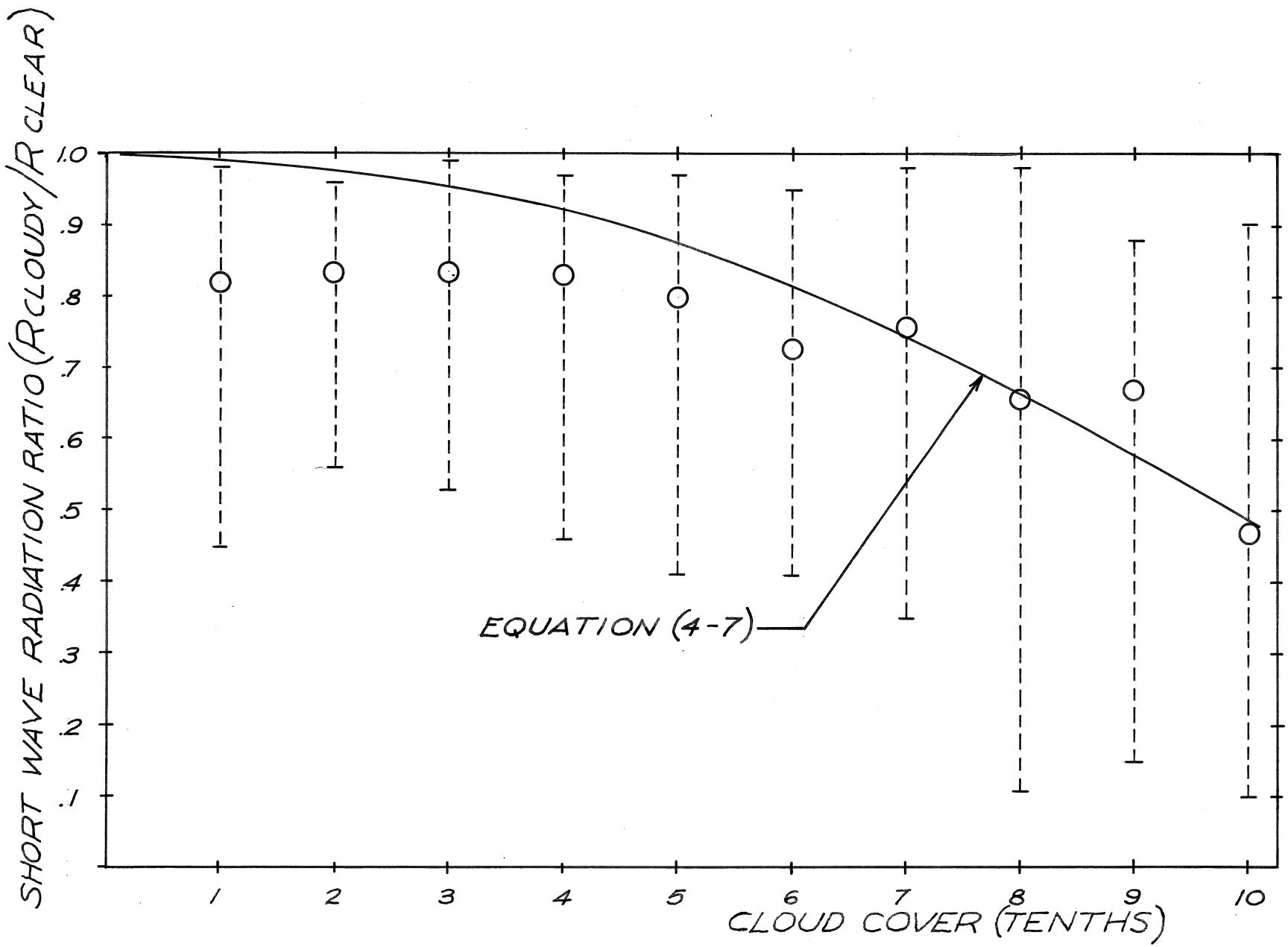

Figure 4-5. Effect of cloudiness on clear sky shortwave radiation. Circles are mean values over the range indicated by the dashed lines.

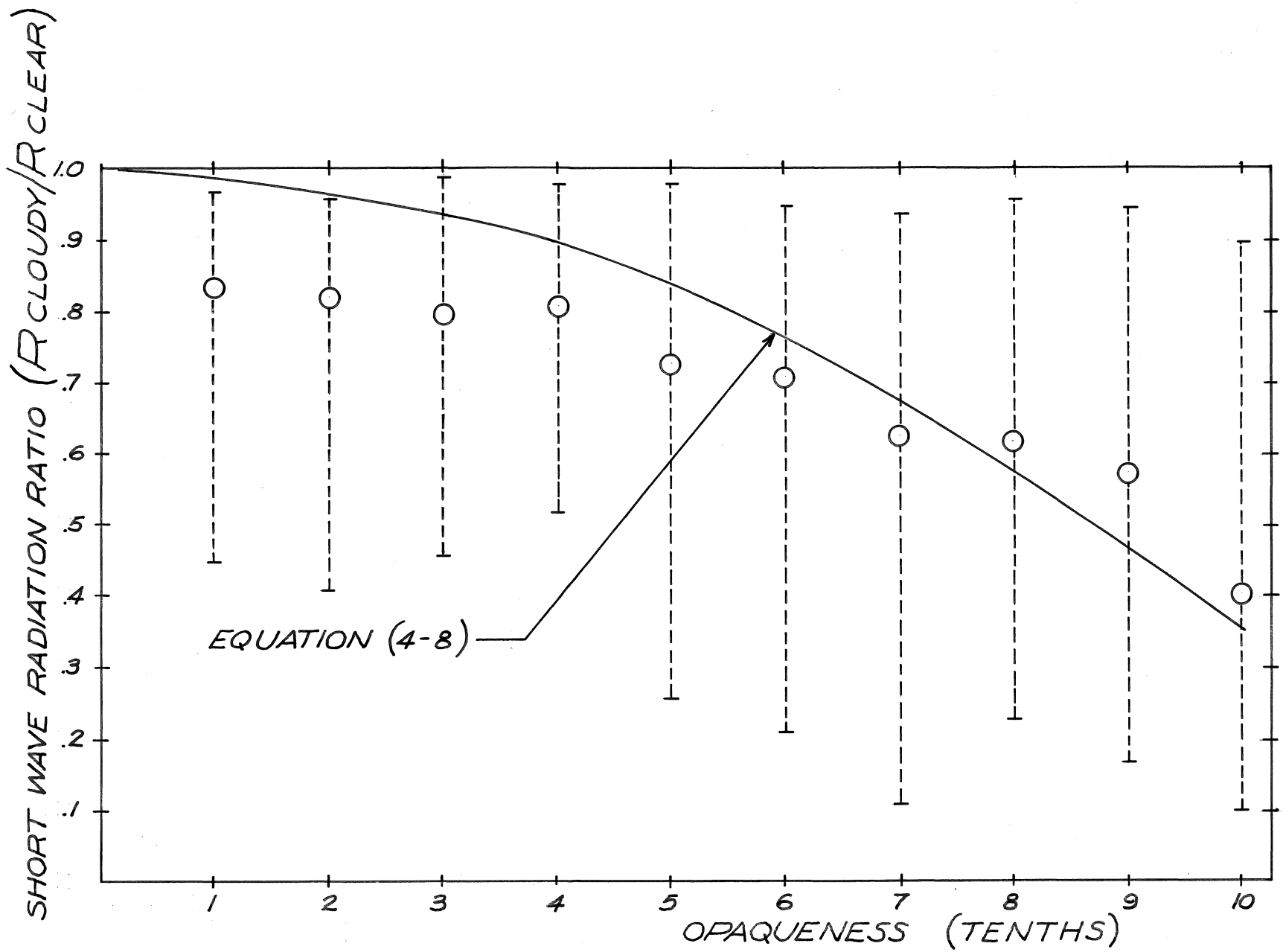

Figure 4-6. Effect of opaqueness on clear sky shortwave radiation. Circles are mean values over the range indicated by the dashed lines.

As discussed in Section 2.4, a parabolic relationship has been indicated by most investigations, and this is borne out by the figures. A least squares regression analysis of 554 data points indicates that the cloudy sky radiation may be represented by

$$I = I_o \, a_t^m \, (1-0.514 \, C^2) \qquad (4-7)$$

or

$$I = I_o \, a_t^m \, (1-0.638 \, O^2) \qquad (4-8)$$

with C and O given as the fraction of sky covered. The multiple correlation coefficient of the cloudiness relationship and opaqueness relationship is 0.87. However, equation 4-8 should probably be used at high cloudiness values because opaqueness is a more precise indication of the degree of transmission of solar radiation. Since equations 4-7 and 4-8 are forced to pass through the point(0,1), predicted radiation at low cloudiness and opaqueness values will be slightly high.

4.4 Clear Sky Longwave Radiation

From the known values of incoming longwave radiation and air temperature, clear sky atmospheric emissivities were calculated from equation 2-27. It was expected that the emissivities would exhibit a functional relationship with vapor pressure, as discussed in Section 2.5. However, considerable scatter is evident in the plot shown in Figure 4-7. The origin of this scatter is uncertain, however, the emissivity values calculated from night time measurements were generally the lowest on the plot. There should be no reason to isolate those values from the daytime readings since the atmosphere radiates in the same manner at all times. However, the percentage error in voltmeter readings is greater at night when the radiation values are small. Consequently, these values may be suspect. In light of the considerable scatter, a simple linear relationship between emissivity and vapor pressure was determined by a linear regression:

$$\varepsilon = 0.3313 + 0.531 \, e \qquad (4-9)$$

with e in in. Hg.

Additional data gathered at a future date may explain the origin of the excessive scatter that results in a rather inconclusive emissivity - vapor pressure relationship. The results of a correlation of emissivity with temperature were no more meaningful.

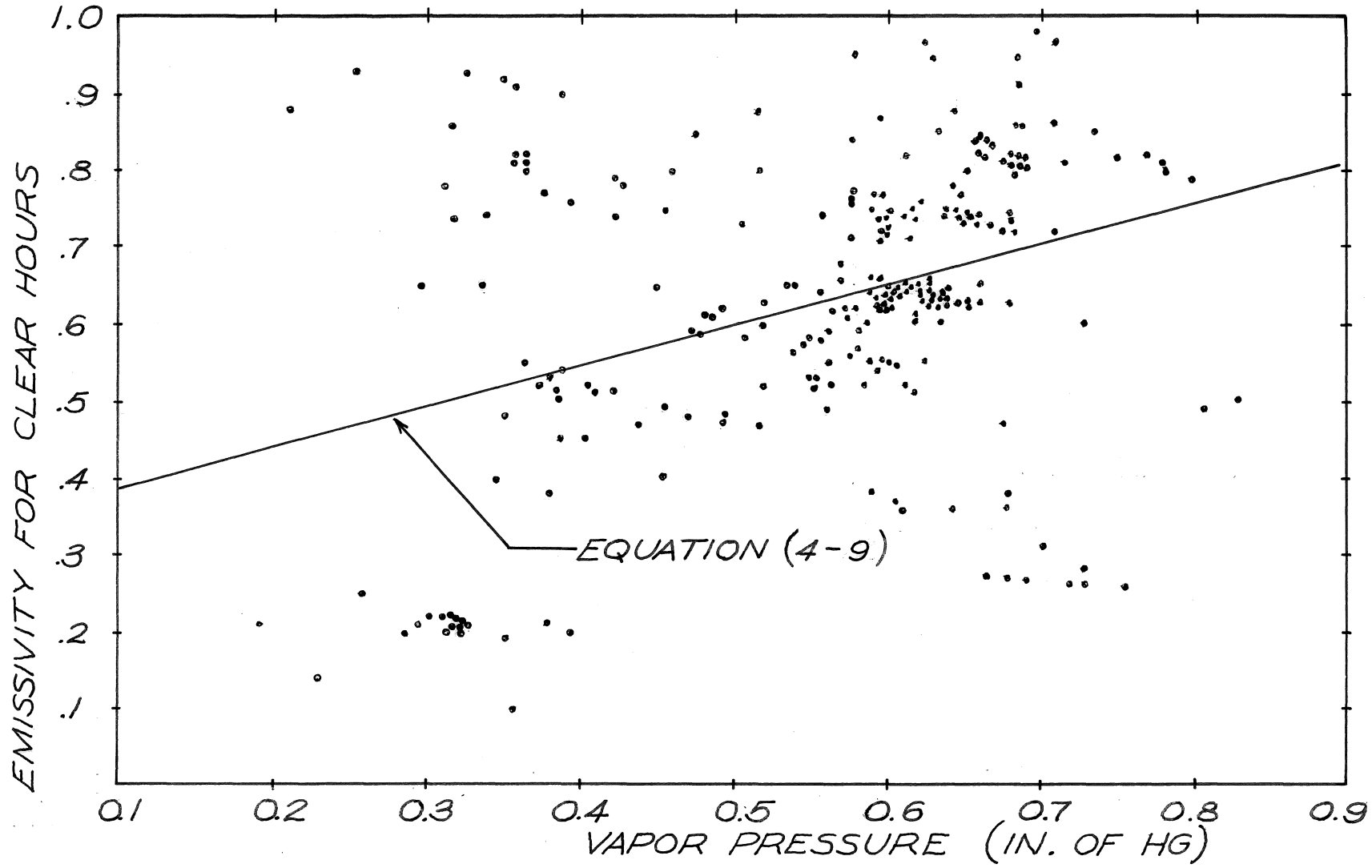

Figure 4-7. Atmospheric emissivity as a function of vapor pressure.

4.5 Cloudy Sky Longwave Radiation

In light of the weak predictive equation developed for the clear sky emissivities, the evaluation of the effect of clouds is difficult. Using equation 4-9, clear sky emissivities were calculated. The ratio of emissivity with clouds calculated from equation 2-11 to that of equation 4-9 was then compared with both cloudiness and opaqueness in Figures 4-8 and 4-9. The results indicate a more or less uniform increase in emissivities with cloudiness and opaqueness, and the determination of a functional form is not really warranted. However, when a parabolic relationship is fitted through the data, the result is

$$I_a = \varepsilon\sigma T^4 \ (1+0.945\ C^2) \qquad (4\text{-}10)$$

and

$$I_a = \varepsilon\sigma T^4 \ (1+0.928\ O^2)\ . \qquad (4\text{-}11)$$

The multiple correlation coefficients for equations 4-10 and 4-11 are 0.53 and 0.43, respectively. Although these prediction equations are obviously subject to large fluctuations, equations 4-9 and 4-10 might be used in north-central Florida.

5. CONCLUSIONS

5.1 Shortwave Radiation Predictions

Shortwave radiation may be reliably predicted using equations 4-6 and 4-8. However, no correlation could be determined between atmospheric transmission coefficient and vapor pressure, and a correlation with air mass was to be expected. The resulting prediction equation 4-6 is therefore probably valid only for the north-central Florida area of the measurements, where climatic conditions give rise to no variation with vapor content. However, the cloudiness and opaqueness relationships of equations 4-7 and 4-8 may be extended to other localities. The use of opaqueness instead of cloudiness results in slightly better correlation. These simple predictive relationships are most suitable to the type of data typically gathered at weather stations, and therefore include only the parameters indicated.

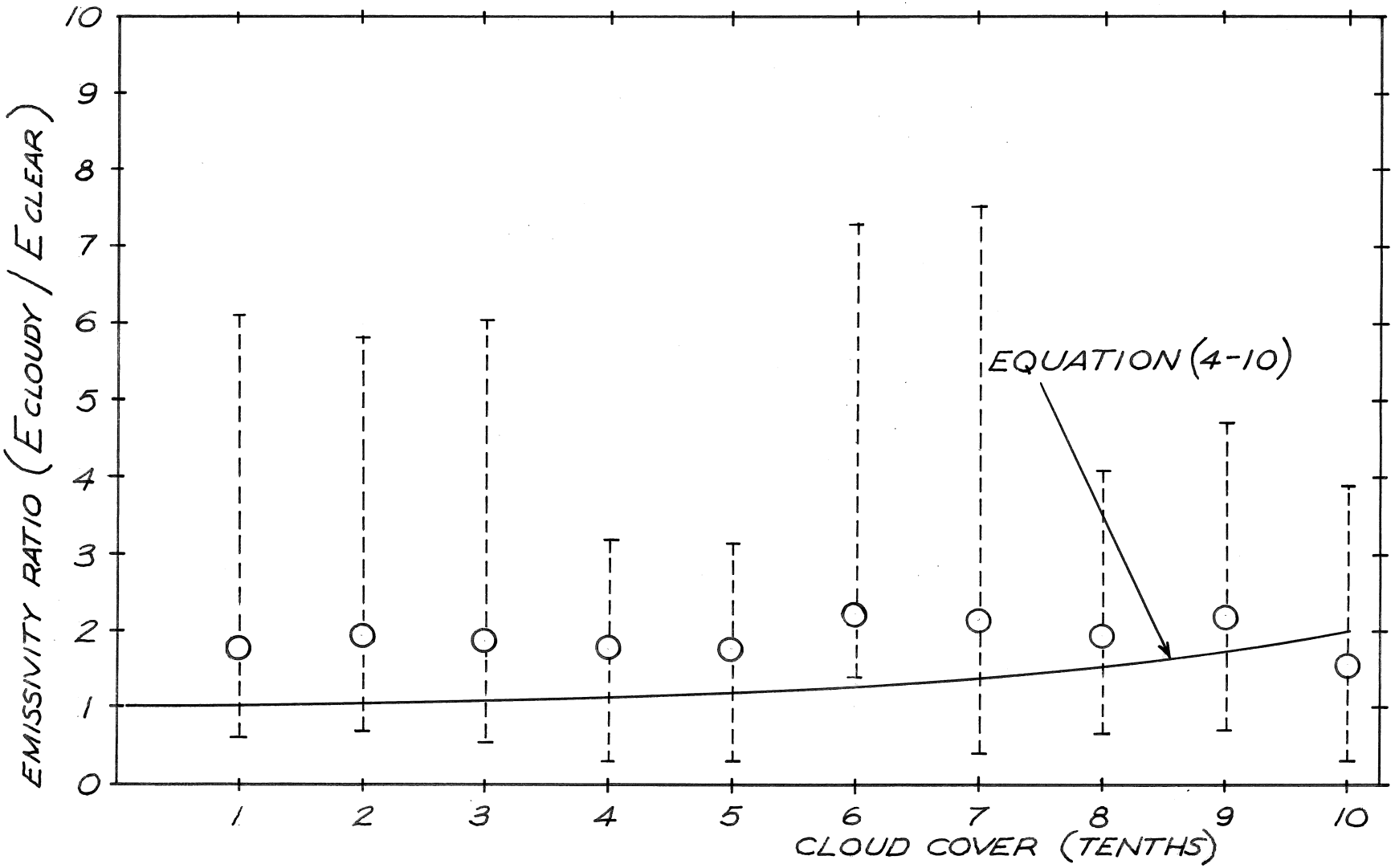

Figure 4-8. Effect of cloudiness on clear sky longwave radiation. Circles are mean values over the range indicated by the dashed lines.

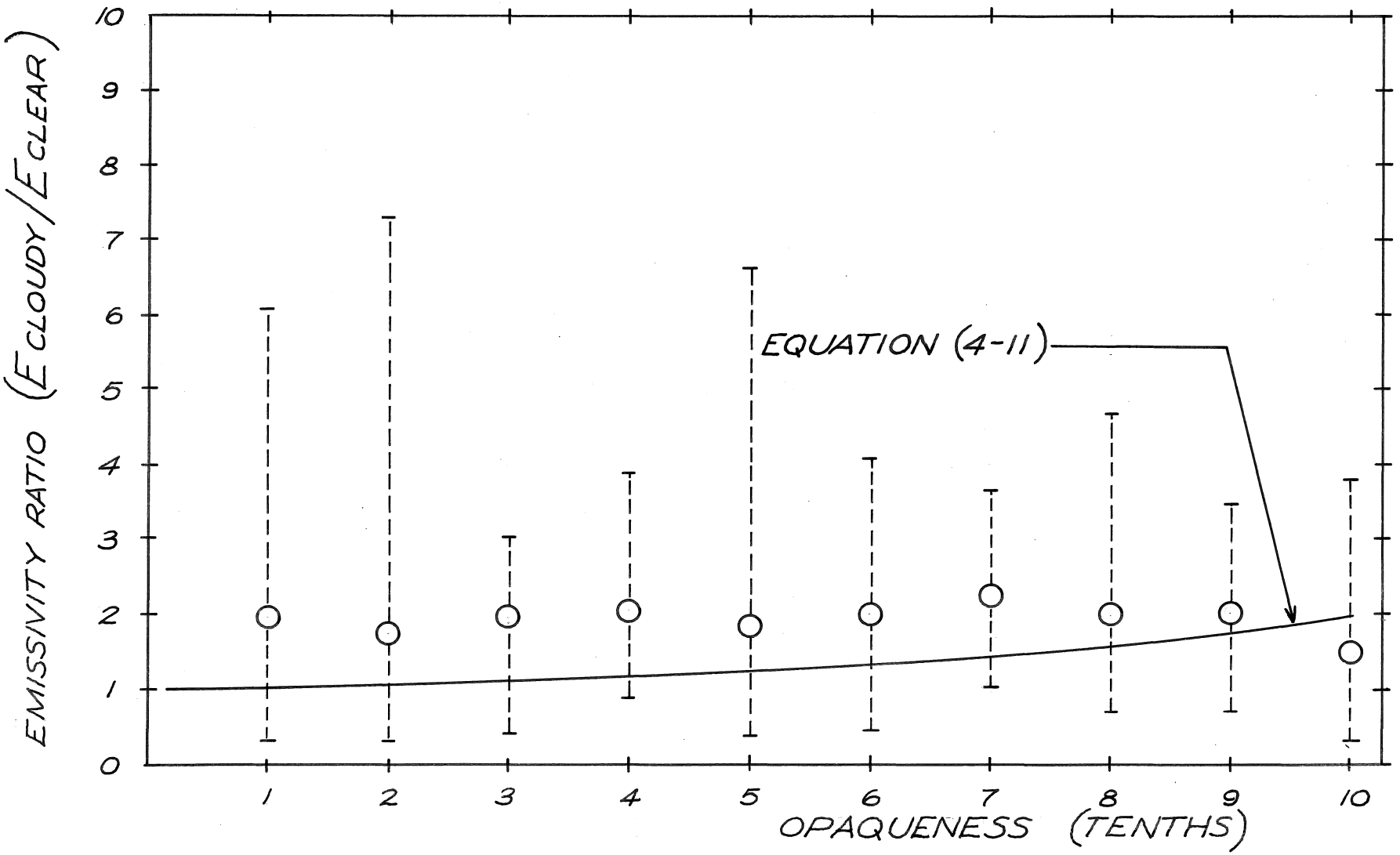

Figure 4-9. Effect of opaqueness on clear sky longwave radiation. Circles are mean values over the range indicated by the dashed lines.

5.2 Longwave Radiation Predictions

The prediction of longwave radiation may be accomplished using equations 4-9 and 4-10; however, the scatter of the data leaves these relationships open to some doubt. The scatter is probably caused in part by inaccuracies in nighttime radiation values. On the basis of the data, a linear relationship of emissivity with vapor pressure was found to be as suitable as any other proposed functional form.

5.3 Energy Budget Evaluation

The preceding sections indicate the manner in which the short and longwave radiation components of the energy budget may be calculated. The inclusion of the predictive equations in the solution of the energy budget equation 1-1 is demonstrated in Appendix I, along with the simple numerical scheme involved. Although the numerical method employed is not new, the evaluation of the temperature distributions of north-central Florida waters should be considerably improved by the use of radiation prediction methods suited to the area. The relationship between measured and predicted temperature values indicates that while shortwave predictions are good, predicted longwave emissivities may be too low.

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APPENDIX I: A SAMPLE ENERGY BUDGET CALCULATION

I.1 Introduction

The use of equation 1-1 and the radiation prediction equations to evaluate temperature changes is shown by an example in which measured and computed temperatures may be compared. The energy budget equation 1-1 is solved numerically, and predicted temperatures are compared with those measured in Newnan's Lake, a 6000 acre lake (volume = 36.6×10^6 cubic meters) on the eastern edge of Gainesville, Florida.

I.2 Numerical Method

For a lake, the net advection is zero, and $Q_v = 0$ in equation 1-1. Hence, expressions are required only for Q_s, Q_a, and Q_L before the change in temperature can be calculated.

The net incident shortwave radiation is

$$Q_s = AI\ (1-R) \qquad \text{(I-1)}$$

where

A = area of absorbing surface,
I = incident shortwave radiation found from equation 4-8,
R = reflection coefficient or albedo.

The albedo may be calculated as a function of solar altitude and cloud cover from Anderson's (1) empirical formula

$$R = a_o\ \alpha^{b_o} \qquad \text{(I-2)}$$

where α is in degrees and the constants a_o and b_o are given in Table I-1.

TABLE I-1

Cloudiness C	0 Clear		0.1 - 0.5 Scattered		0.6 - 0.9 Broken		1.0 Overcast	
	a_o	b_o	a_o	b_o	a_o	b_o	a_o	b_o
Constants	1.18	-0.77	2.20	-0.97	0.95	-0.75	0.35	-1.45

The net incoming longwave radiation may be evaluated from

$$Q_a = 0.97\ AI_a \qquad \text{(I-3)}$$

where a reflection coefficient of 0.03 has been assumed and I_a is evaluated from equations 4-9 and 4-10.

Heat losses are due to back radiation, evaporation and conduction. The back radiation flux, I_b, is

$$I_b = 0.97\ \sigma T_w^4 \qquad \text{(I-4)}$$

where T_w is the water temperature (assumed uniform over depth) and an emissivity of 0.97 has been used. The flux of latent and sensible heat, I_e, due to evaporation and conduction may be evaluated from Kohler's (12) formula

$$I_e = 0.000135\ W\rho(e_s - r_h e_a)\left[L + c_p T_w + \frac{372\ (T_w - T_a)}{(e_s - r_h e_a)}\right] \qquad \text{(I-5)}$$

where I_e is in kilocalories/m^2 - day, and where other variables are defined as follows with the exact units that must be used:

ρ = water density in k_g/m^3,
W = wind speed in m/sec, measured 2 m above water surface,
e_s = saturation vapor pressure at temperature of water, T_w, in mb (milli-bars),
e_a = saturation vapor pressure at temperature of air, T_a, in mb,
r_h = relative humidity expressed as a fraction,
L = latent heat of evaporization in kilocalories/k_g,
c_p = specific heat in kilocalories/k_g - °C,
T_w, T_a = water and air temperatures respectively, in °C.

Heat losses may thus be evaluated:

$$Q_L = A\ (I_b + I_e) \quad . \qquad \text{(I-6)}$$

When the temperature of the water, T_w, is known at a given time step, n, it may be evaluated at the succeeding time step, n+1, a time Δt later, by the finite difference solution of equation 1-1. The initial temperature (n=0) is given by an initial condition. Thus

$$T_{w_{n+1}} = T_{w_n} + \frac{\Delta t}{\rho c_p \forall} (Q_{s_n} + Q_{a_n} - Q_{L_n}) \qquad \text{(I-7)}$$

where the subscript n indicates that the variable is to be evaluated from water temperature and meteorological data at that time step. The numerical scheme is therefore a simple explicit one in which water temperatures used to evaluate heat losses are obtained from the preceding iteration. Equation I-7 is readily programmed for computer evaluation.

I.3 Calculations for Newnan's Lake

Hourly radiation values were obtained from the prediction equations and an arithmetic average taken to obtain the daily fluxes, Q_s and Q_a. Equation I-7 was then solved with a time step of Δt = 1 day for the period April 2 to June 1, 1970. In evaluation of evaporation and conduction losses, a daily average wind speed based on airport measurements, was used. The predicted temperatures were compared with measured values as shown in Figure I-1. Use of equation 4-9 for predicted emissivities results in predicted temperatures that are too low, however the trend is correct. Higher emissivities, as given by Anderson's (1) equation:

$$\varepsilon = 0.74 + 0.166\ e \qquad \text{(I-8)}$$

with e in in. Hg, result in better agreement as shown in the figure. This indicates that emissivities predicted by equation 4-9 are probably too low. However, variability in evaporation predictions undoubtedly contributes to the error in predicted temperatures.

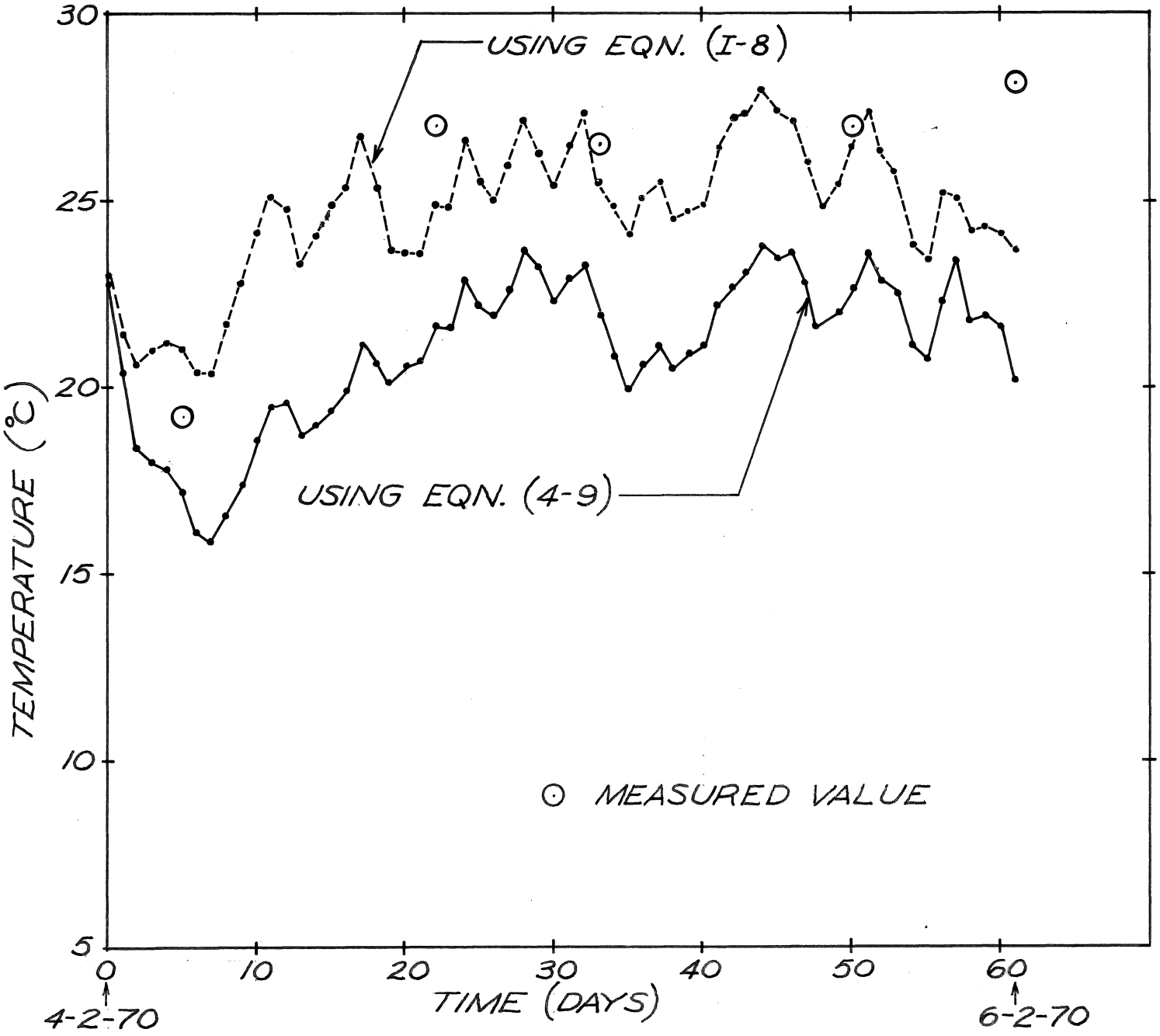

Figure I-1. Comparison of predicted and measured temperatures in Newnan's Lake.

APPENDIX II: LISTING OF DATA

This appendix contains a listing of measured and computed data analyzed in this report. The data are hourly values for the period March 18, 1970 (day 77) to August 13, 1970 (day 225). Data gathered in August were not included in the analysis.

A series of asterisks appear at several places in the listing. These indicate that data are not available for these hours because recorders were occasionally shared with another project, or because of difficulties with the recorders. In addition, atmospheric transmission coefficients and emissivities are calculated for clear sky hours only. A single asterisk above a column indicates that these are measured values.

The column headings are as follows:

DAY = number of day of year (e.g. March 18 = day 77).

HR = number of hour of day (e.g. noon = hour 12). Hour corresponds to Eastern Standard Time prior to April 26 and Eastern Daylight Time from April 26 and beyond.

SEQN = a sequence number for use in organizing the data, (note: an overlap in sequence numbers occurs at day 212).

SOLC = solar constant adjusted for earth-sun distance (from equation 2-3) in langley/minute.

DECLN = declination of earth (from equation 2-6) in degrees.

HRANG = solar altitude angle, α, (from equation 2-5), in degrees.

AIRMS = optical air mass (from equation 2-11 and 2-12).

CL = cloudiness, in tenths of sky covered.

OP = opaqueness, in tenths of sky covered.

RHM = relative humidity, in percent.

VPRES = vapor pressure, (from equation 4-3) in inches of mercury.

SWRADT = total shortwave radiation in langley/hour.

TLRADT = total radiation (all wavelengths) in langley/hour.

LWRADT = longwave radiation (TLRADT-SWRADT) in langley/hour.

TRAN = atmospheric transmission coefficient, (from equation 4-5), for clear sky hours only.

EMSV = atmospheric emissivity, (from equation 2-27), for clear sky hours only.

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
77	1	1	2.02	-0.50	5.73	36.00	10	10	97	58	0.471	0.0	13.20	13.20	****	0.39
77	2	2	2.02	-0.50	5.73	36.00	10	10	97	58	0.471	0.0	13.20	13.20	****	0.39
77	3	3	2.02	-0.50	5.73	36.00	7	3	99	56	0.447	0.0	13.20	13.20	****	0.40
77	4	4	2.02	-0.50	5.73	36.00	5	2	100	56	0.452	0.0	13.20	13.20	****	0.40
77	5	5	2.02	-0.50	5.73	36.00	0	0	100	56	0.452	0.0	13.20	13.20	****	0.40
77	6	6	2.02	-0.50	5.73	10.94	8	4	100	56	0.452	0.0	13.20	13.20	****	0.40
77	7	7	2.02	-0.50	8.45	6.52	2	2	100	56	0.452	4.86	22.32	17.46	****	0.53
77	8	8	2.02	-0.50	21.39	2.72	0	0	100	59	0.503	30.78	68.76	37.98	0.88	****
77	9	9	2.02	-0.50	33.88	1.79	0	0	94	66	0.605	55.08	114.36	59.28	0.89	****
77	10	10	2.02	-0.50	45.38	1.40	2	2	85	70	0.628	68.04	134.28	66.24	****	****
77	11	11	2.02	-0.50	54.82	1.22	9	8	80	73	0.654	46.98	103.56	56.58	****	****
77	12	12	2.02	-0.50	60.11	1.15	8	7	70	74	0.592	76.14	145.08	68.94	****	****
77	13	13	2.02	-0.50	59.01	1.17	9	9	64	77	0.598	79.38	159.96	80.58	****	****
77	14	14	2.02	-0.50	52.07	1.27	8	8	56	80	0.578	79.38	159.96	80.58	****	****
77	15	15	2.02	-0.50	41.78	1.50	9	9	56	80	0.578	63.18	158.16	94.98	****	****
77	16	16	2.02	-0.50	29.87	2.00	8	8	56	80	0.578	46.98	96.96	49.98	****	****
77	17	17	2.02	-0.50	17.20	3.35	6	6	56	79	0.559	30.78	75.36	44.58	****	****
77	18	18	2.02	-0.50	5.73	11.94	7	3	60	76	0.543	25.92	39.84	13.92	****	0.36
77	19	19	2.02	-0.50	8.94	6.19	1	1	75	72	0.593	0.32	13.37	13.04	****	0.35
77	20	20	2.02	-0.50	5.73	36.00	0	0	85	69	0.607	0.0	13.20	13.20	****	0.36
77	21	21	2.02	-0.50	5.73	36.00	0	0	93	68	0.642	0.0	13.20	13.20	****	0.36
77	22	22	2.02	-0.50	5.73	36.00	0	0	97	65	0.603	0.0	13.20	13.20	****	0.37
77	23	23	2.02	-0.50	5.73	36.00	0	0	98	64	0.588	0.0	13.20	13.20	****	0.38
77	24	24	2.02	-0.50	5.73	36.00	8	8	99	63	0.574	0.0	13.20	13.20	****	0.38
78	1	25	2.01	-0.10	5.73	36.00	10	10	99	73	0.810	0.0	19.80	19.80	****	0.53
78	2	26	2.01	-0.10	5.73	36.00	10	10	99	72	0.783	0.0	19.80	19.80	****	0.53
78	3	27	2.01	-0.10	5.73	36.00	10	10	99	72	0.783	0.0	19.80	19.80	****	0.53
78	4	28	2.01	-0.10	5.73	36.00	10	10	99	72	0.783	0.0	19.80	19.80	****	0.53
78	5	29	2.01	-0.10	5.73	36.00	10	10	99	71	0.756	0.0	19.80	19.80	****	0.53
78	6	30	2.01	-0.10	5.73	11.19	10	10	99	70	0.732	0.0	19.80	19.80	****	0.54
78	7	31	2.01	-0.10	8.58	6.43	10	10	99	70	0.732	4.86	35.52	30.66	****	0.83
78	8	32	2.01	-0.10	21.54	2.71	10	10	100	72	0.791	21.87	57.54	35.67	****	0.95
78	9	33	2.01	-0.10	34.05	1.78	10	7	100	65	0.622	46.17	96.54	50.37	****	****
78	10	34	2.01	-0.10	45.61	1.40	10	7	92	69	0.657	57.51	122.22	64.71	****	****
78	11	35	2.01	-0.10	55.13	1.22	10	6	80	76	0.724	62.37	137.94	75.57	****	****
78	12	36	2.01	-0.10	60.50	1.15	10	6	65	80	0.671	75.33	151.26	75.93	****	****
78	13	37	2.01	-0.10	59.41	1.16	10	5	56	84	0.658	86.67	170.34	83.67	****	****
78	14	38	2.01	-0.10	52.44	1.26	10	4	52	84	0.611	75.33	151.26	75.93	****	****
78	15	39	2.01	-0.10	42.10	1.49	10	4	48	84	0.564	55.89	114.78	58.89	****	****
78	16	40	2.01	-0.10	30.16	1.98	9	4	52	82	0.573	34.83	77.46	42.63	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
78	17	41	2.01	-0.10	17.46	3.30	9	9	53	82	0.584	33.21	70.02	36.81	****	0.91
78	18	42	2.01	-0.10	5.73	11.39	8	7	58	79	0.579	5.67	22.74	17.07	****	0.43
78	19	43	2.01	-0.10	8.68	6.36	9	6	65	76	0.588	0.32	13.37	13.04	****	0.34
78	20	44	2.01	-0.10	5.73	36.00	10	4	70	73	0.573	0.0	13.20	13.20	****	0.35
78	21	45	2.01	-0.10	5.73	36.00	3	1	79	71	0.604	0.0	13.20	13.20	****	0.36
78	22	46	2.01	-0.10	5.73	36.00	3	1	89	68	0.614	0.0	13.20	13.20	****	0.36
78	23	47	2.01	-0.10	5.73	36.00	3	1	94	66	0.605	0.0	13.20	13.20	****	0.37
78	24	48	2.01	-0.10	5.73	36.00	6	4	96	66	0.618	0.0	13.20	13.20	****	0.37
79	1	49	2.01	0.30	5.73	36.00	8	7	96	66	0.618	0.0	13.39	13.39	****	0.37
79	2	50	2.01	0.30	5.73	36.00	10	10	96	66	0.618	0.0	19.99	19.99	****	0.56
79	3	51	2.01	0.30	5.73	36.00	10	10	96	66	0.618	0.0	19.99	19.99	****	0.56
79	4	52	2.01	0.30	5.73	36.00	10	10	96	66	0.618	0.0	19.99	19.99	****	0.56
79	5	53	2.01	0.30	5.73	36.00	10	10	97	66	0.625	0.0	19.99	19.99	****	0.56
79	6	54	2.01	0.30	5.73	11.45	4	3	97	65	0.603	0.0	13.39	13.39	****	0.38
79	7	55	2.01	0.30	8.71	6.34	7	6	98	65	0.610	2.83	21.27	18.43	****	0.52
79	8	56	2.01	0.30	21.68	2.69	10	9	97	66	0.625	16.60	41.61	25.00	****	0.70
79	9	57	2.01	0.30	34.22	1.77	9	8	95	68	0.655	42.52	88.05	45.52	****	****
79	10	58	2.01	0.30	45.83	1.39	7	5	82	70	0.606	50.62	112.05	61.42	****	****
79	11	59	2.01	0.30	55.43	1.21	8	6	68	76	0.615	73.30	150.21	76.90	****	****
79	12	60	2.01	0.30	60.88	1.14	8	7	65	78	0.629	70.06	135.33	65.26	****	****
79	13	61	2.01	0.30	59.82	1.16	8	7	63	78	0.609	66.82	140.25	73.42	****	****
79	14	62	2.01	0.30	52.80	1.25	7	6	64	78	0.619	61.96	131.13	69.16	****	****
79	15	63	2.01	0.30	42.42	1.48	7	6	65	78	0.629	53.86	120.33	66.46	****	****
79	16	64	2.01	0.30	30.45	1.97	9	6	65	78	0.629	40.90	87.21	46.30	****	****
79	17	65	2.01	0.30	17.73	3.25	10	6	70	76	0.633	21.46	50.73	29.26	****	0.76
79	18	66	2.01	0.30	5.73	10.87	10	8	85	71	0.649	3.64	28.29	24.64	****	0.66
79	19	67	2.01	0.30	8.42	6.54	10	10	91	69	0.650	0.40	20.01	19.60	****	0.54
79	20	68	2.01	0.30	5.73	36.00	10	10	92	69	0.657	0.40	20.01	19.60	****	0.54
79	21	69	2.01	0.30	5.73	36.00	10	10	92	70	0.680	0.0	19.60	19.60	****	0.53
79	22	70	2.01	0.30	5.73	36.00	10	10	94	70	0.695	0.0	19.60	19.60	****	0.53
79	23	71	2.01	0.30	5.73	36.00	10	10	95	70	0.702	0.0	19.60	19.60	****	0.53
79	24	72	2.01	0.30	5.73	36.00	10	10	96	73	0.785	0.0	19.60	19.60	****	0.52
80	1	73	2.01	0.70	5.73	36.00	10	10	96	67	0.640	0.0	19.80	19.80	****	0.55
80	2	74	2.01	0.70	5.73	36.00	10	10	96	67	0.640	0.0	19.80	19.80	****	0.55
80	3	75	2.01	0.70	5.73	36.00	10	10	96	67	0.640	0.0	19.80	19.80	****	0.55
80	4	76	2.01	0.70	5.73	36.00	10	10	97	67	0.647	0.0	19.80	19.80	****	0.55
80	5	77	2.01	0.70	5.73	36.00	10	10	97	67	0.647	0.0	19.80	19.80	****	0.55
80	6	78	2.01	0.70	5.73	11.72	10	10	97	67	0.647	0.0	19.80	19.80	****	0.55
80	7	79	2.01	0.70	8.84	6.26	10	10	97	67	0.647	1.62	20.64	19.02	****	0.53
80	8	80	2.01	0.70	21.82	2.67	10	10	97	68	0.669	6.48	29.76	23.28	****	0.64

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
80	9	81	2.01	0.70	34.39	1.77	10	10	93	70	0.687	17.82	48.84	31.02	****	0.84
80	10	82	2.01	0.70	46.05	1.39	10	10	89	71	0.680	24.30	65.40	41.10	****	****
80	11	83	2.01	0.70	55.72	1.21	10	10	80	71	0.611	37.26	91.92	54.66	****	****
80	12	84	2.01	0.70	61.26	1.14	10	10	68	76	0.615	64.80	139.20	74.40	****	****
80	13	85	2.01	0.70	60.22	1.15	10	10	62	77	0.580	61.56	130.92	69.36	****	****
80	14	86	2.01	0.70	53.16	1.25	9	7	60	78	0.580	37.26	111.72	74.46	****	****
80	15	87	2.01	0.70	42.73	1.47	10	10	70	76	0.633	21.06	63.72	42.66	****	****
80	16	88	2.01	0.70	30.73	1.95	10	10	70	75	0.612	22.68	57.96	35.28	****	0.92
80	17	89	2.01	0.70	18.00	3.20	10	10	70	75	0.612	12.96	39.72	26.76	****	0.70
80	18	90	2.01	0.70	5.73	10.41	10	9	73	74	0.618	6.48	29.76	23.28	****	0.61
80	19	91	2.01	0.70	8.15	6.74	10	10	81	72	0.641	0.32	13.37	13.04	****	0.35
80	20	92	2.01	0.70	5.73	36.00	9	7	87	70	0.643	0.0	13.20	13.20	****	0.36
80	21	93	2.01	0.70	5.73	36.00	9	6	90	69	0.643	0.0	13.20	13.20	****	0.36
80	22	94	2.01	0.70	5.73	36.00	9	7	92	69	0.657	0.0	13.20	13.20	****	0.36
80	23	95	2.01	0.70	5.73	36.00	10	10	92	69	0.657	0.0	19.80	19.80	****	0.54
80	24	96	2.01	0.70	5.73	36.00	10	10	92	70	0.680	0.0	19.80	19.80	****	0.54
81	1	97	2.01	1.10	5.73	36.00	10	10	92	70	0.680	0.0	19.80	19.80	****	0.54
81	2	98	2.01	1.10	5.73	36.00	10	10	92	70	0.680	0.0	19.80	19.80	****	0.54
81	3	99	2.01	1.10	5.73	36.00	10	10	93	70	0.687	0.0	19.80	19.80	****	0.54
81	4	100	2.01	1.10	5.73	36.00	10	10	98	67	0.654	0.0	6.60	6.60	****	0.18
81	5	101	2.01	1.10	5.73	36.00	10	10	98	66	0.631	0.0	6.60	6.60	****	0.18
81	6	102	2.01	1.10	5.73	12.01	10	10	98	65	0.610	0.0	19.80	19.80	****	0.56
81	7	103	2.01	1.10	8.97	6.17	10	10	96	64	0.576	0.81	20.22	19.41	****	0.55
81	8	104	2.01	1.10	21.97	2.66	10	10	95	63	0.551	2.43	14.46	12.03	****	0.34
81	9	105	2.01	1.10	34.56	1.76	10	10	98	60	0.512	3.24	14.88	11.64	****	0.34
81	10	106	2.01	1.10	46.27	1.38	10	10	97	59	0.488	11.34	19.08	7.74	****	0.23
81	11	107	2.01	1.10	56.02	1.20	9	9	96	60	0.501	19.44	62.88	43.44	****	****
81	12	108	2.01	1.10	61.64	1.14	10	10	94	55	0.410	11.34	38.88	27.54	****	0.84
81	13	109	2.01	1.10	60.63	1.15	10	10	96	54	0.403	17.82	55.44	37.62	****	****
81	14	110	2.01	1.10	53.53	1.24	10	10	90	58	0.437	53.46	120.12	66.66	****	****
81	15	111	2.01	1.10	43.05	1.46	5	4	63	65	0.392	66.42	146.64	80.22	****	****
81	16	112	2.01	1.10	31.02	1.93	3	1	52	66	0.335	48.60	104.40	55.80	****	****
81	17	113	2.01	1.10	18.27	3.16	6	2	52	65	0.323	29.16	61.32	32.16	****	0.91
81	18	114	2.01	1.10	5.73	9.97	1	1	52	64	0.312	2.43	14.46	12.03	****	0.34
81	19	115	2.01	1.10	7.89	6.94	3	3	66	58	0.321	0.0	6.60	6.60	****	0.20
81	20	116	2.01	1.10	5.73	36.00	5	5	72	54	0.302	0.0	6.60	6.60	****	0.20
81	21	117	2.01	1.10	5.73	36.00	0	0	79	53	0.320	0.0	6.60	6.60	****	0.20
81	22	118	2.01	1.10	5.73	36.00	5	5	81	52	0.316	0.0	6.60	6.60	****	0.21
81	23	119	2.01	1.10	5.73	36.00	3	1	75	50	0.271	0.0	******	******	****	****
81	24	120	2.01	1.10	5.73	36.00	5	2	71	49	0.248	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
82	1	121	2.01	1.50	5.73	36.00	0	0	73	47	0.237	0.0	******	******	****	****
82	2	122	2.01	1.50	5.73	36.00	0	0	74	46	0.231	0.0	******	******	****	****
82	3	123	2.01	1.50	5.73	36.00	0	0	74	44	0.214	0.0	******	******	****	****
82	4	124	2.01	1.50	5.73	36.00	0	0	79	43	0.220	0.0	******	******	****	****
82	5	125	2.01	1.50	5.73	36.00	0	0	83	41	0.213	0.0	******	******	****	****
82	6	126	2.01	1.50	5.73	12.31	0	0	88	40	0.218	0.0	******	******	****	****
82	7	127	2.01	1.50	9.10	6.09	0	0	85	42	0.228	4.86	9.12	4.26	0.80	0.14
82	8	128	2.01	1.50	22.11	2.64	1	0	82	47	0.266	24.30	45.60	21.30	****	0.69
82	9	129	2.01	1.50	34.73	1.75	9	4	62	50	0.224	******	******	******	****	****
82	10	130	2.01	1.50	46.49	1.38	7	3	55	50	0.199	******	******	******	****	****
82	11	131	2.01	1.50	56.31	1.20	8	3	45	55	0.196	******	******	******	****	****
82	12	132	2.01	1.50	62.02	1.13	6	3	44	57	0.206	******	******	******	****	****
82	13	133	2.01	1.50	61.03	1.14	7	3	42	60	0.219	******	******	******	****	****
82	14	134	2.01	1.50	53.89	1.24	8	3	40	62	0.224	******	******	******	****	****
82	15	135	2.01	1.50	43.37	1.45	8	3	40	63	0.232	56.70	121.80	65.10	****	****
82	16	136	2.01	1.50	31.30	1.92	0	0	42	63	0.244	45.36	102.72	57.36	0.84	****
82	17	137	2.01	1.50	18.53	3.12	0	0	45	62	0.252	29.16	61.32	32.16	0.92	0.93
82	18	138	2.01	1.50	5.73	9.57	0	0	51	59	0.257	9.72	18.24	8.52	0.98	0.25
82	19	139	2.01	1.50	7.63	7.15	0	0	65	55	0.283	0.0	6.60	6.60	****	0.20
82	20	140	2.01	1.50	5.73	36.00	0	0	74	54	0.311	0.0	6.60	6.60	****	0.20
82	21	141	2.01	1.50	5.73	36.00	0	0	81	50	0.293	0.0	6.60	6.60	****	0.21
82	22	142	2.01	1.50	5.73	36.00	0	0	87	50	0.315	0.0	6.60	6.60	****	0.21
82	23	143	2.01	1.50	5.73	36.00	0	0	88	50	0.319	0.0	6.60	6.60	****	0.21
82	24	144	2.01	1.50	5.73	36.00	0	0	91	49	0.318	0.0	6.60	6.60	****	0.21
83	1	145	2.01	1.90	5.73	36.00	0	0	93	48	0.312	0.0	6.60	6.60	****	0.21
83	2	146	2.01	1.90	5.73	36.00	0	0	96	48	0.323	0.0	6.60	6.60	****	0.21
83	3	147	2.01	1.90	5.73	36.00	0	0	97	47	0.314	0.0	6.60	6.60	****	0.21
83	4	148	2.01	1.90	5.73	36.00	0	0	99	46	0.309	0.0	6.60	6.60	****	0.22
83	5	149	2.01	1.90	5.73	36.00	0	0	100	46	0.312	0.0	6.60	6.60	****	0.22
83	6	150	2.01	1.90	5.73	12.63	0	0	100	45	0.300	0.0	6.60	6.60	****	0.22
83	7	151	2.01	1.90	9.23	6.01	3	1	100	44	0.289	4.86	15.72	10.86	****	0.36
83	8	152	2.01	1.90	22.25	2.62	0	0	100	47	0.324	22.68	51.36	28.68	0.77	0.93
83	9	153	2.01	1.90	34.90	1.74	0	0	92	55	0.401	42.12	94.44	52.32	0.75	****
83	10	154	2.01	1.90	46.70	1.37	0	0	62	60	0.324	58.32	129.24	70.92	0.74	****
83	11	155	2.01	1.90	56.60	1.20	0	0	42	67	0.280	58.32	149.04	90.72	0.63	****
83	12	156	2.01	1.90	62.40	1.13	0	0	41	80	0.423	******	******	******	****	****
83	13	157	2.01	1.90	61.43	1.14	0	0	40	72	0.316	81.00	174.00	93.00	0.79	****
83	14	158	2.01	1.90	54.25	1.23	1	1	40	72	0.316	77.76	165.72	87.96	****	****
83	15	159	2.01	1.90	43.68	1.45	3	1	40	72	0.316	69.66	141.72	72.06	****	****
83	16	160	2.01	1.90	31.58	1.90	3	1	44	70	0.325	56.70	108.60	51.90	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
83	17	161	2.01	1.90	18.80	3.08	0	0	45	68	0.310	37.26	65.52	28.26	0.99	0.78
83	18	162	2.01	1.90	5.73	9.20	3	1	47	66	0.303	17.82	29.04	11.22	****	0.31
83	19	163	2.01	1.90	7.37	7.38	4	1	55	62	0.308	3.24	8.28	5.04	****	0.15
83	20	164	2.01	1.90	5.73	36.00	3	1	60	60	0.313	0.0	6.60	6.60	****	0.19
83	21	165	2.01	1.90	5.73	36.00	2	1	75	57	0.351	0.0	6.60	6.60	****	0.20
83	22	166	2.01	1.90	5.73	36.00	3	1	90	54	0.378	0.0	6.60	6.60	****	0.20
83	23	167	2.01	1.90	5.73	36.00	0	0	93	54	0.391	0.0	6.60	6.60	****	0.20
83	24	168	2.01	1.90	5.73	36.00	0	0	97	52	0.378	0.0	6.60	6.60	****	0.21
84	1	169	2.01	2.30	5.73	36.00	7	3	98	50	0.355	0.0	6.21	6.21	****	0.20
84	2	170	2.01	2.30	5.73	36.00	5	2	98	50	0.355	0.0	6.21	6.21	****	0.20
84	3	171	2.01	2.30	5.73	36.00	5	2	100	49	0.349	0.0	6.21	6.21	****	0.20
84	4	172	2.01	2.30	5.73	36.00	6	6	100	49	0.349	0.0	6.21	6.21	****	0.20
84	5	173	2.01	2.30	5.73	36.00	9	9	100	49	0.349	0.0	6.21	6.21	****	0.20
84	6	174	2.01	2.30	5.73	12.96	9	7	100	49	0.349	0.0	12.81	12.81	****	0.41
84	7	175	2.01	2.30	9.36	5.94	10	9	100	49	0.349	4.05	21.90	17.85	****	0.57
84	8	176	2.01	2.30	22.39	2.61	8	6	100	50	0.362	20.25	56.70	36.45	****	****
84	9	177	2.01	2.30	35.06	1.74	7	3	85	58	0.413	49.41	98.22	48.81	****	****
84	10	178	2.01	2.30	46.91	1.37	7	3	58	63	0.336	52.65	106.50	53.85	****	****
84	11	179	2.01	2.30	56.89	1.19	9	4	55	66	0.354	54.27	127.14	72.87	****	****
84	12	180	2.01	2.30	62.78	1.12	9	4	48	71	0.367	76.95	165.30	88.35	****	****
84	13	181	2.01	2.30	61.84	1.13	9	6	51	71	0.390	59.13	136.26	77.13	****	****
84	14	182	2.01	2.30	54.61	1.23	10	10	51	70	0.377	25.11	72.42	47.31	****	****
84	15	183	2.01	2.30	43.99	1.44	10	10	52	70	0.384	17.01	48.42	31.41	****	0.85
84	16	184	2.01	2.30	31.86	1.89	10	10	55	70	0.406	10.53	38.46	27.93	****	0.76
84	17	185	2.01	2.30	19.06	3.03	10	10	60	69	0.428	0.0	26.79	26.79	****	0.73
84	18	186	2.01	2.30	5.99	8.86	10	10	70	67	0.467	0.0	******	******	****	****
84	19	187	2.01	2.30	7.10	7.63	10	10	88	64	0.528	0.0	13.59	13.59	****	0.39
84	20	188	2.01	2.30	5.73	36.00	10	10	82	65	0.510	0.0	13.59	13.59	****	0.38
84	21	189	2.01	2.30	5.73	36.00	10	10	83	65	0.516	0.0	13.59	13.59	****	0.38
84	22	190	2.01	2.30	5.73	36.00	10	10	90	64	0.540	0.0	20.19	20.19	****	0.57
84	23	191	2.01	2.30	5.73	36.00	10	10	94	64	0.564	0.0	20.19	20.19	****	0.57
84	24	192	2.01	2.30	5.73	36.00	10	10	94	64	0.564	0.0	13.59	13.59	****	0.39
85	1	193	2.01	2.70	5.73	36.00	10	10	95	62	0.532	0.0	13.59	13.59	****	0.39
85	2	194	2.01	2.70	5.73	36.00	10	10	98	61	0.529	0.0	13.59	13.59	****	0.40
85	3	195	2.01	2.70	5.73	36.00	10	10	98	61	0.529	0.0	13.59	13.59	****	0.40
85	4	196	2.01	2.70	5.73	36.00	10	10	98	61	0.529	0.0	20.19	20.19	****	0.59
85	5	197	2.01	2.70	5.73	36.00	10	10	98	61	0.529	0.0	20.19	20.19	****	0.59
85	6	198	2.01	2.70	5.73	13.30	10	10	97	60	0.506	0.0	13.59	13.59	****	0.40
85	7	199	2.01	2.70	9.48	5.86	10	10	97	60	0.506	0.81	20.22	19.41	****	0.57
85	8	200	2.01	2.70	22.52	2.59	10	10	97	61	0.524	4.05	21.90	17.85	****	0.52

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
85	9	201	2.01	2.70	35.23	1.73	10	10	97	62	0.543	7.29	30.18	22.89	****	0.66
85	10	202	2.01	2.70	47.12	1.36	10	10	96	62	0.538	10.53	38.46	27.93	****	0.81
85	11	203	2.01	2.70	57.18	1.19	10	10	90	63	0.522	21.87	64.14	42.27	****	****
85	12	204	2.01	2.70	63.16	1.12	10	10	75	69	0.535	38.07	92.34	54.27	****	****
85	13	205	2.01	2.70	62.24	1.13	9	9	68	72	0.538	60.75	143.70	82.95	****	****
85	14	206	2.01	2.70	54.97	1.22	9	9	62	72	0.490	54.27	127.14	72.87	****	****
85	15	207	2.01	2.70	44.30	1.43	9	9	62	72	0.490	46.17	122.94	76.77	****	****
85	16	208	2.01	2.70	32.14	1.87	8	7	61	72	0.483	36.45	84.90	48.45	****	****
85	17	209	2.01	2.70	19.33	3.00	9	7	60	72	0.475	28.35	67.50	39.15	****	****
85	18	210	2.01	2.70	6.25	8.54	8	6	60	72	0.475	13.77	33.54	19.77	****	0.53
85	19	211	2.01	2.70	6.84	7.89	1	1	68	66	0.438	2.43	14.46	12.03	****	0.34
85	20	212	2.01	2.70	5.73	36.00	4	3	76	65	0.473	0.81	13.62	12.81	****	0.36
85	21	213	2.01	2.70	5.73	36.00	4	3	82	64	0.492	0.0	12.81	12.81	****	0.36
85	22	214	2.01	2.70	5.73	36.00	4	3	88	62	0.493	0.0	12.81	12.81	****	0.37
85	23	215	2.01	2.70	5.73	36.00	6	4	92	61	0.497	0.0	12.81	12.81	****	0.37
85	24	216	2.01	2.70	5.73	36.00	8	8	94	61	0.508	0.0	12.81	12.81	****	0.37
86	1	217	2.01	3.10	5.73	36.00	7	6	94	61	0.508	0.0	13.20	13.20	****	0.38
86	2	218	2.01	3.10	5.73	36.00	4	3	80	60	0.418	0.0	13.20	13.20	****	0.39
86	3	219	2.01	3.10	5.73	36.00	5	4	66	58	0.321	0.0	13.20	13.20	****	0.39
86	4	220	2.01	3.10	5.73	36.00	5	4	65	58	0.316	0.0	13.20	13.20	****	0.39
86	5	221	2.01	3.10	5.73	36.00	7	6	65	57	0.304	0.0	13.20	13.20	****	0.40
86	6	222	2.01	3.10	5.73	13.67	9	8	64	56	0.289	0.0	13.20	13.20	****	0.40
86	7	223	2.01	3.10	9.61	5.79	10	10	63	54	0.265	3.24	14.88	11.64	****	0.36
86	8	224	2.01	3.10	22.66	2.58	10	5	63	54	0.265	17.82	42.24	24.42	****	0.75
86	9	225	2.01	3.10	35.39	1.72	9	7	58	56	0.262	29.16	74.52	45.36	****	****
86	10	226	2.01	3.10	47.33	1.36	9	4	53	56	0.240	56.70	128.40	71.70	****	****
86	11	227	2.01	3.10	57.47	1.18	1	1	48	60	0.251	46.98	143.16	96.18	****	****
86	12	228	2.01	3.10	63.54	1.12	3	1	44	65	0.274	76.14	178.08	101.94	****	****
86	13	229	2.01	3.10	62.64	1.12	2	1	42	68	0.290	76.14	178.08	101.94	****	****
86	14	230	2.01	3.10	55.32	1.21	3	1	41	71	0.313	72.90	163.20	90.30	****	****
86	15	231	2.01	3.10	44.61	1.42	0	0	39	74	0.330	63.18	144.96	81.78	0.81	****
86	16	232	2.01	3.10	32.42	1.86	0	0	37	75	0.324	59.94	116.88	56.94	0.96	****
86	17	233	2.01	3.10	19.59	2.96	2	1	39	74	0.330	25.92	59.64	33.72	****	0.89
86	18	234	2.01	3.10	6.51	8.24	0	0	42	73	0.344	9.72	24.84	15.12	0.96	0.40
86	19	235	2.01	3.10	6.58	8.17	5	2	50	70	0.369	1.62	7.44	5.82	****	0.16
86	20	236	2.01	3.10	5.73	36.00	5	4	61	65	0.379	0.0	6.60	6.60	****	0.19
86	21	237	2.01	3.10	5.73	36.00	5	4	69	62	0.386	0.0	13.20	13.20	****	0.38
86	22	238	2.01	3.10	5.73	36.00	7	5	70	60	0.365	0.0	13.20	13.20	****	0.39
86	23	239	2.01	3.10	5.73	36.00	10	10	75	58	0.364	0.0	******	******	****	****
86	24	240	2.01	3.10	5.73	36.00	10	10	87	57	0.407	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
87	1	241	2.01	3.30	5.73	36.00	10	10	98	55	0.427	0.0	******	******	****	****
87	2	242	2.01	3.30	5.73	36.00	10	10	98	56	0.443	0.0	20.19	20.19	****	0.61
87	3	243	2.01	3.30	5.73	36.00	10	10	98	58	0.476	0.0	******	******	****	****
87	4	244	2.01	3.30	5.73	36.00	10	10	98	58	0.476	0.0	******	******	****	****
87	5	245	2.01	3.30	5.73	36.00	10	10	100	58	0.486	0.0	86.19	86.19	****	****
87	6	246	2.01	3.30	5.73	13.83	10	10	100	59	0.503	0.0	66.39	66.39	****	****
87	7	247	2.01	3.30	9.67	5.76	10	10	100	60	0.522	0.81	79.62	78.81	****	****
87	8	248	2.01	3.30	22.72	2.57	10	10	100	60	0.522	0.81	66.42	65.61	****	****
87	9	249	2.01	3.30	35.46	1.72	10	10	100	60	0.522	2.43	47.46	45.03	****	****
87	10	250	2.01	3.30	47.42	1.36	10	10	100	60	0.522	2.43	47.46	45.03	****	****
87	11	251	2.01	3.30	57.60	1.18	10	10	100	60	0.522	2.43	40.86	38.43	****	****
87	12	252	2.01	3.30	63.73	1.11	10	10	100	60	0.522	4.05	35.10	31.05	****	0.91
87	13	253	2.01	3.30	62.85	1.12	10	10	100	61	0.540	5.67	22.74	17.07	****	0.50
87	14	254	2.01	3.30	55.51	1.21	10	10	100	62	0.560	4.05	41.70	37.65	****	****
87	15	255	2.01	3.30	44.78	1.42	10	10	100	62	0.560	2.43	34.26	31.83	****	0.92
87	16	256	2.01	3.30	32.57	1.85	10	10	100	63	0.580	2.43	40.86	38.43	****	****
87	17	257	2.01	3.30	19.73	2.94	10	10	100	63	0.580	0.81	26.82	26.01	****	0.74
87	18	258	2.01	3.30	6.65	8.09	10	10	100	63	0.580	0.81	40.02	39.21	****	****
87	19	259	2.01	3.30	6.44	8.32	10	10	100	63	0.580	0.81	33.42	32.61	****	0.93
87	20	260	2.01	3.30	5.73	36.00	10	10	100	63	0.580	0.81	40.02	39.21	****	****
87	21	261	2.01	3.30	5.73	36.00	10	10	100	63	0.580	0.0	52.41	52.41	****	****
87	22	262	2.01	3.30	5.73	36.00	10	10	100	64	0.600	0.0	45.81	45.81	****	****
87	23	263	2.01	3.30	5.73	36.00	10	10	100	64	0.600	0.0	39.21	39.21	****	****
87	24	264	2.01	3.30	5.73	36.00	10	10	100	64	0.600	0.0	45.81	45.81	****	****
88	1	265	2.00	3.50	5.73	36.00	10	10	100	64	0.600	0.0	13.20	13.20	****	0.38
88	2	266	2.00	3.50	5.73	36.00	10	10	100	64	0.600	0.0	19.80	19.80	****	0.56
88	3	267	2.00	3.50	5.73	36.00	10	10	100	64	0.600	0.0	13.20	13.20	****	0.38
88	4	268	2.00	3.50	5.73	36.00	10	10	100	64	0.600	0.0	13.20	13.20	****	0.38
88	5	269	2.00	3.50	5.73	36.00	10	10	100	67	0.667	0.0	19.80	19.80	****	0.55
88	6	270	2.00	3.50	5.73	13.99	10	10	100	68	0.690	0.0	19.80	19.80	****	0.55
88	7	271	2.00	3.50	9.72	5.73	10	10	100	68	0.690	0.0	13.20	13.20	****	0.36
88	8	272	2.00	3.50	22.78	2.57	10	10	100	69	0.714	0.0	******	******	****	****
88	9	273	2.00	3.50	35.53	1.72	10	10	100	69	0.714	0.0	13.20	13.20	****	0.36
88	10	274	2.00	3.50	47.52	1.35	10	10	100	67	0.667	4.86	81.72	76.86	****	****
88	11	275	2.00	3.50	57.74	1.18	10	10	100	68	0.690	27.54	93.48	65.94	****	****
88	12	276	2.00	3.50	63.91	1.11	10	10	98	70	0.724	35.64	97.68	62.04	****	****
88	13	277	2.00	3.50	63.06	1.12	10	10	90	71	0.688	24.30	72.00	47.70	****	****
88	14	278	2.00	3.50	55.69	1.21	10	10	88	72	0.696	22.68	71.16	48.48	****	****
88	15	279	2.00	3.50	44.94	1.41	10	10	83	72	0.657	29.16	87.72	58.56	****	****
88	16	280	2.00	3.50	32.72	1.84	10	9	82	74	0.694	11.34	45.48	34.14	****	0.90

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
88	17	281	2.00	3.50	19.87	2.92	10	8	83	74	0.702	3.24	21.48	18.24	****	0.48
88	18	282	2.00	3.50	6.79	7.94	10	10	86	73	0.703	1.62	20.64	19.02	****	0.51
88	19	283	2.00	3.50	6.29	8.49	10	10	87	72	0.688	0.0	19.80	19.80	****	0.53
88	20	284	2.00	3.50	5.73	36.00	10	10	90	71	0.688	0.0	19.80	19.80	****	0.53
88	21	285	2.00	3.50	5.73	36.00	10	10	92	70	0.680	0.0	19.80	19.80	****	0.54
88	22	286	2.00	3.50	5.73	36.00	10	10	93	69	0.664	0.0	19.80	19.80	****	0.54
88	23	287	2.00	3.50	5.73	36.00	10	10	94	69	0.671	0.0	19.80	19.80	****	0.54
88	24	288	2.00	3.50	5.73	36.00	10	10	95	69	0.678	0.0	19.80	19.80	****	0.54
89	1	289	2.00	3.80	5.73	36.00	10	10	97	69	0.693	0.0	23.10	23.10	****	0.63
89	2	290	2.00	3.80	5.73	36.00	10	10	98	69	0.700	0.0	23.76	23.76	****	0.65
89	3	291	2.00	3.80	5.73	36.00	10	10	98	69	0.700	0.0	19.80	19.80	****	0.54
89	4	292	2.00	3.80	5.73	36.00	10	10	98	70	0.724	0.0	19.80	19.80	****	0.54
89	5	293	2.00	3.80	5.73	36.00	10	10	98	69	0.700	0.0	19.80	19.80	****	0.54
89	6	294	2.00	3.80	5.73	14.31	10	10	98	68	0.676	0.0	16.50	16.50	****	0.45
89	7	295	2.00	3.80	9.82	5.67	10	10	95	69	0.678	3.24	28.08	24.84	****	0.68
89	8	296	2.00	3.80	22.89	2.56	10	10	93	70	0.687	12.96	49.62	36.66	****	1.00
89	9	297	2.00	3.80	35.66	1.71	10	6	89	72	0.704	25.92	79.44	53.52	****	****
89	10	298	2.00	3.80	47.68	1.35	10	10	85	74	0.719	42.12	114.24	72.12	****	****
89	11	299	2.00	3.80	57.95	1.18	10	10	80	77	0.748	48.60	140.70	92.10	****	****
89	12	300	2.00	3.80	64.20	1.11	10	10	75	80	0.774	61.56	157.32	95.76	****	****
89	13	301	2.00	3.80	63.36	1.12	9	6	68	83	0.774	58.32	132.54	74.22	****	****
89	14	302	2.00	3.80	55.96	1.21	9	9	60	86	0.752	57.51	142.02	84.51	****	****
89	15	303	2.00	3.80	45.16	1.41	9	9	45	86	0.564	43.74	121.68	77.94	****	****
89	16	304	2.00	3.80	32.92	1.83	9	7	50	86	0.626	37.26	85.32	48.06	****	****
89	17	305	2.00	3.80	20.06	2.89	9	5	56	83	0.637	22.68	54.66	31.98	****	0.79
89	18	306	2.00	3.80	6.97	7.76	8	4	63	80	0.650	8.91	31.02	22.11	****	0.56
89	19	307	2.00	3.80	6.10	8.72	7	3	74	77	0.692	0.81	11.64	10.83	****	0.28
89	20	308	2.00	3.80	5.73	36.00	6	3	85	74	0.719	0.0	9.90	9.90	****	0.26
89	21	309	2.00	3.80	5.73	36.00	5	2	90	73	0.736	0.0	9.90	9.90	****	0.26
89	22	310	2.00	3.80	5.73	36.00	5	2	95	71	0.726	0.0	9.90	9.90	****	0.27
89	23	311	2.00	3.80	5.73	36.00	5	2	96	71	0.733	0.0	9.90	9.90	****	0.27
89	24	312	2.00	3.80	5.73	36.00	3	1	97	70	0.717	0.0	9.90	9.90	****	0.27
90	1	313	2.00	4.00	5.73	36.00	0	0	98	69	0.700	0.0	11.22	11.22	****	0.31
90	2	314	2.00	4.00	5.73	36.00	0	0	98	68	0.676	0.0	13.20	13.20	****	0.36
90	3	315	2.00	4.00	5.73	36.00	0	0	98	68	0.676	0.0	9.90	9.90	****	0.27
90	4	316	2.00	4.00	5.73	36.00	3	1	98	68	0.676	0.0	12.54	12.54	****	0.35
90	5	317	2.00	4.00	5.73	36.00	3	1	98	68	0.676	0.0	12.54	12.54	****	0.35
90	6	318	2.00	4.00	5.73	14.48	0	0	98	68	0.676	0.0	13.86	13.86	****	0.38
90	7	319	2.00	4.00	9.87	5.65	10	10	99	70	0.732	1.62	21.30	19.68	****	0.53
90	8	320	2.00	4.00	22.94	2.55	10	10	99	72	0.783	12.96	46.32	33.36	****	0.89

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
90	9	321	2.00	4.00	35.72	1.71	9	8	90	75	0.787	34.02	90.24	56.22	****	****
90	10	322	2.00	4.00	47.77	1.35	9	9	80	78	0.774	38.88	102.66	63.78	****	****
90	11	323	2.00	4.00	58.08	1.18	9	9	72	80	0.743	47.14	123.44	76.30	****	****
90	12	324	2.00	4.00	64.38	1.11	7	7	68	82	0.749	56.70	138.30	81.60	****	****
90	13	325	2.00	4.00	63.56	1.12	5	5	64	84	0.752	53.46	133.32	79.86	****	****
90	14	326	2.00	4.00	56.14	1.20	3	3	60	86	0.752	53.46	133.32	79.86	****	****
90	15	327	2.00	4.00	45.33	1.40	3	3	54	86	0.677	53.46	120.12	66.66	****	****
90	16	328	2.00	4.00	33.07	1.83	2	2	55	86	0.689	37.26	91.92	54.66	****	****
90	17	329	2.00	4.00	20.21	2.87	3	3	58	84	0.681	22.68	57.96	35.28	****	0.86
90	18	330	2.00	4.00	7.11	7.62	1	1	60	82	0.661	9.72	28.14	18.42	****	0.46
90	19	331	2.00	4.00	5.96	8.90	0	0	75	78	0.725	0.81	11.64	10.83	0.74	0.28
90	20	332	2.00	4.00	5.73	36.00	0	0	85	74	0.719	0.0	9.90	9.90	****	0.26
90	21	333	2.00	4.00	5.73	36.00	0	0	92	73	0.753	0.0	9.90	9.90	****	0.26
90	22	334	2.00	4.00	5.73	36.00	0	0	92	72	0.728	0.0	9.90	9.90	****	0.26
90	23	335	2.00	4.00	5.73	36.00	0	0	93	70	0.687	0.0	9.90	9.90	****	0.27
90	24	336	2.00	4.00	5.73	36.00	0	0	96	68	0.662	0.0	9.90	9.90	****	0.27
91	1	337	2.00	4.20	5.73	36.00	10	10	96	68	0.662	0.0	13.12	13.12	****	0.36
91	2	338	2.00	4.20	5.73	36.00	10	10	98	68	0.676	0.0	18.40	18.40	****	0.51
91	3	339	2.00	4.20	5.73	36.00	10	10	98	68	0.676	0.0	19.72	19.72	****	0.54
91	4	340	2.00	4.20	5.73	36.00	10	10	98	67	0.654	0.0	19.06	19.06	****	0.53
91	5	341	2.00	4.20	5.73	36.00	10	10	98	66	0.631	0.0	16.42	16.42	****	0.46
91	6	342	2.00	4.20	5.73	14.73	10	10	98	66	0.631	0.0	18.40	18.40	****	0.52
91	7	343	2.00	4.20	9.95	5.61	10	10	98	67	0.654	1.78	21.38	19.60	****	0.54
91	8	344	2.00	4.20	23.02	2.54	10	10	98	67	0.654	6.64	30.50	23.86	****	0.66
91	9	345	2.00	4.20	35.81	1.70	10	10	97	70	0.717	11.50	45.56	34.06	****	0.93
91	10	346	2.00	4.20	47.88	1.35	10	10	95	72	0.751	34.18	90.32	56.14	****	****
91	11	347	2.00	4.20	58.23	1.18	5	4	85	77	0.795	40.66	133.28	92.62	****	****
91	12	348	2.00	4.20	64.57	1.11	2	2	72	82	0.793	60.10	143.36	83.26	****	****
91	13	349	2.00	4.20	63.76	1.11	4	4	60	84	0.705	61.72	154.10	92.38	****	****
91	14	350	2.00	4.20	56.31	1.20	4	3	58	86	0.727	55.24	140.84	85.60	****	****
91	15	351	2.00	4.20	45.47	1.40	5	4	58	86	0.727	34.18	83.72	49.54	****	****
91	16	352	2.00	4.20	33.20	1.82	10	9	58	86	0.727	24.46	72.08	47.62	****	****
91	17	353	2.00	4.20	20.33	2.86	9	8	58	83	0.660	14.74	47.24	32.50	****	0.80
91	18	354	2.00	4.20	7.23	7.51	3	2	63	80	0.650	6.64	23.24	16.60	****	0.42
91	19	355	2.00	4.20	5.84	9.06	9	7	70	77	0.654	0.16	13.28	13.12	****	0.34
91	20	356	2.00	4.20	5.73	36.00	9	7	78	75	0.682	0.0	13.28	13.28	****	0.35
91	21	357	2.00	4.20	5.73	36.00	9	7	83	74	0.702	0.0	13.28	13.28	****	0.35
91	22	358	2.00	4.20	5.73	36.00	9	6	85	73	0.695	0.0	13.28	13.28	****	0.35
91	23	359	2.00	4.20	5.73	36.00	7	3	88	72	0.696	0.0	9.98	9.98	****	0.27
91	24	360	2.00	4.20	5.73	36.00	5	2	90	72	0.712	0.0	13.28	13.28	****	0.36

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
92	1	361	2.00	4.60	5.73	36.00	5	4	92	71	0.703	0.0	12.54	12.54	****	0.34
92	2	362	2.00	4.60	5.73	36.00	7	7	92	71	0.703	0.0	11.88	11.88	****	0.32
92	3	363	2.00	4.60	5.73	36.00	10	10	93	70	0.687	0.0	13.20	13.20	****	0.36
92	4	364	2.00	4.60	5.73	36.00	10	10	94	70	0.695	0.0	14.52	14.52	****	0.39
92	5	365	2.00	4.60	5.73	36.00	10	10	94	70	0.695	0.0	13.86	13.86	****	0.38
92	6	366	2.00	4.60	5.73	15.17	10	9	94	70	0.695	0.0	16.50	16.50	****	0.45
92	7	367	2.00	4.60	10.08	5.54	10	9	94	71	0.718	1.94	20.81	18.86	****	0.51
92	8	368	2.00	4.60	23.15	2.53	10	9	94	72	0.744	5.18	29.09	23.90	****	0.64
92	9	369	2.00	4.60	35.97	1.70	10	10	90	75	0.787	11.66	45.65	33.98	****	0.89
92	10	370	2.00	4.60	48.08	1.34	10	10	85	77	0.795	11.66	58.85	47.18	****	****
92	11	371	2.00	4.60	58.51	1.17	10	10	82	77	0.767	19.76	63.05	43.28	****	****
92	12	372	2.00	4.60	64.95	1.10	10	10	82	78	0.793	10.04	38.21	28.16	****	0.72
92	13	373	2.00	4.60	64.16	1.11	10	10	90	71	0.688	14.90	27.53	12.62	****	0.34
92	14	374	2.00	4.60	56.67	1.20	10	10	80	72	0.633	18.14	49.01	30.86	****	0.83
92	15	375	2.00	4.60	45.78	1.39	10	10	68	74	0.575	40.01	70.25	30.23	****	0.80
92	16	376	2.00	4.60	33.48	1.81	10	6	50	74	0.423	26.24	66.41	40.16	****	****
92	17	377	2.00	4.60	20.59	2.82	10	8	53	72	0.419	11.66	31.13	19.46	****	0.52
92	18	378	2.00	4.60	7.49	7.28	10	10	56	70	0.414	3.56	15.05	11.48	****	0.31
92	19	379	2.00	4.60	5.73	9.42	10	10	65	68	0.448	0.32	6.77	6.44	****	0.18
92	20	380	2.00	4.60	5.73	36.00	10	10	80	66	0.515	0.0	6.60	6.60	****	0.18
92	21	381	2.00	4.60	5.73	36.00	10	9	81	65	0.504	0.0	6.60	6.60	****	0.19
92	22	382	2.00	4.60	5.73	36.00	10	9	82	64	0.492	0.0	6.60	6.60	****	0.19
92	23	383	2.00	4.60	5.73	36.00	10	9	87	62	0.487	0.0	5.28	5.28	****	0.15
92	24	384	2.00	4.60	5.73	36.00	8	4	88	60	0.459	0.0	3.30	3.30	****	0.10
93	1	385	2.00	4.90	5.73	36.00	0	0	85	59	0.428	0.0	1.40	1.40	****	0.04
93	2	386	2.00	4.90	5.73	36.00	0	0	73	58	0.355	0.0	3.38	3.38	****	0.10
93	3	387	2.00	4.90	5.73	36.00	5	2	75	57	0.351	0.0	4.70	4.70	****	0.14
93	4	388	2.00	4.90	5.73	36.00	0	0	68	56	0.307	0.0	1.40	1.40	****	0.04
93	5	389	2.00	4.90	5.73	36.00	0	0	70	55	0.305	0.0	1.40	1.40	****	0.04
93	6	390	2.00	4.90	5.73	15.46	5	2	75	53	0.304	0.0	3.38	3.38	****	0.10
93	7	391	2.00	4.90	10.15	5.50	8	3	69	53	0.279	6.64	16.64	10.00	****	0.31
93	8	392	2.00	4.90	23.24	2.52	8	2	68	53	0.275	17.98	42.32	24.34	****	0.75
93	9	393	2.00	4.90	36.06	1.69	8	5	62	54	0.260	22.84	61.34	38.50	****	****
93	10	394	2.00	4.90	48.21	1.34	8	6	60	56	0.271	24.46	68.78	44.32	****	****
93	11	395	2.00	4.90	58.70	1.17	10	8	58	58	0.282	24.46	68.78	44.32	****	****
93	12	396	2.00	4.90	65.22	1.10	8	7	56	60	0.292	32.56	89.48	56.92	****	****
93	13	397	2.00	4.90	64.47	1.11	9	8	58	63	0.336	34.18	93.62	59.44	****	****
93	14	398	2.00	4.90	56.94	1.19	9	8	50	66	0.322	56.86	141.68	84.82	****	****
93	15	399	2.00	4.90	46.02	1.39	9	7	48	67	0.320	45.52	109.40	63.88	****	****
93	16	400	2.00	4.90	33.70	1.80	9	8	48	68	0.331	34.18	83.72	49.54	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
93	17	401	2.00	4.90	20.80	2.79	9	8	48	67	0.320	17.98	52.22	34.24	****	0.95
93	18	402	2.00	4.90	7.70	7.10	9	5	50	66	0.322	9.88	24.92	15.04	****	0.42
93	19	403	2.00	4.90	5.73	9.74	8	4	60	62	0.336	0.16	6.68	6.52	****	0.19
93	20	404	2.00	4.90	5.73	36.00	8	5	68	58	0.330	0.16	6.68	6.52	****	0.19
93	21	405	2.00	4.90	5.73	36.00	7	4	75	56	0.339	0.0	5.86	5.86	****	0.18
93	22	406	2.00	4.90	5.73	36.00	5	3	82	54	0.344	0.0	5.20	5.20	****	0.16
93	23	407	2.00	4.90	5.73	36.00	5	3	85	53	0.344	0.0	5.20	5.20	****	0.16
93	24	408	2.00	4.90	5.73	36.00	2	1	88	52	0.343	0.0	5.20	5.20	****	0.16
94	1	409	2.00	5.30	5.73	36.00	0	0	90	52	0.351	0.0	5.94	5.94	****	0.19
94	2	410	2.00	5.30	5.73	36.00	0	0	90	52	0.351	0.0	6.60	6.60	****	0.21
94	3	411	2.00	5.30	5.73	36.00	2	2	90	52	0.351	0.0	******	******	****	****
94	4	412	2.00	5.30	5.73	36.00	3	3	92	52	0.359	0.0	******	******	****	****
94	5	413	2.00	5.30	5.73	36.00	5	5	92	53	0.373	0.0	9.90	9.90	****	0.31
94	6	414	2.00	5.30	5.73	15.95	7	7	92	54	0.386	0.0	9.90	9.90	****	0.30
94	7	415	2.00	5.30	10.28	5.44	10	10	92	56	0.416	1.62	17.34	15.72	****	0.48
94	8	416	2.00	5.30	23.37	2.51	10	10	92	58	0.447	3.24	24.78	21.54	****	0.64
94	9	417	2.00	5.30	36.22	1.69	10	10	92	59	0.463	6.48	23.16	16.68	****	0.49
94	10	418	2.00	5.30	48.40	1.34	10	10	95	60	0.496	6.48	16.56	10.08	****	0.30
94	11	419	2.00	5.30	58.97	1.17	10	10	96	61	0.518	8.10	37.20	29.10	****	0.85
94	12	420	2.00	5.30	65.60	1.10	10	10	97	62	0.543	3.24	11.58	8.34	****	0.24
94	13	421	2.00	5.30	64.87	1.10	10	10	100	62	0.560	4.86	55.32	50.46	****	****
94	14	422	2.00	5.30	57.29	1.19	10	10	100	62	0.560	3.24	67.68	64.44	****	****
94	15	423	2.00	5.30	46.32	1.38	10	10	100	62	0.560	1.62	73.44	71.82	****	****
94	16	424	2.00	5.30	33.97	1.78	10	10	100	62	0.560	1.62	86.64	85.02	****	****
94	17	425	2.00	5.30	21.06	2.76	10	10	100	62	0.560	1.62	86.64	85.02	****	****
94	18	426	2.00	5.30	7.96	6.89	10	10	100	62	0.560	0.0	82.50	82.50	****	****
94	19	427	2.00	5.30	5.73	10.16	10	10	100	62	0.560	0.0	72.60	72.60	****	****
94	20	428	2.00	5.30	5.73	36.00	10	10	100	62	0.560	0.0	85.80	85.80	****	****
94	21	429	2.00	5.30	5.73	36.00	10	10	100	62	0.560	0.0	26.40	26.40	****	0.76
94	22	430	2.00	5.30	5.73	36.00	10	10	100	62	0.560	0.0	26.40	26.40	****	0.76
94	23	431	2.00	5.30	5.73	36.00	10	10	100	62	0.560	0.0	29.70	29.70	****	0.86
94	24	432	2.00	5.30	5.73	36.00	10	10	100	61	0.540	0.0	13.20	13.20	****	0.38
95	1	433	2.00	5.70	5.73	36.00	10	10	100	61	0.540	0.0	6.60	6.60	****	0.19
95	2	434	2.00	5.70	5.73	36.00	10	10	100	61	0.540	0.0	******	******	****	****
95	3	435	2.00	5.70	5.73	36.00	10	10	100	61	0.540	0.0	******	******	****	****
95	4	436	2.00	5.70	5.73	36.00	10	10	100	60	0.522	0.0	******	******	****	****
95	5	437	2.00	5.70	5.73	36.00	10	10	100	60	0.522	0.0	******	******	****	****
95	6	438	2.00	5.70	5.73	16.45	10	10	100	61	0.540	0.0	******	******	****	****
95	7	439	2.00	5.70	10.40	5.38	10	10	100	61	0.540	0.81	7.02	6.21	****	0.18
95	8	440	2.00	5.70	23.50	2.49	10	10	100	62	0.560	4.05	21.90	17.85	****	0.52

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
95	9	441	2.00	5.70	36.37	1.68	10	10	100	62	0.560	0.81	0.42	******	****	****
95	10	442	2.00	5.70	48.60	1.33	10	10	100	62	0.560	2.43	1.26	******	****	****
95	11	443	2.00	5.70	59.24	1.16	10	10	100	62	0.560	6.48	9.96	3.48	****	0.10
95	12	444	2.00	5.70	65.97	1.09	10	10	100	62	0.560	3.24	11.58	8.34	****	0.24
95	13	445	2.00	5.70	65.28	1.10	10	10	100	62	0.560	4.86	5.82	0.96	****	0.03
95	14	446	2.00	5.70	57.65	1.18	10	10	100	63	0.580	2.43	5.88	3.45	****	0.10
95	15	447	2.00	5.70	46.63	1.37	10	10	99	63	0.574	8.91	17.82	8.91	****	0.26
95	16	448	2.00	5.70	34.25	1.77	10	10	99	63	0.574	4.05	2.10	******	****	****
95	17	449	2.00	5.70	21.32	2.73	10	10	99	63	0.574	1.62	14.04	12.42	****	0.36
95	18	450	2.00	5.70	8.21	6.69	10	10	99	63	0.574	0.81	11.64	10.83	****	0.31
95	19	451	2.00	5.70	5.73	10.61	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
95	20	452	2.00	5.70	5.73	36.00	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
95	21	453	2.00	5.70	5.73	36.00	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
95	22	454	2.00	5.70	5.73	36.00	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
95	23	455	2.00	5.70	5.73	36.00	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
95	24	456	2.00	5.70	5.73	36.00	10	10	99	62	0.554	0.0	13.20	13.20	****	0.38
96	1	457	1.99	6.10	5.73	36.00	10	10	100	62	0.560	0.0	13.20	13.20	****	0.38
96	2	458	1.99	6.10	5.73	36.00	9	8	100	62	0.560	0.0	13.20	13.20	****	0.38
96	3	459	1.99	6.10	5.73	36.00	10	10	99	61	0.535	0.0	13.20	13.20	****	0.38
96	4	460	1.99	6.10	5.73	36.00	10	10	98	60	0.512	0.0	13.20	13.20	****	0.39
96	5	461	1.99	6.10	5.73	36.00	7	5	98	60	0.512	0.0	13.20	13.20	****	0.39
96	6	462	1.99	6.10	5.73	17.00	5	3	98	60	0.512	0.0	6.60	6.60	****	0.19
96	7	463	1.99	6.10	10.53	5.32	10	10	95	61	0.513	3.24	14.88	11.64	****	0.34
96	8	464	1.99	6.10	23.63	2.48	10	10	92	62	0.515	12.96	39.72	26.76	****	0.77
96	9	465	1.99	6.10	36.52	1.68	7	5	85	63	0.493	25.92	66.24	40.32	****	****
96	10	466	1.99	6.10	48.79	1.33	10	9	80	66	0.515	37.26	91.92	54.66	****	****
96	11	467	1.99	6.10	59.51	1.16	10	9	72	68	0.497	43.74	115.08	71.34	****	****
96	12	468	1.99	6.10	66.34	1.09	10	9	65	70	0.480	51.84	125.88	74.04	****	****
96	13	469	1.99	6.10	65.68	1.10	10	8	53	72	0.419	51.84	132.48	80.64	****	****
96	14	470	1.99	6.10	58.00	1.18	8	6	49	74	0.415	55.08	140.76	85.68	****	****
96	15	471	1.99	6.10	46.93	1.37	7	3	42	75	0.367	46.98	116.76	69.78	****	****
96	16	472	1.99	6.10	34.52	1.76	5	2	40	76	0.362	37.26	91.92	54.66	****	****
96	17	473	1.99	6.10	21.58	2.70	4	2	39	74	0.330	25.92	59.64	33.72	****	0.89
96	18	474	1.99	6.10	8.47	6.51	2	1	40	71	0.306	9.72	******	******	****	****
96	19	475	1.99	6.10	5.73	11.10	2	1	62	65	0.386	1.62	******	******	****	****
96	20	476	1.99	6.10	5.73	36.00	1	0	73	63	0.423	0.0	******	******	****	****
96	21	477	1.99	6.10	5.73	36.00	0	0	84	60	0.438	0.0	******	******	****	****
96	22	478	1.99	6.10	5.73	36.00	0	0	85	59	0.428	0.0	******	******	****	****
96	23	479	1.99	6.10	5.73	36.00	0	0	90	58	0.437	0.0	******	******	****	****
96	24	480	1.99	6.10	5.73	36.00	10	10	93	57	0.435	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
97	1	481	1.99	6.40	5.73	36.00	0	0	96	56	0.434	0.0	******	******	****	****
97	2	482	1.99	6.40	5.73	36.00	0	0	96	56	0.434	0.0	******	******	****	****
97	3	483	1.99	6.40	5.73	36.00	0	0	96	56	0.434	0.0	******	******	****	****
97	4	484	1.99	6.40	5.73	36.00	0	0	96	55	0.419	0.0	******	******	****	****
97	5	485	1.99	6.40	5.73	36.00	0	0	93	54	0.391	0.0	******	******	****	****
97	6	486	1.99	6.40	5.73	17.35	0	0	89	54	0.374	0.0	******	******	****	****
97	7	487	1.99	6.40	10.61	5.28	0	0	87	55	0.379	1.62	14.04	12.42	0.61	0.38
97	8	488	1.99	6.40	23.71	2.47	0	0	60	60	0.313	21.06	50.52	29.46	0.72	0.86
97	9	489	1.99	6.40	36.61	1.67	0	0	45	64	0.270	35.64	84.48	48.84	0.66	****
97	10	490	1.99	6.40	48.91	1.33	0	0	40	69	0.286	48.60	117.60	69.00	0.63	****
97	11	491	1.99	6.40	59.69	1.16	0	0	32	72	0.253	42.12	134.04	91.92	0.46	****
97	12	492	1.99	6.40	66.61	1.09	0	0	32	73	0.262	63.18	151.56	88.38	0.60	****
97	13	493	1.99	6.40	65.99	1.09	0	0	31	75	0.271	63.18	158.16	94.98	0.61	****
97	14	494	1.99	6.40	58.27	1.17	0	0	29	76	0.262	59.94	143.28	83.34	0.64	****
97	15	495	1.99	6.40	47.17	1.36	3	1	25	76	0.226	51.84	125.88	74.04	****	****
97	16	496	1.99	6.40	34.74	1.75	0	0	23	76	0.208	40.50	******	******	0.74	****
97	17	497	1.99	6.40	21.79	2.68	0	0	24	75	0.210	25.92	59.64	33.72	0.82	0.88
97	18	498	1.99	6.40	8.68	6.36	0	0	25	71	0.191	11.34	19.08	7.74	0.93	0.21
97	19	499	1.99	6.40	5.73	11.54	0	0	52	64	0.312	1.62	0.84	******	0.84	****
97	20	500	1.99	6.40	5.73	36.00	0	0	63	60	0.329	0.0	******	******	****	****
97	21	501	1.99	6.40	5.73	36.00	0	0	72	56	0.325	0.0	******	******	****	****
97	22	502	1.99	6.40	5.73	36.00	0	0	79	56	0.357	0.0	******	******	****	****
97	23	503	1.99	6.40	5.73	36.00	0	0	82	55	0.358	0.0	******	******	****	****
97	24	504	1.99	6.40	5.73	36.00	0	0	85	54	0.357	0.0	******	******	****	****
98	1	505	1.99	6.80	5.73	36.00	0	0	87	53	0.352	0.0	******	******	****	****
98	2	506	1.99	6.80	5.73	36.00	0	0	90	52	0.351	0.0	******	******	****	****
98	3	507	1.99	6.80	5.73	36.00	0	0	93	51	0.350	0.0	******	******	****	****
98	4	508	1.99	6.80	5.73	36.00	0	0	95	51	0.357	0.0	******	******	****	****
98	5	509	1.99	6.80	5.73	36.00	0	0	96	50	0.348	0.0	******	******	****	****
98	6	510	1.99	6.80	5.73	17.95	0	0	99	48	0.333	0.0	******	******	****	****
98	7	511	1.99	6.80	10.73	5.22	0	0	100	51	0.376	1.62	******	******	0.61	****
98	8	512	1.99	6.80	23.84	2.46	0	0	80	60	0.418	21.06	24.12	3.06	0.71	0.09
98	9	513	1.99	6.80	36.76	1.67	0	0	60	65	0.373	35.64	84.48	48.84	0.66	****
98	10	514	1.99	6.80	49.10	1.32	0	0	53	70	0.392	48.60	150.60	102.00	0.63	****
98	11	515	1.99	6.80	59.96	1.15	3	3	51	71	0.390	48.60	******	******	****	****
98	12	516	1.99	6.80	66.98	1.09	5	5	50	74	0.423	46.98	******	******	****	****
98	13	517	1.99	6.80	66.39	1.09	4	4	50	74	0.423	64.80	******	******	****	****
98	14	518	1.99	6.80	58.62	1.17	2	2	42	85	0.510	59.94	******	******	****	****
98	15	519	1.99	6.80	47.46	1.36	2	2	42	88	0.561	51.84	******	******	****	****
98	16	520	1.99	6.80	35.01	1.74	2	2	43	80	0.444	30.78	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
98	17	521	1.99	6.80	22.04	2.65	3	1	45	75	0.394	24.30	******	******	****	****
98	18	522	1.99	6.80	8.93	6.20	3	1	60	70	0.443	8.10	******	******	****	****
98	19	523	1.99	6.80	5.73	12.12	3	1	73	65	0.454	1.62	******	******	****	****
98	20	524	1.99	6.80	5.73	36.00	0	0	79	63	0.458	0.0	******	******	****	****
98	21	525	1.99	6.80	5.73	36.00	0	0	82	61	0.443	0.0	******	******	****	****
98	22	526	1.99	6.80	5.73	36.00	0	0	87	60	0.454	0.0	******	******	****	****
98	23	527	1.99	6.80	5.73	36.00	0	0	90	59	0.453	0.0	******	******	****	****
98	24	528	1.99	6.80	5.73	36.00	0	0	95	57	0.445	0.0	******	******	****	****
99	1	529	1.99	7.20	5.73	36.00	0	0	97	56	0.438	0.0	******	******	****	****
99	2	530	1.99	7.20	5.73	36.00	0	0	99	56	0.447	0.0	******	******	****	****
99	3	531	1.99	7.20	5.73	36.00	0	0	99	55	0.432	0.0	******	******	****	****
99	4	532	1.99	7.20	5.73	36.00	0	0	100	54	0.420	0.0	******	******	****	****
99	5	533	1.99	7.20	5.73	36.00	0	0	100	54	0.420	0.0	******	******	****	****
99	6	534	1.99	7.20	5.73	18.68	7	3	100	55	0.436	0.0	******	******	****	****
99	7	535	1.99	7.20	10.88	5.16	3	1	95	59	0.478	4.86	15.72	10.86	****	0.32
99	8	536	1.99	7.20	23.98	2.45	3	1	78	63	0.452	21.06	50.52	29.46	****	0.84
99	9	537	1.99	7.20	36.92	1.66	2	1	65	68	0.448	34.02	83.64	49.62	****	****
99	10	538	1.99	7.20	49.30	1.32	0	0	55	72	0.435	45.36	******	******	0.59	****
99	11	539	1.99	7.20	60.23	1.15	5	5	52	75	0.455	48.60	******	******	****	****
99	12	540	1.99	7.20	67.35	1.08	8	6	49	76	0.443	45.36	******	******	****	****
99	13	541	1.99	7.20	66.79	1.09	7	7	48	78	0.464	42.12	******	******	****	****
99	14	542	1.99	7.20	58.95	1.17	7	7	46	78	0.445	40.50	******	******	****	****
99	15	543	1.99	7.20	47.74	1.35	7	7	48	77	0.449	35.64	******	******	****	****
99	16	544	1.99	7.20	35.25	1.73	7	7	49	76	0.443	24.30	******	******	****	****
99	17	545	1.99	7.20	22.28	2.62	4	3	50	76	0.452	21.06	******	******	****	****
99	18	546	1.99	7.20	9.17	6.05	0	0	55	72	0.435	8.10	******	******	0.87	****
99	19	547	1.99	7.20	5.73	12.70	0	0	65	68	0.448	1.62	******	******	0.85	****
99	20	548	1.99	7.20	5.73	36.00	0	0	75	65	0.466	0.0	******	******	****	****
99	21	549	1.99	7.20	5.73	36.00	0	0	85	64	0.510	0.0	******	******	****	****
99	22	550	1.99	7.20	5.73	36.00	0	0	90	62	0.504	0.0	******	******	****	****
99	23	551	1.99	7.20	5.73	36.00	0	0	95	60	0.496	0.0	******	******	****	****
99	24	552	1.99	7.20	5.73	36.00	0	0	97	59	0.488	0.0	******	******	****	****
100	1	553	1.99	7.60	5.73	36.00	0	0	99	58	0.481	0.0	******	******	****	****
100	2	554	1.99	7.60	5.73	36.00	0	0	99	58	0.481	0.0	******	******	****	****
100	3	555	1.99	7.60	5.73	36.00	0	0	99	58	0.481	0.0	******	******	****	****
100	4	556	1.99	7.60	5.73	36.00	5	2	99	58	0.481	0.0	******	******	****	****
100	5	557	1.99	7.60	5.73	36.00	5	2	99	57	0.463	0.0	******	******	****	****
100	6	558	1.99	7.60	5.73	19.37	8	6	99	57	0.463	0.0	******	******	****	****
100	7	559	1.99	7.60	11.00	5.10	8	6	99	59	0.498	3.24	******	******	****	****
100	8	560	1.99	7.60	24.11	2.43	8	5	99	61	0.535	16.20	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
100	9	561	1.99	7.60	37.06	1.66	9	6	85	67	0.567	29.16	74.52	45.36	****	****
100	10	562	1.99	7.60	49.48	1.31	9	6	70	70	0.517	40.50	106.80	66.30	****	****
100	11	563	1.99	7.60	60.49	1.15	10	7	60	74	0.508	43.74	115.08	71.34	****	****
100	12	564	1.99	7.60	67.72	1.08	10	6	52	74	0.440	48.60	******	******	****	****
100	13	565	1.99	7.60	67.19	1.08	10	10	50	75	0.438	30.78	******	******	****	****
100	14	566	1.99	7.60	59.29	1.16	9	6	46	79	0.460	45.36	122.52	77.16	****	****
100	15	567	1.99	7.60	48.03	1.34	9	4	40	80	0.413	48.60	124.20	75.60	****	****
100	16	568	1.99	7.60	35.52	1.72	4	1	42	80	0.433	30.78	75.36	44.58	****	****
100	17	569	1.99	7.60	22.53	2.59	5	1	50	78	0.483	17.82	48.84	31.02	****	0.79
100	18	570	1.99	7.60	9.42	5.90	3	1	58	77	0.542	6.48	16.56	10.08	****	0.26
100	19	571	1.99	7.60	5.73	13.39	8	6	63	71	0.481	0.0	6.60	6.60	****	0.18
100	20	572	1.99	7.60	5.73	36.00	3	1	72	68	0.497	0.0	6.60	6.60	****	0.18
100	21	573	1.99	7.60	5.73	36.00	8	4	85	66	0.547	0.0	6.60	6.60	****	0.18
100	22	574	1.99	7.60	5.73	36.00	5	1	90	64	0.540	0.0	******	******	****	****
100	23	575	1.99	7.60	5.73	36.00	6	2	92	63	0.534	0.0	******	******	****	****
100	24	576	1.99	7.60	5.73	36.00	8	4	95	62	0.532	0.0	******	******	****	****
101	1	577	1.99	7.90	5.73	36.00	4	1	95	62	0.532	0.0	6.60	6.60	****	0.19
101	2	578	1.99	7.90	5.73	36.00	10	10	97	62	0.543	0.0	6.60	6.60	****	0.19
101	3	579	1.99	7.90	5.73	36.00	10	10	98	62	0.549	0.0	6.60	6.60	****	0.19
101	4	580	1.99	7.90	5.73	36.00	10	9	98	61	0.529	0.0	6.60	6.60	****	0.19
101	5	581	1.99	7.90	5.73	36.00	8	10	98	60	0.512	0.0	6.60	6.60	****	0.19
101	6	582	1.99	7.90	5.73	19.81	7	6	98	60	0.512	0.0	6.60	6.60	****	0.19
101	7	583	1.99	7.90	11.08	5.07	7	6	98	62	0.549	8.10	17.40	9.30	****	0.27
101	8	584	1.99	7.90	24.19	2.43	8	6	95	65	0.591	24.30	52.20	27.90	****	0.79
101	9	585	1.99	7.90	37.15	1.65	8	7	80	69	0.571	34.02	83.64	49.62	****	****
101	10	586	1.99	7.90	49.60	1.31	8	7	74	72	0.585	30.78	101.76	70.98	****	****
101	11	587	1.99	7.90	60.66	1.15	8	6	60	76	0.543	45.36	109.32	63.96	****	****
101	12	588	1.99	7.90	67.99	1.08	9	6	57	78	0.551	48.60	137.40	88.80	****	****
101	13	589	1.99	7.90	67.50	1.08	9	7	53	78	0.513	40.50	126.60	86.10	****	****
101	14	590	1.99	7.90	59.56	1.16	10	8	55	78	0.532	42.12	94.44	52.32	****	****
101	15	591	1.99	7.90	48.27	1.34	10	10	57	76	0.516	14.58	60.36	45.78	****	****
101	16	592	1.99	7.90	35.74	1.71	10	10	60	76	0.543	11.34	38.88	27.54	****	0.72
101	17	593	1.99	7.90	22.74	2.57	10	10	63	74	0.533	4.86	28.92	24.06	****	0.63
101	18	594	1.99	7.90	9.63	5.78	10	10	70	72	0.554	0.0	13.20	13.20	****	0.35
101	19	595	1.99	7.90	5.73	14.01	10	10	78	71	0.596	0.0	6.60	6.60	****	0.18
101	20	596	1.99	7.90	5.73	36.00	10	10	88	68	0.607	0.0	******	******	****	****
101	21	597	1.99	7.90	5.73	36.00	10	10	93	65	0.578	0.0	6.60	6.60	****	0.19
101	22	598	1.99	7.90	5.73	36.00	10	10	95	64	0.570	0.0	13.20	13.20	****	0.38
101	23	599	1.99	7.90	5.73	36.00	10	10	97	63	0.563	0.0	13.20	13.20	****	0.38
101	24	600	1.99	7.90	5.73	36.00	10	10	97	62	0.543	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
102	1	601	1.99	8.30	5.73	36.00	10	10	97	64	0.582	0.0	******	******	****	****
102	2	602	1.99	8.30	5.73	36.00	10	10	98	63	0.568	0.0	******	******	****	****
102	3	603	1.99	8.30	5.73	36.00	10	10	100	63	0.580	0.0	******	******	****	****
102	4	604	1.99	8.30	5.73	36.00	10	10	100	63	0.580	0.0	******	******	****	****
102	5	605	1.99	8.30	5.73	36.00	10	10	100	62	0.560	0.0	******	******	****	****
102	6	606	1.99	8.30	5.73	20.57	10	10	100	62	0.560	0.0	******	******	****	****
102	7	607	1.99	8.30	11.20	5.02	10	10	100	62	0.560	0.0	19.80	19.80	****	0.57
102	8	608	1.99	8.30	24.31	2.42	10	10	100	65	0.622	16.20	34.80	18.60	****	0.52
102	9	609	1.99	8.30	37.29	1.65	3	3	100	67	0.667	32.40	63.00	30.60	****	0.85
102	10	610	1.99	8.30	49.78	1.31	7	4	95	70	0.702	37.26	98.52	61.26	****	****
102	11	611	1.99	8.30	60.91	1.14	8	6	85	74	0.719	43.74	128.28	84.54	****	****
102	12	612	1.99	8.30	68.35	1.08	10	10	80	75	0.700	48.60	137.40	88.80	****	****
102	13	613	1.99	8.30	67.90	1.08	10	10	78	78	0.754	40.50	113.40	72.90	****	****
102	14	614	1.99	8.30	59.90	1.15	9	8	79	80	0.815	40.50	133.20	92.70	****	****
102	15	615	1.99	8.30	48.56	1.33	7	4	80	80	0.826	32.40	89.40	57.00	****	****
102	16	616	1.99	8.30	36.00	1.70	8	5	79	80	0.815	8.10	57.00	48.90	****	****
102	17	617	1.99	8.30	23.00	2.54	9	8	74	74	0.626	6.48	******	******	****	****
102	18	618	1.99	8.30	9.88	5.64	8	6	73	73	0.597	3.24	21.48	18.24	****	0.48
102	19	619	1.99	8.30	5.73	14.84	9	9	70	70	0.517	0.0	6.60	6.60	****	0.18
102	20	620	1.99	8.30	5.73	36.00	4	3	69	69	0.493	0.0	6.60	6.60	****	0.18
102	21	621	1.99	8.30	5.73	36.00	5	4	68	68	0.469	0.0	6.60	6.60	****	0.18
102	22	622	1.99	8.30	5.73	36.00	9	8	68	68	0.469	0.0	13.20	13.20	****	0.36
102	23	623	1.99	8.30	5.73	36.00	7	6	68	68	0.469	0.0	13.20	13.20	****	0.36
102	24	624	1.99	8.30	5.73	36.00	8	8	67	66	0.431	0.0	6.60	6.60	****	0.18
103	1	625	1.98	8.70	5.73	36.00	4	3	90	65	0.560	0.0	******	******	****	****
103	2	626	1.98	8.70	5.73	36.00	0	0	91	63	0.528	0.0	******	******	****	****
103	3	627	1.98	8.70	5.73	36.00	0	0	92	63	0.534	0.0	******	******	****	****
103	4	628	1.98	8.70	5.73	36.00	0	0	95	62	0.532	0.0	******	******	****	****
103	5	629	1.98	8.70	5.73	36.00	0	0	97	61	0.524	0.0	******	******	****	****
103	6	630	1.98	8.70	5.73	21.49	10	10	98	60	0.512	0.0	******	******	****	****
103	7	631	1.98	8.70	11.34	4.96	10	10	98	60	0.512	******	******	******	****	****
103	8	632	1.98	8.70	24.46	2.40	10	10	96	60	0.501	******	******	******	****	****
103	9	633	1.98	8.70	37.45	1.64	10	10	96	63	0.557	******	******	******	****	****
103	10	634	1.98	8.70	49.97	1.30	9	8	90	66	0.580	******	******	******	****	****
103	11	635	1.98	8.70	61.18	1.14	3	2	75	72	0.593	******	******	******	****	****
103	12	636	1.98	8.70	68.72	1.07	4	3	70	75	0.612	******	******	******	****	****
103	13	637	1.98	8.70	68.29	1.08	5	4	63	76	0.570	******	******	******	****	****
103	14	638	1.98	8.70	60.23	1.15	2	2	60	79	0.599	******	******	******	****	****
103	15	639	1.98	8.70	48.83	1.33	3	3	56	80	0.578	******	******	******	****	****
103	16	640	1.98	8.70	36.24	1.69	2	2	55	80	0.568	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
103	17	641	1.98	8.70	23.23	2.52	0	0	55	80	0.568	******	******	******	****	****
103	18	642	1.98	8.70	10.12	5.52	0	0	56	80	0.578	******	******	******	****	****
103	19	643	1.98	8.70	5.73	15.69	0	0	70	75	0.612	******	******	******	****	****
103	20	644	1.98	8.70	5.73	36.00	0	0	90	70	0.665	******	******	******	****	****
103	21	645	1.98	8.70	5.73	36.00	0	0	92	69	0.657	0.0	******	******	****	****
103	22	646	1.98	8.70	5.73	36.00	0	0	96	67	0.640	0.0	******	******	****	****
103	23	647	1.98	8.70	5.73	36.00	0	0	97	66	0.625	0.0	******	******	****	****
103	24	648	1.98	8.70	5.73	36.00	0	0	98	65	0.610	0.0	******	******	****	****
104	1	649	1.98	9.10	5.73	36.00	0	0	100	64	0.600	0.0	******	******	****	****
104	2	650	1.98	9.10	5.73	36.00	0	0	100	63	0.580	0.0	******	******	****	****
104	3	651	1.98	9.10	5.73	36.00	10	10	100	63	0.580	0.0	******	******	****	****
104	4	652	1.98	9.10	5.73	36.00	10	10	100	63	0.580	0.0	******	******	****	****
104	5	653	1.98	9.10	5.73	36.00	10	9	100	62	0.560	0.0	******	******	****	****
104	6	654	1.98	9.10	5.73	20.88	10	9	100	62	0.560	0.0	******	******	****	****
104	7	655	1.98	9.10	11.23	5.01	10	8	100	63	0.580	******	******	******	****	****
104	8	656	1.98	9.10	24.34	2.41	6	5	97	64	0.582	******	******	******	****	****
104	9	657	1.98	9.10	37.35	1.64	0	0	90	68	0.621	******	******	******	****	****
104	10	658	1.98	9.10	49.92	1.31	0	0	75	71	0.573	******	******	******	****	****
104	11	659	1.98	9.10	61.24	1.14	0	0	65	78	0.629	******	******	******	****	****
104	12	660	1.98	9.10	69.01	1.07	0	0	55	80	0.568	******	******	******	****	****
104	13	661	1.98	9.10	68.78	1.07	0	0	50	82	0.551	******	******	******	****	****
104	14	662	1.98	9.10	60.75	1.15	0	0	48	83	0.546	******	******	******	****	****
104	15	663	1.98	9.10	49.34	1.32	0	0	42	84	0.493	******	******	******	****	****
104	16	664	1.98	9.10	36.74	1.67	0	0	38	83	0.432	******	******	******	****	****
104	17	665	1.98	9.10	23.72	2.47	0	0	39	80	0.402	******	******	******	****	****
104	18	666	1.98	9.10	10.61	5.28	0	0	41	76	0.371	******	******	******	****	****
104	19	667	1.98	9.10	5.73	17.72	0	0	52	73	0.425	******	******	******	****	****
104	20	668	1.98	9.10	5.73	36.00	0	0	60	70	0.443	******	******	******	****	****
104	21	669	1.98	9.10	5.73	36.00	0	0	73	68	0.504	0.0	******	******	****	****
104	22	670	1.98	9.10	5.73	36.00	0	0	85	66	0.547	0.0	******	******	****	****
104	23	671	1.98	9.10	5.73	36.00	0	0	89	65	0.554	0.0	******	******	****	****
104	24	672	1.98	9.10	5.73	36.00	0	0	88	64	0.528	0.0	******	******	****	****
105	1	673	1.98	9.40	5.73	36.00	0	0	89	62	0.498	0.0	******	******	****	****
105	2	674	1.98	9.40	5.73	36.00	0	0	90	61	0.486	0.0	******	******	****	****
105	3	675	1.98	9.40	5.73	36.00	0	0	93	60	0.485	0.0	******	******	****	****
105	4	676	1.98	9.40	5.73	36.00	0	0	94	58	0.457	0.0	******	******	****	****
105	5	677	1.98	9.40	5.73	36.00	0	0	85	58	0.413	0.0	******	******	****	****
105	6	678	1.98	9.40	5.73	21.92	0	0	75	58	0.364	0.0	******	******	****	****
105	7	679	1.98	9.40	11.39	4.94	0	0	68	59	0.342	******	******	******	****	****
105	8	680	1.98	9.40	24.50	2.40	0	0	60	61	0.324	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
105	9	681	1.98	9.40	37.52	1.64	0	0	55	64	0.330	******	******	******	****	****
105	10	682	1.98	9.40	50.11	1.30	0	0	50	68	0.345	******	******	******	****	****
105	11	683	1.98	9.40	61.47	1.14	0	0	43	74	0.364	******	******	******	****	****
105	12	684	1.98	9.40	69.30	1.07	0	0	40	75	0.350	162.00	******	******	****	****
105	13	685	1.98	9.40	69.06	1.07	0	0	39	77	0.365	162.00	******	******	****	****
105	14	686	1.98	9.40	60.95	1.14	0	0	38	78	0.367	147.42	******	******	****	****
105	15	687	1.98	9.40	49.49	1.31	0	0	34	81	0.362	126.36	******	******	****	****
105	16	688	1.98	9.40	36.87	1.66	0	0	34	81	0.362	97.20	******	******	****	****
105	17	689	1.98	9.40	23.84	2.46	0	0	33	81	0.352	59.94	******	******	****	****
105	18	690	1.98	9.40	10.73	5.23	0	0	35	80	0.361	22.68	******	******	****	****
105	19	691	1.98	9.40	5.73	18.33	0	0	55	71	0.420	1.62	******	******	0.90	****
105	20	692	1.98	9.40	5.73	36.00	0	0	75	66	0.483	0.0	******	******	****	****
105	21	693	1.98	9.40	5.73	36.00	0	0	75	63	0.435	0.0	******	******	****	****
105	22	694	1.98	9.40	5.73	36.00	8	3	83	62	0.465	0.0	******	******	****	****
105	23	695	1.98	9.40	5.73	36.00	6	2	86	61	0.464	0.0	******	******	****	****
105	24	696	1.98	9.40	5.73	36.00	2	2	90	60	0.470	0.0	******	******	****	****
106	1	697	1.98	9.80	5.73	36.00	6	2	92	60	0.480	0.0	******	******	****	****
106	2	698	1.98	9.80	5.73	36.00	4	2	94	59	0.473	0.0	******	******	****	****
106	3	699	1.98	9.80	5.73	36.00	3	1	97	58	0.471	0.0	******	******	****	****
106	4	700	1.98	9.80	5.73	36.00	2	1	98	57	0.459	0.0	******	******	****	****
106	5	701	1.98	9.80	5.73	36.00	0	0	98	56	0.443	0.0	******	******	****	****
106	6	702	1.98	9.80	5.73	23.57	8	8	98	56	0.443	0.0	******	******	****	****
106	7	703	1.98	9.80	11.62	4.85	8	8	98	59	0.493	5.46	******	******	****	****
106	8	704	1.98	9.80	24.73	2.38	8	8	90	63	0.522	13.26	******	******	****	****
106	9	705	1.98	9.80	37.76	1.63	9	8	82	65	0.510	19.50	******	******	****	****
106	10	706	1.98	9.80	50.37	1.30	8	7	62	69	0.443	42.12	******	******	****	****
106	11	707	1.98	9.80	61.79	1.13	5	3	53	75	0.464	65.52	******	******	****	****
106	12	708	1.98	9.80	69.69	1.07	3	2	47	77	0.439	76.44	******	******	****	****
106	13	709	1.98	9.80	69.42	1.07	3	2	42	80	0.433	74.10	******	******	****	****
106	14	710	1.98	9.80	61.20	1.14	0	0	42	81	0.448	69.42	******	******	0.70	****
106	15	711	1.98	9.80	49.67	1.31	0	0	40	82	0.441	57.72	******	******	0.71	****
106	16	712	1.98	9.80	37.02	1.66	0	0	41	82	0.452	42.12	171.60	129.48	0.73	****
106	17	713	1.98	9.80	23.98	2.45	0	0	41	82	0.452	26.52	118.80	92.28	0.78	****
106	18	714	1.98	9.80	10.87	5.16	4	2	48	80	0.495	9.36	79.20	69.84	****	****
106	19	715	1.98	9.80	5.73	19.10	0	0	60	74	0.508	0.0	52.80	52.80	****	****
106	20	716	1.98	9.80	5.73	36.00	8	7	70	70	0.517	0.0	60.18	60.18	****	****
106	21	717	1.98	9.80	5.73	36.00	5	4	70	68	0.483	0.0	60.18	60.18	****	****
106	22	718	1.98	9.80	5.73	36.00	3	2	70	66	0.451	0.0	53.58	53.58	****	****
106	23	719	1.98	9.80	5.73	36.00	3	2	75	64	0.450	0.0	53.58	53.58	****	****
106	24	720	1.98	9.80	5.73	36.00	1	1	82	63	0.476	0.0	53.58	53.58	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
107	1	721	1.98	10.20	5.73	36.00	3	1	90	62	0.504	0.0	53.58	53.58	****	****
107	2	722	1.98	10.20	5.73	36.00	3	1	94	61	0.508	0.0	53.58	53.58	****	****
107	3	723	1.98	10.20	5.73	36.00	3	1	96	60	0.501	0.0	53.58	53.58	****	****
107	4	724	1.98	10.20	5.73	36.00	3	1	98	59	0.493	0.0	53.58	53.58	****	****
107	5	725	1.98	10.20	5.73	36.00	3	1	98	59	0.493	0.0	53.58	53.58	****	****
107	6	726	1.98	10.20	5.73	25.24	3	1	98	58	0.476	0.0	52.80	52.80	****	****
107	7	727	1.98	10.20	11.83	4.77	2	1	98	60	0.512	9.36	79.20	69.84	****	****
107	8	728	1.98	10.20	24.93	2.36	2	1	90	64	0.540	24.96	125.40	100.44	****	****
107	9	729	1.98	10.20	37.97	1.62	0	0	77	69	0.550	43.68	184.80	141.12	0.73	****
107	10	730	1.98	10.20	50.62	1.29	0	0	70	72	0.554	58.50	224.40	165.90	0.71	****
107	11	731	1.98	10.20	62.10	1.13	0	0	60	75	0.525	64.74	250.80	186.06	0.65	****
107	12	732	1.98	10.20	70.08	1.06	0	0	56	79	0.559	69.42	257.40	187.98	0.64	****
107	13	733	1.98	10.20	69.78	1.06	7	3	53	80	0.547	69.42	257.40	187.98	****	****
107	14	734	1.98	10.20	61.47	1.14	6	2	49	82	0.540	69.42	250.80	181.38	****	****
107	15	735	1.98	10.20	49.87	1.31	7	5	45	84	0.529	52.26	217.80	165.54	****	****
107	16	736	1.98	10.20	37.19	1.65	8	3	45	84	0.529	46.02	171.60	125.58	****	****
107	17	737	1.98	10.20	24.14	2.43	8	4	46	83	0.523	22.62	118.80	96.18	****	****
107	18	738	1.98	10.20	11.04	5.09	8	1	50	82	0.551	7.80	79.20	71.40	****	****
107	19	739	1.98	10.20	5.73	20.05	9	3	65	75	0.569	0.0	52.80	52.80	****	****
107	20	740	1.98	10.20	5.73	36.00	8	2	71	73	0.581	0.0	53.58	53.58	****	****
107	21	741	1.98	10.20	5.73	36.00	0	0	74	69	0.528	0.0	53.58	53.58	****	****
107	22	742	1.98	10.20	5.73	36.00	0	0	80	69	0.571	0.0	53.58	53.58	****	****
107	23	743	1.98	10.20	5.73	36.00	6	2	88	67	0.587	0.0	53.58	53.58	****	****
107	24	744	1.98	10.20	5.73	36.00	7	2	94	66	0.605	0.0	53.58	53.58	****	****
108	1	745	1.98	10.60	5.73	36.00	7	2	96	64	0.576	0.0	27.18	27.18	****	0.77
108	2	746	1.98	10.60	5.73	36.00	9	4	98	64	0.588	0.0	27.18	27.18	****	0.77
108	3	747	1.98	10.60	5.73	36.00	10	7	98	63	0.568	0.0	27.18	27.18	****	0.78
108	4	748	1.98	10.60	5.73	36.00	10	8	98	63	0.568	0.0	27.18	27.18	****	0.78
108	5	749	1.98	10.60	5.73	36.00	10	8	99	62	0.554	0.0	27.18	27.18	****	0.78
108	6	750	1.98	10.60	5.73	26.51	9	7	99	61	0.535	0.0	29.70	29.70	****	0.86
108	7	751	1.98	10.60	11.97	4.72	9	4	99	62	0.554	7.80	39.60	31.80	****	0.92
108	8	752	1.98	10.60	25.07	2.35	10	5	92	65	0.572	25.74	62.70	36.96	****	****
108	9	753	1.98	10.60	38.12	1.62	10	9	88	70	0.650	38.22	82.50	44.28	****	****
108	10	754	1.98	10.60	50.80	1.29	10	10	81	72	0.641	46.02	95.70	49.68	****	****
108	11	755	1.98	10.60	62.35	1.13	10	3	70	76	0.633	62.40	122.10	59.70	****	****
108	12	756	1.98	10.60	70.44	1.06	8	3	69	79	0.689	69.42	125.40	55.98	****	****
108	13	757	1.98	10.60	70.18	1.06	7	3	63	80	0.650	69.42	125.40	55.98	****	****
108	14	758	1.98	10.60	61.78	1.13	7	3	60	82	0.661	63.18	108.90	45.72	****	****
108	15	759	1.98	10.60	50.14	1.30	7	3	56	83	0.637	40.56	89.10	48.54	****	****
108	16	760	1.98	10.60	37.43	1.64	6	2	55	84	0.646	******	85.80	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
108	17	761	1.98	10.60	24.37	2.41	2	2	53	84	0.623	22.62	59.40	36.78	****	0.90
108	18	762	1.98	10.60	11.27	4.99	4	2	60	83	0.683	6.24	36.30	30.06	****	0.74
108	19	763	1.98	10.60	5.73	21.48	4	2	63	78	0.609	0.0	26.40	26.40	****	0.68
108	20	764	1.98	10.60	5.73	36.00	0	0	68	75	0.595	0.0	27.18	27.18	****	0.71
108	21	765	1.98	10.60	5.73	36.00	0	0	73	73	0.597	0.0	27.18	27.18	****	0.72
108	22	766	1.98	10.60	5.73	36.00	0	0	80	70	0.591	0.0	27.18	27.18	****	0.74
108	23	767	1.98	10.60	5.73	36.00	0	0	89	68	0.614	0.0	27.18	27.18	****	0.75
108	24	768	1.98	10.60	5.73	36.00	0	0	93	67	0.620	0.0	27.18	27.18	****	0.76
109	1	769	1.98	10.90	5.73	36.00	0	0	95	65	0.591	0.0	27.18	27.18	****	0.77
109	2	770	1.98	10.90	5.73	36.00	0	0	96	64	0.576	0.0	27.18	27.18	****	0.77
109	3	771	1.98	10.90	5.73	36.00	0	0	99	64	0.594	0.0	27.18	27.18	****	0.77
109	4	772	1.98	10.90	5.73	36.00	3	1	100	63	0.580	0.0	27.18	27.18	****	0.78
109	5	773	1.98	10.90	5.73	36.00	5	2	100	63	0.580	0.0	27.18	27.18	****	0.78
109	6	774	1.98	10.90	5.73	27.46	3	1	100	62	0.560	0.0	29.70	29.70	****	0.86
109	7	775	1.98	10.90	12.07	4.68	3	1	100	63	0.580	8.58	42.90	34.32	****	0.98
109	8	776	1.98	10.90	25.17	2.34	5	5	99	67	0.660	26.52	62.70	36.18	****	****
109	9	777	1.98	10.90	38.23	1.61	5	5	88	71	0.672	45.24	85.80	40.56	****	****
109	10	778	1.98	10.90	50.92	1.29	4	4	70	74	0.592	59.28	112.20	52.92	****	****
109	11	779	1.98	10.90	62.52	1.13	5	1	62	78	0.600	69.42	128.70	59.28	****	****
109	12	780	1.98	10.90	70.71	1.06	4	1	54	82	0.595	74.88	132.00	57.12	****	****
109	13	781	1.98	10.90	70.47	1.06	6	2	51	84	0.599	74.10	132.00	57.90	****	****
109	14	782	1.98	10.90	62.02	1.13	6	1	50	86	0.626	******	125.40	******	****	****
109	15	783	1.98	10.90	50.34	1.30	6	1	46	87	0.595	******	102.30	******	****	****
109	16	784	1.98	10.90	37.61	1.63	6	1	46	87	0.595	******	79.20	******	****	****
109	17	785	1.98	10.90	24.55	2.39	1	1	58	85	0.704	28.08	66.00	37.92	****	0.92
109	18	786	1.98	10.90	11.45	4.92	0	0	69	80	0.712	10.92	42.90	31.98	0.86	0.81
109	19	787	1.98	10.90	5.73	22.72	0	0	76	75	0.665	******	29.70	******	****	****
109	20	788	1.98	10.90	5.73	36.00	0	0	82	73	0.671	0.0	30.48	30.48	****	0.81
109	21	789	1.98	10.90	5.73	36.00	0	0	86	72	0.680	0.0	30.48	30.48	****	0.82
109	22	790	1.98	10.90	5.73	36.00	0	0	86	71	0.657	0.0	30.48	30.48	****	0.82
109	23	791	1.98	10.90	5.73	36.00	0	0	89	70	0.658	0.0	27.18	27.18	****	0.74
109	24	792	1.98	10.90	5.73	36.00	0	0	91	69	0.650	0.0	27.18	27.18	****	0.74
110	1	793	1.98	11.30	5.73	36.00	0	0	95	69	0.678	0.0	27.18	27.18	****	0.74
110	2	794	1.98	11.30	5.73	36.00	0	0	95	68	0.655	0.0	30.48	30.48	****	0.84
110	3	795	1.98	11.30	5.73	36.00	0	0	93	68	0.642	0.0	30.48	30.48	****	0.84
110	4	796	1.98	11.30	5.73	36.00	4	4	94	69	0.671	0.0	30.48	30.48	****	0.83
110	5	797	1.98	11.30	5.73	36.00	4	4	96	69	0.685	0.0	30.48	30.48	****	0.83
110	6	798	1.98	11.30	5.73	28.68	4	4	97	68	0.669	0.0	33.00	33.00	****	0.91
110	7	799	1.98	11.30	12.19	4.64	7	6	95	69	0.678	5.46	42.90	37.44	****	****
110	8	800	1.98	11.30	25.28	2.33	10	10	93	70	0.687	9.36	49.50	40.14	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
110	9	801	1.98	11.30	38.35	1.61	10	10	92	74	0.778	15.60	56.10	40.50	****	****
110	10	802	1.98	11.30	51.08	1.28	10	10	90	75	0.787	7.80	49.50	41.70	****	****
110	11	803	1.98	11.30	62.75	1.12	10	10	90	76	0.814	8.58	******	******	****	****
110	12	804	1.98	11.30	71.06	1.06	10	10	90	77	0.841	10.92	42.90	31.98	****	0.82
110	13	805	1.98	11.30	70.87	1.06	10	10	89	77	0.832	9.36	******	******	****	****
110	14	806	1.98	11.30	62.35	1.13	10	10	90	77	0.841	13.26	******	******	****	****
110	15	807	1.98	11.30	50.62	1.29	10	10	85	80	0.877	27.30	69.30	42.00	****	****
110	16	808	1.98	11.30	37.87	1.63	10	10	85	77	0.795	******	49.50	******	****	****
110	17	809	1.98	11.30	24.80	2.37	10	9	88	77	0.823	10.14	46.20	36.06	****	0.93
110	18	810	1.98	11.30	11.70	4.82	9	6	88	76	0.796	3.90	42.90	39.00	****	****
110	19	811	1.98	11.30	5.73	24.64	10	10	94	75	0.822	0.0	******	******	****	****
110	20	812	1.98	11.30	5.73	36.00	10	8	96	74	0.812	0.0	37.08	37.08	****	0.98
110	21	813	1.98	11.30	5.73	36.00	10	9	96	74	0.812	0.0	37.08	37.08	****	0.98
110	22	814	1.98	11.30	5.73	36.00	10	9	97	73	0.793	0.0	37.08	37.08	****	0.98
110	23	815	1.98	11.30	5.73	36.00	2	2	98	72	0.775	0.0	37.08	37.08	****	0.99
110	24	816	1.98	11.30	5.73	36.00	10	10	98	74	0.829	0.0	40.38	40.38	****	****
111	1	817	1.97	11.60	5.73	36.00	10	10	98	74	0.829	0.0	40.38	40.38	****	****
111	2	818	1.97	11.60	5.73	36.00	10	10	98	74	0.829	0.0	40.38	40.38	****	****
111	3	819	1.97	11.60	5.73	36.00	10	10	98	74	0.829	0.0	40.38	40.38	****	****
111	4	820	1.97	11.60	5.73	36.00	10	10	98	74	0.829	0.0	37.08	37.08	****	0.98
111	5	821	1.97	11.60	5.73	36.00	8	8	98	73	0.802	0.0	******	******	****	****
111	6	822	1.97	11.60	5.73	29.70	10	10	99	73	0.810	0.0	******	******	****	****
111	7	823	1.97	11.60	12.28	4.60	9	8	99	74	0.838	7.02	46.20	39.18	****	****
111	8	824	1.97	11.60	25.37	2.32	10	9	89	76	0.805	14.82	52.80	37.98	****	0.99
111	9	825	1.97	11.60	38.45	1.60	7	7	86	78	0.832	******	******	******	****	****
111	10	826	1.97	11.60	51.20	1.28	7	7	80	82	0.882	******	******	******	****	****
111	11	827	1.97	11.60	62.92	1.12	7	6	72	84	0.846	******	******	******	****	****
111	12	828	1.97	11.60	71.33	1.05	7	7	65	86	0.814	******	******	******	****	****
111	13	829	1.97	11.60	71.17	1.06	7	7	62	86	0.777	******	******	******	****	****
111	14	830	1.97	11.60	62.59	1.13	7	7	58	88	0.774	******	******	******	****	****
111	15	831	1.97	11.60	50.82	1.29	6	6	60	87	0.776	******	95.70	******	****	****
111	16	832	1.97	11.60	38.05	1.62	6	6	60	86	0.752	46.02	89.10	43.08	****	****
111	17	833	1.97	11.60	24.98	2.36	3	3	62	84	0.728	27.30	66.00	38.70	****	0.95
111	18	834	1.97	11.60	11.89	4.75	2	2	70	81	0.746	9.36	39.60	30.24	****	0.76
111	19	835	1.97	11.60	5.73	26.18	1	1	80	78	0.774	0.0	29.70	29.70	****	0.76
111	20	836	1.97	11.60	5.73	36.00	0	0	88	76	0.796	0.0	30.48	30.48	****	0.79
111	21	837	1.97	11.60	5.73	36.00	0	0	92	74	0.778	0.0	30.48	30.48	****	0.80
111	22	838	1.97	11.60	5.73	36.00	0	0	95	73	0.777	0.0	30.48	30.48	****	0.81
111	23	839	1.97	11.60	5.73	36.00	0	0	97	72	0.767	0.0	30.48	30.48	****	0.82
111	24	840	1.97	11.60	5.73	36.00	0	0	98	71	0.749	0.0	30.48	30.48	****	0.82

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
112	1	841	1.97	12.00	5.73	36.00	0	0	99	70	0.732	0.0	31.26	31.26	****	0.85
112	2	842	1.97	12.00	5.73	36.00	0	0	99	69	0.707	0.0	31.26	31.26	****	0.86
112	3	843	1.97	12.00	5.73	36.00	0	0	99	68	0.683	0.0	31.26	31.26	****	0.86
112	4	844	1.97	12.00	5.73	36.00	0	0	99	68	0.683	0.0	31.26	31.26	****	0.86
112	5	845	1.97	12.00	5.73	36.00	0	0	99	68	0.683	0.0	34.56	34.56	****	0.95
112	6	846	1.97	12.00	5.73	31.30	0	0	99	68	0.683	0.0	33.00	33.00	****	0.91
112	7	847	1.97	12.00	12.42	4.55	10	2	100	72	0.791	7.80	49.50	41.70	****	****
112	8	848	1.97	12.00	25.51	2.31	0	0	92	76	0.833	24.96	69.30	44.34	0.73	****
112	9	849	1.97	12.00	38.59	1.60	0	0	80	81	0.853	41.34	95.70	54.36	0.70	****
112	10	850	1.97	12.00	51.37	1.28	0	0	72	85	0.874	54.60	115.50	60.90	0.66	****
112	11	851	1.97	12.00	63.16	1.12	4	3	63	86	0.789	56.94	125.40	68.46	****	****
112	12	852	1.97	12.00	71.69	1.05	5	5	60	90	0.853	51.48	112.20	60.72	****	****
112	13	853	1.97	12.00	71.56	1.05	7	7	54	91	0.792	******	141.90	******	****	****
112	14	854	1.97	12.00	62.90	1.12	7	7	50	92	0.757	******	118.80	******	****	****
112	15	855	1.97	12.00	51.07	1.28	4	4	45	92	0.681	******	115.50	******	****	****
112	16	856	1.97	12.00	38.28	1.61	2	2	45	92	0.681	******	99.00	******	****	****
112	17	857	1.97	12.00	25.20	2.34	1	1	47	90	0.668	******	66.00	******	****	****
112	18	858	1.97	12.00	12.11	4.66	1	1	52	85	0.631	******	39.60	******	****	****
112	19	859	1.97	12.00	5.73	28.30	1	1	60	82	0.661	******	29.70	******	****	****
112	20	860	1.97	12.00	5.73	36.00	1	1	62	80	0.640	******	29.70	******	****	****
112	21	861	1.97	12.00	5.73	36.00	0	0	72	78	0.696	0.0	******	******	****	****
112	22	862	1.97	12.00	5.73	36.00	0	0	72	77	0.673	0.0	******	******	****	****
112	23	863	1.97	12.00	5.73	36.00	0	0	77	75	0.674	0.0	******	******	****	****
112	24	864	1.97	12.00	5.73	36.00	0	0	81	74	0.685	0.0	******	******	****	****
113	1	865	1.97	12.30	5.73	36.00	0	0	90	72	0.712	0.0	******	******	****	****
113	2	866	1.97	12.30	5.73	36.00	0	0	95	70	0.702	0.0	******	******	****	****
113	3	867	1.97	12.30	5.73	36.00	0	0	97	69	0.693	0.0	******	******	****	****
113	4	868	1.97	12.30	5.73	36.00	0	0	98	68	0.676	0.0	******	******	****	****
113	5	869	1.97	12.30	5.73	36.00	0	0	98	68	0.676	0.0	******	******	****	****
113	6	870	1.97	12.30	5.73	32.42	2	2	99	68	0.683	0.0	******	******	****	****
113	7	871	1.97	12.30	12.52	4.52	0	0	99	70	0.732	******	49.50	******	****	****
113	8	872	1.97	12.30	25.60	2.30	0	0	90	74	0.761	******	72.60	******	****	****
113	9	873	1.97	12.30	38.69	1.60	0	0	83	76	0.751	******	79.20	******	****	****
113	10	874	1.97	12.30	51.48	1.28	7	7	70	80	0.722	******	102.30	******	****	****
113	11	875	1.97	12.30	63.32	1.12	8	7	60	84	0.705	******	122.10	******	****	****
113	12	876	1.97	12.30	71.95	1.05	4	3	52	86	0.652	78.78	141.90	63.12	****	****
113	13	877	1.97	12.30	71.86	1.05	3	3	46	88	0.614	73.32	138.60	65.28	****	****
113	14	878	1.97	12.30	63.14	1.12	3	3	43	90	0.611	72.54	132.00	59.46	****	****
113	15	879	1.97	12.30	51.27	1.28	3	2	42	90	0.597	59.28	112.20	52.92	****	****
113	16	880	1.97	12.30	38.46	1.60	3	2	41	90	0.583	46.80	125.40	78.60	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
113	17	881	1.97	12.30	25.38	2.32	3	1	43	90	0.611	27.30	69.30	42.00	****	0.98
113	18	882	1.97	12.30	12.29	4.60	2	1	49	88	0.654	8.58	39.60	31.02	****	0.74
113	19	883	1.97	12.30	5.73	30.16	2	1	54	79	0.539	0.0	29.70	29.70	****	0.75
113	20	884	1.97	12.30	5.73	36.00	4	1	61	76	0.552	0.0	27.18	27.18	****	0.71
113	21	885	1.97	12.30	5.73	36.00	0	0	70	75	0.612	0.0	27.18	27.18	****	0.71
113	22	886	1.97	12.30	5.73	36.00	0	0	83	72	0.657	0.0	27.18	27.18	****	0.73
113	23	887	1.97	12.30	5.73	36.00	0	0	86	70	0.636	0.0	27.18	27.18	****	0.74
113	24	888	1.97	12.30	5.73	36.00	0	0	91	69	0.650	0.0	27.18	27.18	****	0.74
114	1	889	1.97	12.70	5.73	36.00	0	0	95	69	0.678	0.0	27.18	27.18	****	0.74
114	2	890	1.97	12.70	5.73	36.00	0	0	96	68	0.662	0.0	30.48	30.48	****	0.84
114	3	891	1.97	12.70	5.73	36.00	0	0	95	68	0.655	0.0	30.48	30.48	****	0.84
114	4	892	1.97	12.70	5.73	36.00	8	2	95	68	0.655	0.0	33.78	33.78	****	0.93
114	5	893	1.97	12.70	5.73	36.00	9	4	95	68	0.655	0.0	33.78	33.78	****	0.93
114	6	894	1.97	12.70	5.73	34.13	9	4	95	68	0.655	0.0	33.00	33.00	****	0.91
114	7	895	1.97	12.70	12.66	4.47	9	5	95	70	0.702	7.02	42.90	35.88	****	0.97
114	8	896	1.97	12.70	25.73	2.29	10	10	92	72	0.728	13.26	52.80	39.54	****	****
114	9	897	1.97	12.70	38.82	1.59	10	10	89	74	0.753	24.18	66.00	41.82	****	****
114	10	898	1.97	12.70	51.65	1.27	7	5	72	79	0.719	******	105.60	******	****	****
114	11	899	1.97	12.70	63.55	1.12	8	5	61	82	0.672	******	115.50	******	****	****
114	12	900	1.97	12.70	72.30	1.05	8	6	60	82	0.661	******	99.00	******	****	****
114	13	901	1.97	12.70	72.25	1.05	9	7	59	83	0.671	******	102.30	******	****	****
114	14	902	1.97	12.70	63.44	1.12	9	7	56	83	0.637	51.48	99.00	47.52	****	****
114	15	903	1.97	12.70	51.52	1.28	8	7	58	82	0.639	36.66	79.20	42.54	****	****
114	16	904	1.97	12.70	38.69	1.60	10	10	61	82	0.672	24.18	62.70	38.52	****	0.96
114	17	905	1.97	12.70	25.60	2.30	10	9	59	82	0.650	28.08	59.40	31.32	****	0.78
114	18	906	1.97	12.70	12.52	4.52	10	9	60	82	0.661	11.70	46.20	34.50	****	0.86
114	19	907	1.97	12.70	5.73	32.70	8	5	64	76	0.579	0.0	26.40	26.40	****	0.69
114	20	908	1.97	12.70	5.73	36.00	8	5	73	75	0.639	0.0	27.18	27.18	****	0.71
114	21	909	1.97	12.70	5.73	36.00	7	4	85	72	0.672	0.0	27.18	27.18	****	0.73
114	22	910	1.97	12.70	5.73	36.00	10	9	92	70	0.680	0.0	27.18	27.18	****	0.74
114	23	911	1.97	12.70	5.73	36.00	10	9	93	70	0.687	0.0	27.18	27.18	****	0.74
114	24	912	1.97	12.70	5.73	36.00	1	0	96	68	0.662	0.0	27.18	27.18	****	0.75
115	1	913	1.97	13.00	5.73	36.00	0	0	98	66	0.631	0.0	30.48	30.48	****	0.85
115	2	914	1.97	13.00	5.73	36.00	0	0	99	64	0.594	0.0	30.48	30.48	****	0.87
115	3	915	1.97	13.00	5.73	36.00	3	1	99	64	0.594	0.0	33.78	33.78	****	0.96
115	4	916	1.97	13.00	5.73	36.00	10	7	100	64	0.600	0.0	33.78	33.78	****	0.96
115	5	917	1.97	13.00	5.73	36.00	10	7	100	65	0.622	0.0	37.08	37.08	****	****
115	6	918	1.97	13.00	5.73	35.36	10	7	100	66	0.644	0.0	42.90	42.90	****	****
115	7	919	1.97	13.00	12.75	4.44	10	9	100	67	0.667	6.24	46.20	39.96	****	****
115	8	920	1.97	13.00	25.82	2.28	10	10	96	71	0.733	16.38	59.40	43.02	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
115	9	921	1.97	13.00	38.92	1.59	10	10	85	75	0.744	31.98	72.60	40.62	****	****
115	10	922	1.97	13.00	51.76	1.27	10	8	70	79	0.699	53.82	105.60	51.78	****	****
115	11	923	1.97	13.00	63.71	1.11	8	6	60	82	0.661	******	115.50	******	****	****
115	12	924	1.97	13.00	72.56	1.05	8	6	56	84	0.658	******	122.10	******	****	****
115	13	925	1.97	13.00	72.54	1.05	10	5	55	84	0.646	60.06	122.10	62.04	****	****
115	14	926	1.97	13.00	63.67	1.11	9	4	54	84	0.634	57.72	115.50	57.78	****	****
115	15	927	1.97	13.00	51.71	1.27	9	4	52	86	0.652	46.02	99.00	52.98	****	****
115	16	928	1.97	13.00	38.87	1.59	9	7	52	84	0.611	30.42	69.30	38.88	****	0.95
115	17	929	1.97	13.00	25.77	2.29	9	8	55	86	0.689	17.16	56.10	38.94	****	0.94
115	18	930	1.97	13.00	12.70	4.46	8	3	54	85	0.656	14.04	46.20	32.16	****	0.78
115	19	931	1.97	13.00	5.73	34.80	5	2	57	82	0.628	0.0	29.70	29.70	****	0.74
115	20	932	1.97	13.00	5.73	36.00	4	2	66	78	0.638	0.0	30.48	30.48	****	0.78
115	21	933	1.97	13.00	5.73	36.00	4	2	85	76	0.769	0.0	30.48	30.48	****	0.79
115	22	934	1.97	13.00	5.73	36.00	4	2	90	70	0.665	0.0	30.48	30.48	****	0.83
115	23	935	1.97	13.00	5.73	36.00	6	3	94	69	0.671	0.0	33.78	33.78	****	0.92
115	24	936	1.97	13.00	5.73	36.00	6	5	95	69	0.678	0.0	33.78	33.78	****	0.92
116	1	937	1.97	13.30	5.73	36.00	7	4	95	68	0.655	0.0	33.00	33.00	****	0.91
116	2	938	1.97	13.30	5.73	36.00	7	4	95	67	0.634	0.0	33.00	33.00	****	0.92
116	3	939	1.97	13.30	5.73	36.00	9	8	95	68	0.655	0.0	33.00	33.00	****	0.91
116	4	940	1.97	13.30	5.73	36.00	10	7	95	68	0.655	0.0	33.00	33.00	****	0.91
116	5	941	1.97	13.30	5.73	36.00	10	9	97	68	0.669	0.0	33.00	33.00	****	0.91
116	6	942	1.97	13.30	5.73	36.00	10	10	98	68	0.676	0.0	36.30	36.30	****	****
116	7	943	1.97	13.30	5.73	36.19	10	10	98	70	0.724	0.78	42.90	42.12	****	****
116	8	944	1.97	13.30	12.87	4.40	10	10	90	74	0.761	7.80	82.50	74.70	****	****
116	9	945	1.97	13.30	25.93	2.28	9	8	83	76	0.751	21.84	******	******	****	****
116	10	946	1.97	13.30	39.03	1.58	10	5	70	80	0.722	36.66	******	******	****	****
116	11	947	1.97	13.30	51.89	1.27	10	10	67	81	0.714	47.58	99.00	51.42	****	****
116	12	948	1.97	13.30	63.89	1.11	10	10	65	82	0.716	42.90	89.10	46.20	****	****
116	13	949	1.97	13.30	72.83	1.05	10	10	62	82	0.683	43.68	89.10	45.42	****	****
116	14	950	1.97	13.30	72.83	1.05	10	10	60	84	0.705	41.34	79.20	37.86	****	0.93
116	15	951	1.97	13.30	63.89	1.11	10	10	61	82	0.672	46.02	95.70	49.68	****	****
116	16	952	1.97	13.30	51.89	1.27	9	8	61	82	0.672	38.22	82.50	44.28	****	****
116	17	953	1.97	13.30	39.03	1.58	9	8	62	82	0.683	33.54	72.60	39.06	****	0.97
116	18	954	1.97	13.30	25.93	2.28	8	5	66	80	0.681	21.84	59.40	37.56	****	0.95
116	19	955	1.97	13.30	12.86	4.41	7	4	72	75	0.630	11.70	42.90	31.20	****	0.82
116	20	956	1.97	13.30	5.73	36.26	5	2	82	74	0.694	0.78	29.70	28.92	****	0.76
116	21	957	1.97	13.30	5.73	36.00	5	2	90	73	0.736	0.0	29.70	29.70	****	0.79
116	22	958	1.97	13.30	5.73	36.00	5	2	94	72	0.744	0.0	29.70	29.70	****	0.79
116	23	959	1.97	13.30	5.73	36.00	4	2	97	70	0.717	0.0	29.70	29.70	****	0.81
116	24	960	1.97	13.30	5.73	36.00	7	5	97	71	0.741	0.0	29.70	29.70	****	0.80

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
117	1	961	1.97	13.60	5.73	36.00	7	6	97	70	0.717	0.0	33.00	33.00	****	0.90
117	2	962	1.97	13.60	5.73	36.00	8	4	98	70	0.724	0.0	33.00	33.00	****	0.90
117	3	963	1.97	13.60	5.73	36.00	9	3	98	70	0.724	0.0	33.00	33.00	****	0.90
117	4	964	1.97	13.60	5.73	36.00	9	6	98	70	0.724	0.0	33.00	33.00	****	0.90
117	5	965	1.97	13.60	5.73	36.00	9	7	98	70	0.724	0.0	33.00	33.00	****	0.90
117	6	966	1.97	13.60	5.73	36.00	8	6	99	70	0.732	0.0	33.00	33.00	****	0.90
117	7	967	1.97	13.60	5.73	34.98	9	4	98	70	0.724	1.56	36.30	34.74	****	0.94
117	8	968	1.97	13.60	12.96	4.37	9	3	98	70	0.724	10.92	49.50	38.58	****	****
117	9	969	1.97	13.60	26.02	2.27	9	6	98	73	0.802	27.30	69.30	42.00	****	****
117	10	970	1.97	13.60	39.12	1.58	8	3	90	76	0.814	39.00	85.80	46.80	****	****
117	11	971	1.97	13.60	52.00	1.27	8	3	76	78	0.735	47.58	99.00	51.42	****	****
117	12	972	1.97	13.60	64.05	1.11	8	6	70	80	0.722	49.92	108.90	58.98	****	****
117	13	973	1.97	13.60	73.09	1.04	8	6	59	84	0.693	53.04	112.20	59.16	****	****
117	14	974	1.97	13.60	73.13	1.04	9	8	54	84	0.634	46.80	102.30	55.50	****	****
117	15	975	1.97	13.60	64.12	1.11	9	8	52	86	0.652	60.84	112.20	51.36	****	****
117	16	976	1.97	13.60	52.08	1.27	8	7	49	87	0.634	45.24	89.10	43.86	****	****
117	17	977	1.97	13.60	39.21	1.58	9	4	50	86	0.626	35.88	75.90	40.02	****	0.97
117	18	978	1.97	13.60	26.10	2.26	5	2	52	86	0.652	27.30	62.70	35.40	****	0.85
117	19	979	1.97	13.60	13.04	4.35	3	1	55	83	0.626	11.70	42.90	31.20	****	0.77
117	20	980	1.97	13.60	5.73	34.08	3	1	62	78	0.600	0.78	33.00	32.22	****	0.82
117	21	981	1.97	13.60	5.73	36.00	2	1	73	75	0.639	0.0	26.40	26.40	****	0.69
117	22	982	1.97	13.60	5.73	36.00	2	1	80	72	0.633	0.0	26.40	26.40	****	0.71
117	23	983	1.97	13.60	5.73	36.00	0	0	89	71	0.680	0.0	29.70	29.70	****	0.80
117	24	984	1.97	13.60	5.73	36.00	0	0	92	70	0.680	0.0	29.70	29.70	****	0.81
118	1	985	1.97	13.90	5.73	36.00	0	0	96	69	0.685	0.0	29.70	29.70	****	0.81
118	2	986	1.97	13.90	5.73	36.00	8	8	97	67	0.647	0.0	29.70	29.70	****	0.83
118	3	987	1.97	13.90	5.73	36.00	10	10	98	66	0.631	0.0	33.00	33.00	****	0.92
118	4	988	1.97	13.90	5.73	36.00	10	10	100	66	0.644	0.0	46.20	46.20	****	****
118	5	989	1.97	13.90	5.73	36.00	10	10	100	68	0.690	0.0	59.40	59.40	****	****
118	6	990	1.97	13.90	5.73	36.00	10	10	100	68	0.690	0.0	72.60	72.60	****	****
118	7	991	1.97	13.90	5.73	33.75	10	10	100	68	0.690	0.78	72.60	71.82	****	****
118	8	992	1.97	13.90	13.06	4.34	9	8	100	69	0.714	6.24	79.20	72.96	****	****
118	9	993	1.97	13.90	26.11	2.26	8	8	100	73	0.818	23.40	79.20	55.80	****	****
118	10	994	1.97	13.90	39.21	1.58	8	8	92	77	0.860	38.22	89.10	50.88	****	****
118	11	995	1.97	13.90	52.11	1.27	9	6	80	82	0.882	51.48	115.50	64.02	****	****
118	12	996	1.97	13.90	64.20	1.11	9	4	66	84	0.775	******	115.50	******	****	****
118	13	997	1.97	13.90	73.35	1.04	8	6	55	86	0.689	******	122.10	******	****	****
118	14	998	1.97	13.90	73.42	1.04	8	6	50	88	0.667	******	115.50	******	****	****
118	15	999	1.97	13.90	64.35	1.11	4	3	50	87	0.646	******	108.90	******	****	****
118	16	1000	1.97	13.90	52.27	1.26	3	2	48	87	0.621	60.84	108.90	48.06	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
118	17	1001	1.97	13.90	39.38	1.57	5	2	43	88	0.574	44.46	85.80	41.34	****	0.98
118	18	1002	1.97	13.90	26.28	2.25	4	2	44	87	0.569	28.86	62.70	33.84	****	0.81
118	19	1003	1.97	13.90	13.22	4.29	3	1	47	84	0.552	11.70	42.90	31.20	****	0.76
118	20	1004	1.97	13.90	5.73	32.01	3	1	55	79	0.549	0.78	23.10	22.32	****	0.57
118	21	1005	1.97	13.90	5.73	36.00	3	1	70	75	0.612	0.0	23.10	23.10	****	0.60
118	22	1006	1.97	13.90	5.73	36.00	3	1	80	72	0.633	0.0	26.40	26.40	****	0.71
118	23	1007	1.97	13.90	5.73	36.00	3	1	91	70	0.672	0.0	29.70	29.70	****	0.81
118	24	1008	1.97	13.90	5.73	36.00	10	9	95	69	0.678	0.0	29.70	29.70	****	0.81
119	1	1009	1.97	14.20	5.73	36.00	10	10	97	68	0.669	0.0	33.00	33.00	****	0.91
119	2	1010	1.97	14.20	5.73	36.00	10	10	98	68	0.676	0.0	36.30	36.30	****	****
119	3	1011	1.97	14.20	5.73	36.00	10	10	98	68	0.676	0.0	42.90	42.90	****	****
119	4	1012	1.97	14.20	5.73	36.00	10	10	99	68	0.683	0.0	49.50	49.50	****	****
119	5	1013	1.97	14.20	5.73	36.00	10	10	99	68	0.683	0.0	46.20	46.20	****	****
119	6	1014	1.97	14.20	5.73	36.00	8	8	99	68	0.683	0.0	52.80	52.80	****	****
119	7	1015	1.97	14.20	5.73	32.35	10	9	99	68	0.683	0.78	46.20	45.42	****	****
119	8	1016	1.97	14.20	13.17	4.31	10	10	99	71	0.756	9.36	49.50	40.14	****	****
119	9	1017	1.97	14.20	26.22	2.25	8	4	95	73	0.777	15.60	56.10	40.50	****	****
119	10	1018	1.97	14.20	39.32	1.57	9	4	87	75	0.761	37.44	82.50	45.06	****	****
119	11	1019	1.97	14.20	52.24	1.26	8	3	75	80	0.774	54.60	108.90	54.30	****	****
119	12	1020	1.97	14.20	64.37	1.11	8	4	65	84	0.764	******	128.70	******	****	****
119	13	1021	1.97	14.20	73.61	1.04	9	5	58	85	0.704	******	122.10	******	****	****
119	14	1022	1.97	14.20	73.70	1.04	10	6	57	88	0.761	******	125.40	******	****	****
119	15	1023	1.97	14.20	64.56	1.11	10	8	53	88	0.708	55.38	112.20	56.82	****	****
119	16	1024	1.97	14.20	52.44	1.26	7	3	50	88	0.667	39.00	85.80	46.80	****	****
119	17	1025	1.97	14.20	39.53	1.57	6	2	52	87	0.672	25.74	72.60	46.86	****	****
119	18	1026	1.97	14.20	26.43	2.24	10	5	52	87	0.672	19.50	56.10	36.60	****	0.88
119	19	1027	1.97	14.20	13.38	4.24	10	6	60	83	0.683	5.46	39.60	34.14	****	0.84
119	20	1028	1.97	14.20	5.73	30.24	7	3	61	81	0.650	******	33.00	******	****	****
119	21	1029	1.97	14.20	5.73	36.00	5	2	77	79	0.769	0.0	******	******	****	****
119	22	1030	1.97	14.20	5.73	36.00	4	2	83	77	0.776	0.0	******	******	****	****
119	23	1031	1.97	14.20	5.73	36.00	3	1	84	75	0.735	0.0	******	******	****	****
119	24	1032	1.97	14.20	5.73	36.00	3	1	89	74	0.753	0.0	******	******	****	****
120	1	1033	1.97	14.50	5.73	36.00	4	3	90	74	0.761	0.0	******	******	****	****
120	2	1034	1.97	14.50	5.73	36.00	3	1	92	72	0.728	0.0	******	******	****	****
120	3	1035	1.97	14.50	5.73	36.00	0	0	96	71	0.733	0.0	******	******	****	****
120	4	1036	1.97	14.50	5.73	36.00	0	0	96	70	0.709	0.0	******	******	****	****
120	5	1037	1.97	14.50	5.73	36.00	3	2	97	70	0.717	0.0	******	******	****	****
120	6	1038	1.97	14.50	5.73	36.00	8	7	98	69	0.700	0.0	******	******	****	****
120	7	1039	1.97	14.50	5.73	31.23	7	6	98	69	0.700	******	39.60	******	****	****
120	8	1040	1.97	14.50	13.26	4.28	5	2	98	71	0.749	7.80	42.90	35.10	****	0.95

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
120	9	1041	1.97	14.50	26.30	2.25	8	2	85	75	0.744	31.20	72.60	41.40	****	****
120	10	1042	1.97	14.50	39.41	1.57	8	2	78	80	0.805	46.02	95.70	49.68	****	****
120	11	1043	1.97	14.50	52.34	1.26	9	4	66	84	0.775	56.94	115.50	58.56	****	****
120	12	1044	1.97	14.50	64.52	1.11	10	6	56	87	0.724	60.06	115.50	55.44	****	****
120	13	1045	1.97	14.50	73.86	1.04	10	7	52	90	0.739	62.40	122.10	59.70	****	****
120	14	1046	1.97	14.50	74.00	1.04	10	8	46	90	0.654	56.16	115.50	59.34	****	****
120	15	1047	1.97	14.50	64.78	1.10	10	8	46	90	0.654	43.68	95.70	52.02	****	****
120	16	1048	1.97	14.50	52.63	1.26	8	5	46	90	0.654	39.00	89.10	50.10	****	****
120	17	1049	1.97	14.50	39.71	1.56	8	3	46	90	0.654	33.54	85.80	52.26	****	****
120	18	1050	1.97	14.50	26.60	2.22	4	2	50	87	0.646	24.18	66.00	41.82	****	****
120	19	1051	1.97	14.50	13.56	4.19	3	1	55	85	0.668	9.36	42.90	33.54	****	0.81
120	20	1052	1.97	14.50	5.73	28.38	0	0	61	80	0.630	******	33.00	******	****	****
120	21	1053	1.97	14.50	5.73	36.00	0	0	70	76	0.633	0.0	******	******	****	****
120	22	1054	1.97	14.50	5.73	36.00	0	0	79	75	0.691	0.0	******	******	****	****
120	23	1055	1.97	14.50	5.73	36.00	0	0	85	74	0.719	0.0	******	******	****	****
120	24	1056	1.97	14.50	5.73	36.00	0	0	89	72	0.704	0.0	******	******	****	****
121	1	1057	1.97	14.80	5.73	36.00	0	0	92	72	0.728	0.0	******	******	****	****
121	2	1058	1.97	14.80	5.73	36.00	0	0	93	70	0.687	0.0	******	******	****	****
121	3	1059	1.97	14.80	5.73	36.00	6	6	95	70	0.702	0.0	******	******	****	****
121	4	1060	1.97	14.80	5.73	36.00	0	0	95	70	0.702	0.0	******	******	****	****
121	5	1061	1.97	14.80	5.73	36.00	0	0	95	69	0.678	0.0	******	******	****	****
121	6	1062	1.97	14.80	5.73	36.00	0	0	95	68	0.655	0.0	******	******	****	****
121	7	1063	1.97	14.80	5.73	29.93	4	4	95	68	0.655	******	33.00	******	****	****
121	8	1064	1.97	14.80	13.38	4.25	1	0	91	68	0.628	******	49.50	******	****	****
121	9	1065	1.97	14.80	26.41	2.24	6	6	85	72	0.672	******	72.60	******	****	****
121	10	1066	1.97	14.80	39.52	1.57	4	3	70	75	0.612	******	102.30	******	****	****
121	11	1067	1.97	14.80	52.46	1.26	7	6	55	79	0.549	******	122.10	******	****	****
121	12	1068	1.97	14.80	64.69	1.11	6	5	51	82	0.562	******	125.40	******	****	****
121	13	1069	1.97	14.80	74.12	1.04	6	5	48	84	0.564	******	128.70	******	****	****
121	14	1070	1.97	14.80	74.28	1.04	5	4	44	87	0.569	******	138.60	******	****	****
121	15	1071	1.97	14.80	64.99	1.10	5	4	44	87	0.569	******	125.40	******	****	****
121	16	1072	1.97	14.80	52.80	1.25	4	4	49	85	0.595	******	95.70	******	****	****
121	17	1073	1.97	14.80	39.86	1.56	5	2	52	84	0.611	******	82.50	******	****	****
121	18	1074	1.97	14.80	26.75	2.21	5	2	50	84	0.587	******	66.00	******	****	****
121	19	1075	1.97	14.80	13.72	4.15	5	2	51	80	0.526	******	33.00	******	****	****
121	20	1076	1.97	14.80	5.73	26.84	3	1	54	77	0.505	******	29.70	******	****	****
121	21	1077	1.97	14.80	5.73	36.00	3	1	59	74	0.499	0.0	******	******	****	****
121	22	1078	1.97	14.80	5.73	36.00	9	5	66	72	0.522	0.0	******	******	****	****
121	23	1079	1.97	14.80	5.73	36.00	8	5	76	71	0.581	0.0	******	******	****	****
121	24	1080	1.97	14.80	5.73	36.00	6	4	82	70	0.606	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES *	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
122	1	1081	1.97	15.10	5.73	36.00	5	2	86	69	0.614	0.0	******	******	****	****
122	2	1082	1.97	15.10	5.73	36.00	5	2	90	68	0.621	0.0	******	******	****	****
122	3	1083	1.97	15.10	5.73	36.00	5	2	91	67	0.607	0.0	******	******	****	****
122	4	1084	1.97	15.10	5.73	36.00	5	2	91	66	0.586	0.0	******	******	****	****
122	5	1085	1.97	15.10	5.73	36.00	5	2	92	66	0.592	0.0	******	******	****	****
122	6	1086	1.97	15.10	5.73	36.00	5	2	94	65	0.585	0.0	******	******	****	****
122	7	1087	1.97	15.10	5.73	28.66	3	1	96	64	0.576	******	29.70	******	****	****
122	8	1088	1.97	15.10	13.49	4.21	3	1	97	64	0.582	******	49.50	******	****	****
122	9	1089	1.97	15.10	26.52	2.23	4	2	88	68	0.607	******	79.20	******	****	****
122	10	1090	1.97	15.10	39.63	1.56	5	2	70	73	0.573	******	102.30	******	****	****
122	11	1091	1.97	15.10	52.59	1.26	5	2	65	76	0.588	******	82.50	******	****	****
122	12	1092	1.97	15.10	64.85	1.10	5	5	57	79	0.569	******	128.70	******	****	****
122	13	1093	1.97	15.10	74.38	1.04	5	5	49	83	0.558	******	155.10	******	****	****
122	14	1094	1.97	15.10	74.57	1.04	5	5	45	84	0.529	******	108.90	******	****	****
122	15	1095	1.97	15.10	65.19	1.10	7	7	46	82	0.507	******	89.10	******	****	****
122	16	1096	1.97	15.10	52.96	1.25	9	9	46	82	0.507	******	92.40	******	****	****
122	17	1097	1.97	15.10	40.01	1.55	9	9	45	82	0.496	14.82	56.10	41.28	****	****
122	18	1098	1.97	15.10	26.90	2.20	9	5	50	81	0.533	12.48	52.80	40.32	****	****
122	19	1099	1.97	15.10	13.87	4.10	6	2	55	79	0.549	5.46	39.60	34.14	****	0.87
122	20	1100	1.97	15.10	5.73	25.44	0	0	60	75	0.525	******	29.70	******	****	****
122	21	1101	1.97	15.10	5.73	36.00	0	0	68	73	0.556	0.0	******	******	****	****
122	22	1102	1.97	15.10	5.73	36.00	0	0	72	70	0.532	0.0	******	******	****	****
122	23	1103	1.97	15.10	5.73	36.00	0	0	75	68	0.517	0.0	******	******	****	****
122	24	1104	1.97	15.10	5.73	36.00	0	0	81	67	0.540	0.0	******	******	****	****
123	1	1105	1.96	15.40	5.73	36.00	0	0	85	65	0.529	0.0	******	******	****	****
123	2	1106	1.96	15.40	5.73	36.00	0	0	89	64	0.534	0.0	******	******	****	****
123	3	1107	1.96	15.40	5.73	36.00	0	0	92	63	0.534	0.0	******	******	****	****
123	4	1108	1.96	15.40	5.73	36.00	0	0	96	62	0.538	0.0	******	******	****	****
123	5	1109	1.96	15.40	5.73	36.00	3	3	98	61	0.529	0.0	******	******	****	****
123	6	1110	1.96	15.40	5.73	36.00	7	2	99	60	0.517	0.0	******	******	****	****
123	7	1111	1.96	15.40	5.73	27.67	5	1	99	60	0.517	******	36.30	******	****	****
123	8	1112	1.96	15.40	13.58	4.18	5	1	99	61	0.535	******	56.10	******	****	****
123	9	1113	1.96	15.40	26.60	2.22	4	1	99	67	0.660	******	79.20	******	****	****
123	10	1114	1.96	15.40	39.71	1.56	3	1	75	72	0.593	******	105.60	******	****	****
123	11	1115	1.96	15.40	52.69	1.26	8	4	63	75	0.551	******	122.10	******	****	****
123	12	1116	1.96	15.40	65.00	1.10	9	6	52	80	0.537	******	128.70	******	****	****
123	13	1117	1.96	15.40	74.63	1.04	9	4	49	82	0.540	******	135.30	******	****	****
123	14	1118	1.96	15.40	74.86	1.04	9	4	48	84	0.564	******	138.60	******	****	****
123	15	1119	1.96	15.40	65.41	1.10	7	3	45	84	0.529	67.08	125.40	58.32	****	****
123	16	1120	1.96	15.40	53.15	1.25	7	3	42	85	0.510	65.52	115.50	49.98	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
123	17	1121	1.96	15.40	40.19	1.55	6	2	42	86	0.526	39.78	92.40	52.62	****	****
123	18	1122	1.96	15.40	27.07	2.19	7	3	42	83	0.478	14.04	46.20	32.16	****	0.79
123	19	1123	1.96	15.40	14.05	4.05	7	3	50	80	0.516	5.46	39.60	34.14	****	0.86
123	20	1124	1.96	15.40	5.73	23.97	7	2	57	78	0.551	1.56	33.00	31.44	****	0.80
123	21	1125	1.96	15.40	5.73	36.00	5	1	62	75	0.542	0.0	29.70	29.70	****	0.78
123	22	1126	1.96	15.40	5.73	36.00	3	1	70	72	0.554	0.0	29.70	29.70	****	0.79
123	23	1127	1.96	15.40	5.73	36.00	3	1	80	70	0.591	0.0	33.00	33.00	****	0.90
123	24	1128	1.96	15.40	5.73	36.00	5	4	90	68	0.621	0.0	33.00	33.00	****	0.91
124	1	1129	1.96	15.70	5.73	36.00	4	3	89	69	0.635	0.0	33.00	33.00	****	0.90
124	2	1130	1.96	15.70	5.73	36.00	3	1	92	68	0.635	0.0	33.00	33.00	****	0.91
124	3	1131	1.96	15.70	5.73	36.00	4	3	95	67	0.634	0.0	33.00	33.00	****	0.92
124	4	1132	1.96	15.70	5.73	36.00	5	4	96	67	0.640	0.0	36.30	36.30	****	****
124	5	1133	1.96	15.70	5.73	36.00	5	4	97	67	0.647	0.0	36.30	36.30	****	****
124	6	1134	1.96	15.70	5.73	36.00	10	10	97	67	0.647	0.0	36.30	36.30	****	****
124	7	1135	1.96	15.70	5.73	26.55	8	7	97	67	0.647	1.56	39.60	38.04	****	****
124	8	1136	1.96	15.70	13.70	4.15	9	8	97	67	0.647	7.80	49.50	41.70	****	****
124	9	1137	1.96	15.70	26.71	2.22	9	8	92	70	0.680	21.84	69.30	47.46	****	****
124	10	1138	1.96	15.70	39.82	1.56	7	6	88	72	0.696	35.10	85.80	50.70	****	****
124	11	1139	1.96	15.70	52.80	1.25	6	5	82	74	0.694	39.00	85.80	46.80	****	****
124	12	1140	1.96	15.70	65.15	1.10	7	6	65	76	0.588	******	132.00	******	****	****
124	13	1141	1.96	15.70	74.89	1.04	8	7	65	76	0.588	******	99.00	******	****	****
124	14	1142	1.96	15.70	75.14	1.03	10	10	97	72	0.767	******	******	******	****	****
124	15	1143	1.96	15.70	65.61	1.10	10	10	82	72	0.649	******	82.50	******	****	****
124	16	1144	1.96	15.70	53.31	1.25	10	10	81	71	0.619	23.40	59.40	36.00	****	0.97
124	17	1145	1.96	15.70	40.33	1.54	10	10	80	70	0.591	8.58	42.90	34.32	****	0.93
124	18	1146	1.96	15.70	27.22	2.18	10	10	80	68	0.552	10.14	42.90	32.76	****	0.90
124	19	1147	1.96	15.70	14.21	4.01	10	10	81	65	0.504	3.90	36.30	32.40	****	0.91
124	20	1148	1.96	15.70	5.73	22.76	10	10	81	63	0.470	1.56	33.00	31.44	****	0.90
124	21	1149	1.96	15.70	5.73	36.00	10	10	81	62	0.454	0.0	33.00	33.00	****	0.95
124	22	1150	1.96	15.70	5.73	36.00	10	10	79	61	0.427	0.0	33.00	33.00	****	0.96
124	23	1151	1.96	15.70	5.73	36.00	10	10	79	60	0.412	0.0	33.00	33.00	****	0.97
124	24	1152	1.96	15.70	5.73	36.00	8	8	78	60	0.407	0.0	33.00	33.00	****	0.97
125	1	1153	1.96	16.00	5.73	36.00	3	3	77	60	0.402	0.0	29.70	29.70	****	0.87
125	2	1154	1.96	16.00	5.73	36.00	0	0	80	56	0.362	0.0	26.40	26.40	****	0.80
125	3	1155	1.96	16.00	5.73	36.00	0	0	85	54	0.357	0.0	26.40	26.40	****	0.81
125	4	1156	1.96	16.00	5.73	36.00	0	0	86	54	0.361	0.0	26.40	26.40	****	0.81
125	5	1157	1.96	16.00	5.73	36.00	0	0	88	53	0.356	0.0	26.40	26.40	****	0.82
125	6	1158	1.96	16.00	5.73	36.00	0	0	93	52	0.363	0.0	26.40	26.40	****	0.82
125	7	1159	1.96	16.00	5.73	25.48	0	0	95	51	0.357	0.78	29.70	28.92	0.90	0.91
125	8	1160	1.96	16.00	13.81	4.12	0	0	95	53	0.385	13.26	49.50	36.24	0.83	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
125	9	1161	1.96	16.00	26.81	2.21	0	0	87	58	0.423	22.62	75.90	53.28	0.68	****
125	10	1162	1.96	16.00	39.92	1.56	0	0	75	62	0.420	49.14	99.00	49.86	0.76	****
125	11	1163	1.96	16.00	52.92	1.25	0	0	60	66	0.386	63.96	122.10	58.14	0.74	****
125	12	1164	1.96	16.00	65.31	1.10	0	0	50	70	0.369	71.76	132.00	60.24	0.70	****
125	13	1165	1.96	16.00	75.14	1.03	0	0	44	73	0.360	79.56	138.60	59.04	0.71	****
125	14	1166	1.96	16.00	75.42	1.03	0	0	40	75	0.350	80.34	138.60	58.26	0.71	****
125	15	1167	1.96	16.00	65.81	1.10	0	0	37	77	0.346	76.44	128.70	52.26	0.73	****
125	16	1168	1.96	16.00	53.47	1.24	0	0	36	78	0.348	66.30	112.20	45.90	0.75	****
125	17	1169	1.96	16.00	40.48	1.54	0	0	36	78	0.348	53.04	89.10	36.06	0.79	0.92
125	18	1170	1.96	16.00	27.37	2.17	0	0	36	77	0.337	37.44	66.00	28.56	0.84	0.74
125	19	1171	1.96	16.00	14.36	3.97	0	0	37	76	0.335	17.94	42.90	24.96	0.88	0.65
125	20	1172	1.96	16.00	5.73	21.64	0	0	40	70	0.296	2.34	26.40	24.06	0.93	0.65
125	21	1173	1.96	16.00	5.73	36.00	0	0	49	66	0.316	0.0	26.40	26.40	****	0.74
125	22	1174	1.96	16.00	5.73	36.00	0	0	70	62	0.392	0.0	26.40	26.40	****	0.76
125	23	1175	1.96	16.00	5.73	36.00	0	0	85	59	0.428	0.0	26.40	26.40	****	0.78
125	24	1176	1.96	16.00	5.73	36.00	0	0	90	57	0.421	0.0	26.40	26.40	****	0.79
126	1	1177	1.96	16.30	5.73	36.00	0	0	93	56	0.420	0.0	16.50	16.50	****	0.50
126	2	1178	1.96	16.30	5.73	36.00	0	0	96	54	0.403	0.0	16.50	16.50	****	0.51
126	3	1179	1.96	16.30	5.73	36.00	0	0	97	54	0.407	0.0	16.50	16.50	****	0.51
126	4	1180	1.96	16.30	5.73	36.00	0	0	98	52	0.382	0.0	16.50	16.50	****	0.51
126	5	1181	1.96	16.30	5.73	36.00	0	0	98	52	0.382	0.0	16.50	16.50	****	0.51
126	6	1182	1.96	16.30	5.73	36.00	0	0	99	51	0.372	0.0	16.50	16.50	****	0.52
126	7	1183	1.96	16.30	5.73	24.48	0	0	99	52	0.386	2.34	19.80	17.46	0.94	0.54
126	8	1184	1.96	16.30	13.92	4.09	0	0	99	60	0.517	21.84	39.60	17.76	0.94	0.52
126	9	1185	1.96	16.30	26.91	2.20	0	0	68	70	0.503	39.00	66.00	27.00	0.87	0.73
126	10	1186	1.96	16.30	40.02	1.55	0	0	50	74	0.423	54.60	82.50	27.90	0.81	0.74
126	11	1187	1.96	16.30	53.03	1.25	0	0	45	78	0.435	67.86	115.50	47.64	0.77	****
126	12	1188	1.96	16.30	65.46	1.10	0	0	39	83	0.444	76.44	128.70	52.26	0.74	****
126	13	1189	1.96	16.30	75.40	1.03	0	0	35	84	0.411	79.56	132.00	52.44	0.71	****
126	14	1190	1.96	16.30	75.70	1.03	0	0	32	86	0.401	78.00	132.00	54.00	0.69	****
126	15	1191	1.96	16.30	66.01	1.09	0	0	32	88	0.427	71.76	122.10	50.34	0.69	****
126	16	1192	1.96	16.30	53.63	1.24	0	0	30	88	0.400	60.06	105.60	45.54	0.69	****
126	17	1193	1.96	16.30	40.63	1.53	0	0	29	88	0.387	44.46	82.50	38.04	0.70	0.90
126	18	1194	1.96	16.30	27.52	2.16	0	0	29	87	0.375	27.30	59.40	32.10	0.73	0.77
126	19	1195	1.96	16.30	14.52	3.93	0	0	29	86	0.363	10.14	33.00	22.86	0.76	0.55
126	20	1196	1.96	16.30	5.73	20.61	0	0	35	79	0.350	0.78	19.80	19.02	0.88	0.48
126	21	1197	1.96	16.30	5.73	36.00	0	0	48	72	0.380	0.0	19.80	19.80	****	0.53
126	22	1198	1.96	16.30	5.73	36.00	0	0	52	70	0.384	0.0	16.50	16.50	****	0.45
126	23	1199	1.96	16.30	5.73	36.00	0	0	58	68	0.400	0.0	16.50	16.50	****	0.45
126	24	1200	1.96	16.30	5.73	36.00	0	0	70	65	0.435	0.0	16.50	16.50	****	0.47

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
127	1	1201	1.96	16.60	5.73	36.00	0	0	89	63	0.516	0.0	16.50	16.50	****	0.47
127	2	1202	1.96	16.60	5.73	36.00	0	0	94	60	0.491	0.0	16.50	16.50	****	0.48
127	3	1203	1.96	16.60	5.73	36.00	0	0	94	60	0.491	0.0	16.50	16.50	****	0.48
127	4	1204	1.96	16.60	5.73	36.00	0	0	90	60	0.470	0.0	16.50	16.50	****	0.48
127	5	1205	1.96	16.60	5.73	36.00	0	0	90	59	0.453	0.0	16.50	16.50	****	0.49
127	6	1206	1.96	16.60	5.73	36.00	0	0	97	58	0.471	0.0	19.80	19.80	****	0.59
127	7	1207	1.96	16.60	5.73	23.51	0	0	98	58	0.476	3.12	23.10	19.98	0.95	0.59
127	8	1208	1.96	16.60	14.04	4.06	1	1	98	62	0.549	18.72	39.60	20.88	****	0.60
127	9	1209	1.96	16.60	27.02	2.19	0	0	62	70	0.458	36.66	66.00	29.34	0.84	0.80
127	10	1210	1.96	16.60	40.13	1.55	0	0	58	75	0.507	52.26	92.40	40.14	0.79	****
127	11	1211	1.96	16.60	53.15	1.25	0	0	41	80	0.423	66.30	108.90	42.60	0.76	****
127	12	1212	1.96	16.60	65.62	1.10	4	4	40	86	0.501	75.66	128.70	53.04	****	****
127	13	1213	1.96	16.60	75.65	1.03	4	4	39	84	0.458	******	108.90	******	****	****
127	14	1214	1.96	16.60	75.98	1.03	4	4	37	89	0.510	******	141.90	******	****	****
127	15	1215	1.96	16.60	66.20	1.09	4	4	35	89	0.482	67.86	122.10	54.24	****	****
127	16	1216	1.96	16.60	53.78	1.24	3	3	33	89	0.455	60.84	105.60	44.76	****	****
127	17	1217	1.96	16.60	40.77	1.53	2	2	32	90	0.455	44.46	79.20	34.74	****	0.81
127	18	1218	1.96	16.60	27.66	2.14	0	0	32	90	0.455	27.30	59.40	32.10	0.72	0.75
127	19	1219	1.96	16.60	14.67	3.89	0	0	38	88	0.507	8.58	33.00	24.42	0.73	0.58
127	20	1220	1.96	16.60	5.73	19.67	0	0	58	78	0.561	0.78	19.80	19.02	0.87	0.49
127	21	1221	1.96	16.60	5.73	36.00	0	0	62	76	0.561	0.0	19.80	19.80	****	0.51
127	22	1222	1.96	16.60	5.73	36.00	0	0	72	71	0.550	0.0	19.80	19.80	****	0.53
127	23	1223	1.96	16.60	5.73	36.00	0	0	80	70	0.591	0.0	19.80	19.80	****	0.54
127	24	1224	1.96	16.60	5.73	36.00	0	0	90	68	0.621	0.0	19.80	19.80	****	0.55
128	1	1225	1.96	16.90	5.73	36.00	0	0	87	66	0.560	0.0	19.80	19.80	****	0.55
128	2	1226	1.96	16.90	5.73	36.00	0	0	93	66	0.599	0.0	23.10	23.10	****	0.65
128	3	1227	1.96	16.90	5.73	36.00	0	0	97	66	0.625	0.0	23.10	23.10	****	0.65
128	4	1228	1.96	16.90	5.73	36.00	0	0	99	65	0.616	0.0	26.40	26.40	****	0.74
128	5	1229	1.96	16.90	5.73	36.00	0	0	99	63	0.574	0.0	26.40	26.40	****	0.76
128	6	1230	1.96	16.90	5.73	36.00	0	0	99	63	0.574	0.0	26.40	26.40	****	0.76
128	7	1231	1.96	16.90	5.73	22.47	0	0	99	62	0.554	3.90	29.70	25.80	0.95	0.74
128	8	1232	1.96	16.90	14.17	4.02	0	0	99	63	0.574	20.28	49.50	29.22	0.92	0.84
128	9	1233	1.96	16.90	27.14	2.18	0	0	85	70	0.628	37.44	72.60	35.16	0.85	0.95
128	10	1234	1.96	16.90	40.25	1.54	0	0	70	74	0.592	53.04	95.70	42.66	0.79	****
128	11	1235	1.96	16.90	53.28	1.25	0	0	62	78	0.600	65.52	115.50	49.98	0.75	****
128	12	1236	1.96	16.90	65.79	1.10	1	1	56	80	0.578	70.20	128.70	58.50	****	****
128	13	1237	1.96	16.90	75.91	1.03	3	3	50	85	0.607	79.56	135.30	55.74	****	****
128	14	1238	1.96	16.90	76.25	1.03	5	5	46	86	0.576	79.56	135.30	55.74	****	****
128	15	1239	1.96	16.90	66.37	1.09	3	3	42	88	0.561	68.64	118.80	50.16	****	****
128	16	1240	1.96	16.90	53.92	1.24	5	5	40	88	0.534	27.30	72.60	45.30	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
128	17	1241	1.96	16.90	40.90	1.52	2	2	49	80	0.506	32.76	62.70	29.94	****	0.75
128	18	1242	1.96	16.90	27.79	2.14	5	5	48	82	0.529	17.16	49.50	32.34	****	0.80
128	19	1243	1.96	16.90	14.81	3.86	0	0	50	81	0.533	7.02	33.00	25.98	0.69	0.65
128	20	1244	1.96	16.90	5.73	18.90	0	0	52	80	0.537	0.78	23.10	22.32	0.87	0.56
128	21	1245	1.96	16.90	5.73	36.00	0	0	68	76	0.615	0.0	19.80	19.80	****	0.51
128	22	1246	1.96	16.90	5.73	36.00	0	0	75	72	0.593	0.0	23.10	23.10	****	0.62
128	23	1247	1.96	16.90	5.73	36.00	0	0	86	70	0.636	0.0	23.10	23.10	****	0.63
128	24	1248	1.96	16.90	5.73	36.00	0	0	87	70	0.643	0.0	23.10	23.10	****	0.63
129	1	1249	1.96	17.20	5.73	36.00	0	0	89	70	0.658	0.0	23.10	23.10	****	0.63
129	2	1250	1.96	17.20	5.73	36.00	0	0	88	69	0.628	0.0	23.10	23.10	****	0.63
129	3	1251	1.96	17.20	5.73	36.00	0	0	89	68	0.614	0.0	23.10	23.10	****	0.64
129	4	1252	1.96	17.20	5.73	36.00	0	0	90	67	0.600	0.0	23.10	23.10	****	0.64
129	5	1253	1.96	17.20	5.73	36.00	0	0	93	66	0.599	0.0	26.40	26.40	****	0.74
129	6	1254	1.96	17.20	5.73	36.00	0	0	96	65	0.597	0.0	26.40	26.40	****	0.74
129	7	1255	1.96	17.20	5.73	21.64	0	0	96	64	0.576	4.68	26.40	21.72	0.96	0.62
129	8	1256	1.96	17.20	14.28	3.99	0	0	97	65	0.603	19.50	49.50	30.00	0.91	0.85
129	9	1257	1.96	17.20	27.24	2.17	0	0	90	68	0.621	37.44	72.60	35.16	0.85	0.97
129	10	1258	1.96	17.20	40.35	1.54	0	0	78	73	0.638	53.82	95.70	41.88	0.80	****
129	11	1259	1.96	17.20	53.39	1.24	3	3	70	75	0.612	66.30	115.50	49.20	****	****
129	12	1260	1.96	17.20	65.93	1.09	3	3	60	79	0.599	78.00	125.40	47.40	****	****
129	13	1261	1.96	17.20	76.16	1.03	4	4	53	83	0.603	******	118.80	******	****	****
129	14	1262	1.96	17.20	76.53	1.03	5	4	50	83	0.569	******	115.50	******	****	****
129	15	1263	1.96	17.20	66.56	1.09	5	4	47	84	0.552	70.20	118.80	48.60	****	****
129	16	1264	1.96	17.20	54.07	1.23	8	4	38	87	0.491	60.06	112.20	52.14	****	****
129	17	1265	1.96	17.20	41.04	1.52	7	3	38	87	0.491	39.00	85.80	46.80	****	****
129	18	1266	1.96	17.20	27.93	2.13	4	1	37	87	0.478	28.08	69.30	41.22	****	0.99
129	19	1267	1.96	17.20	14.96	3.82	3	1	37	88	0.494	9.36	39.60	30.24	****	0.72
129	20	1268	1.96	17.20	5.73	18.07	2	1	49	80	0.506	0.78	23.10	22.32	****	0.56
129	21	1269	1.96	17.20	5.73	36.00	2	1	62	75	0.542	0.0	19.80	19.80	****	0.52
129	22	1270	1.96	17.20	5.73	36.00	2	1	69	73	0.564	0.0	19.80	19.80	****	0.53
129	23	1271	1.96	17.20	5.73	36.00	3	1	73	70	0.539	0.0	19.80	19.80	****	0.54
129	24	1272	1.96	17.20	5.73	36.00	3	1	79	69	0.564	0.0	19.80	19.80	****	0.54
130	1	1273	1.96	17.50	5.73	36.00	3	1	82	69	0.585	0.0	19.80	19.80	****	0.54
130	2	1274	1.96	17.50	5.73	36.00	0	0	85	68	0.586	0.0	19.80	19.80	****	0.55
130	3	1275	1.96	17.50	5.73	36.00	0	0	90	67	0.600	0.0	19.80	19.80	****	0.55
130	4	1276	1.96	17.50	5.73	36.00	0	0	93	65	0.578	0.0	19.80	19.80	****	0.56
130	5	1277	1.96	17.50	5.73	36.00	0	0	96	64	0.576	0.0	19.80	19.80	****	0.56
130	6	1278	1.96	17.50	5.73	36.00	0	0	97	62	0.543	0.0	19.80	19.80	****	0.57
130	7	1279	1.96	17.50	5.73	20.73	0	0	98	62	0.549	4.68	23.10	18.42	0.96	0.53
130	8	1280	1.96	17.50	14.42	3.95	0	0	98	63	0.568	22.62	46.20	23.58	0.94	0.68

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
130	9	1281	1.96	17.50	27.37	2.17	1	1	85	69	0.607	39.78	59.40	19.62	****	0.54
130	10	1282	1.96	17.50	40.47	1.54	3	3	70	74	0.592	56.94	99.00	42.06	****	****
130	11	1283	1.96	17.50	53.52	1.24	5	5	62	76	0.561	70.98	115.50	44.52	****	****
130	12	1284	1.96	17.50	66.10	1.09	5	5	56	80	0.578	79.56	138.60	59.04	****	****
130	13	1285	1.96	17.50	76.42	1.03	5	5	50	84	0.587	81.12	138.60	57.48	****	****
130	14	1286	1.96	17.50	76.79	1.03	5	5	46	84	0.540	78.78	138.60	59.82	****	****
130	15	1287	1.96	17.50	66.73	1.09	3	3	43	87	0.556	73.32	132.00	58.68	****	****
130	16	1288	1.96	17.50	54.20	1.23	2	2	42	88	0.561	62.40	115.50	53.10	****	****
130	17	1289	1.96	17.50	41.16	1.52	2	2	41	88	0.547	48.36	99.00	50.64	****	****
130	18	1290	1.96	17.50	28.06	2.12	3	3	41	88	0.547	23.40	62.70	39.30	****	0.93
130	19	1291	1.96	17.50	15.09	3.79	1	1	41	87	0.530	10.92	46.20	35.28	****	0.84
130	20	1292	1.96	17.50	5.73	17.40	0	0	52	80	0.537	0.78	26.40	25.62	0.86	0.65
130	21	1293	1.96	17.50	5.73	36.00	0	0	63	75	0.551	0.0	19.80	19.80	****	0.52
130	22	1294	1.96	17.50	5.73	36.00	0	0	69	74	0.584	0.0	19.80	19.80	****	0.52
130	23	1295	1.96	17.50	5.73	36.00	0	0	73	82	0.804	0.0	19.80	19.80	****	0.49
130	24	1296	1.96	17.50	5.73	36.00	0	0	80	80	0.826	0.0	19.80	19.80	****	0.50
131	1	1297	1.95	17.80	5.73	36.00	0	0	86	68	0.593	0.0	19.80	19.80	****	0.55
131	2	1298	1.95	17.80	5.73	36.00	0	0	93	66	0.599	0.0	19.80	19.80	****	0.55
131	3	1299	1.95	17.80	5.73	36.00	0	0	96	66	0.618	0.0	23.10	23.10	****	0.65
131	4	1300	1.95	17.80	5.73	36.00	0	0	98	65	0.610	0.0	23.10	23.10	****	0.65
131	5	1301	1.95	17.80	5.73	36.00	0	0	98	65	0.610	0.0	26.40	26.40	****	0.74
131	6	1302	1.95	17.80	5.73	36.00	0	0	99	64	0.594	0.0	23.10	23.10	****	0.66
131	7	1303	1.95	17.80	5.73	19.88	0	0	99	64	0.594	4.68	29.70	25.02	0.95	0.71
131	8	1304	1.95	17.80	14.55	3.92	0	0	99	64	0.594	21.06	46.20	25.14	0.92	0.71
131	9	1305	1.95	17.80	27.49	2.16	2	2	85	72	0.672	39.00	72.60	33.60	****	0.90
131	10	1306	1.95	17.80	40.59	1.53	6	6	70	75	0.612	59.28	82.50	23.22	****	0.61
131	11	1307	1.95	17.80	53.65	1.24	5	5	65	79	0.649	39.00	99.00	60.00	****	****
131	12	1308	1.95	17.80	66.26	1.09	4	4	53	82	0.584	******	128.70	******	****	****
131	13	1309	1.95	17.80	76.68	1.03	4	4	45	86	0.564	******	141.90	******	****	****
131	14	1310	1.95	17.80	77.05	1.03	4	4	44	86	0.551	******	122.10	******	****	****
131	15	1311	1.95	17.80	66.89	1.09	4	4	42	86	0.526	******	112.20	******	****	****
131	16	1312	1.95	17.80	54.33	1.23	3	3	42	88	0.561	42.90	95.70	52.80	****	****
131	17	1313	1.95	17.80	41.28	1.51	2	2	40	89	0.551	31.20	89.10	57.90	****	****
131	18	1314	1.95	17.80	28.18	2.11	2	2	40	89	0.551	19.50	59.40	39.90	****	0.94
131	19	1315	1.95	17.80	15.23	3.75	1	1	45	85	0.546	7.80	39.60	31.80	****	0.77
131	20	1316	1.95	17.80	5.73	16.77	1	1	53	80	0.547	0.78	26.40	25.62	****	0.65
131	21	1317	1.95	17.80	5.73	36.00	0	0	63	75	0.551	0.0	******	******	****	****
131	22	1318	1.95	17.80	5.73	36.00	0	0	70	74	0.592	0.0	******	******	****	****
131	23	1319	1.95	17.80	5.73	36.00	0	0	77	72	0.609	0.0	******	******	****	****
131	24	1320	1.95	17.80	5.73	36.00	0	0	82	70	0.606	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
132	1	1321	1.95	18.00	5.73	36.00	0	0	86	68	0.593	0.0	23.10	23.10	****	0.64
132	2	1322	1.95	18.00	5.73	36.00	0	0	91	67	0.607	0.0	23.10	23.10	****	0.64
132	3	1323	1.95	18.00	5.73	36.00	0	0	96	66	0.618	0.0	23.10	23.10	****	0.65
132	4	1324	1.95	18.00	5.73	36.00	0	0	97	66	0.625	0.0	23.10	23.10	****	0.65
132	5	1325	1.95	18.00	5.73	36.00	0	0	97	65	0.603	0.0	23.10	23.10	****	0.65
132	6	1326	1.95	18.00	5.73	36.00	0	0	98	64	0.588	0.0	26.40	26.40	****	0.75
132	7	1327	1.95	18.00	5.73	19.45	0	0	100	64	0.600	4.68	26.40	21.72	0.95	0.62
132	8	1328	1.95	18.00	14.62	3.90	0	0	100	66	0.644	21.84	49.50	27.66	0.93	0.77
132	9	1329	1.95	18.00	27.55	2.15	0	0	85	73	0.695	39.00	75.90	36.90	0.86	0.98
132	10	1330	1.95	18.00	40.64	1.53	0	0	75	75	0.656	54.60	99.00	44.40	0.80	****
132	11	1331	1.95	18.00	53.71	1.24	0	0	55	79	0.549	66.30	118.80	52.50	0.75	****
132	12	1332	1.95	18.00	66.35	1.09	0	0	47	85	0.571	******	132.00	******	****	****
132	13	1333	1.95	18.00	76.83	1.03	1	1	45	86	0.564	******	138.60	******	****	****
132	14	1334	1.95	18.00	77.24	1.02	1	1	45	89	0.620	******	132.00	******	****	****
132	15	1335	1.95	18.00	67.02	1.09	1	1	38	91	0.557	******	******	******	****	****
132	16	1336	1.95	18.00	54.44	1.23	0	0	34	91	0.499	******	******	******	****	****
132	17	1337	1.95	18.00	41.38	1.51	0	0	34	92	0.515	******	******	******	****	****
132	18	1338	1.95	18.00	28.28	2.10	0	0	34	91	0.499	******	******	******	****	****
132	19	1339	1.95	18.00	15.34	3.73	0	0	40	86	0.501	******	******	******	****	****
132	20	1340	1.95	18.00	5.73	16.28	0	0	49	80	0.506	******	******	******	****	****
132	21	1341	1.95	18.00	5.73	36.00	0	0	55	76	0.498	0.0	******	******	****	****
132	22	1342	1.95	18.00	5.73	36.00	0	0	61	74	0.516	0.0	******	******	****	****
132	23	1343	1.95	18.00	5.73	36.00	0	0	69	72	0.546	0.0	******	******	****	****
132	24	1344	1.95	18.00	5.73	36.00	0	0	76	69	0.543	0.0	******	******	****	****
133	1	1345	1.95	18.30	5.73	36.00	0	0	86	67	0.574	0.0	******	******	****	****
133	2	1346	1.95	18.30	5.73	36.00	0	0	91	66	0.586	0.0	******	******	****	****
133	3	1347	1.95	18.30	5.73	36.00	0	0	93	65	0.578	0.0	******	******	****	****
133	4	1348	1.95	18.30	5.73	36.00	0	0	96	64	0.576	0.0	******	******	****	****
133	5	1349	1.95	18.30	5.73	36.00	0	0	98	63	0.568	0.0	******	******	****	****
133	6	1350	1.95	18.30	5.73	36.00	0	0	99	63	0.574	0.0	******	******	****	****
133	7	1351	1.95	18.30	5.73	18.69	0	0	99	62	0.554	******	******	******	****	****
133	8	1352	1.95	18.30	14.75	3.87	0	0	100	66	0.644	******	******	******	****	****
133	9	1353	1.95	18.30	27.67	2.14	0	0	90	72	0.712	******	******	******	****	****
133	10	1354	1.95	18.30	40.76	1.53	0	0	70	76	0.633	******	******	******	****	****
133	11	1355	1.95	18.30	53.84	1.24	0	0	60	79	0.599	******	******	******	****	****
133	12	1356	1.95	18.30	66.50	1.09	0	0	44	85	0.534	******	******	******	****	****
133	13	1357	1.95	18.30	77.09	1.03	0	0	43	88	0.574	******	******	******	****	****
133	14	1358	1.95	18.30	77.50	1.02	1	1	39	90	0.555	79.56	******	******	****	****
133	15	1359	1.95	18.30	67.18	1.08	1	1	37	92	0.560	74.10	128.70	54.60	****	****
133	16	1360	1.95	18.30	54.56	1.23	1	1	36	92	0.545	65.52	115.50	49.98	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
133	17	1361	1.95	18.30	41.50	1.51	1	1	33	93	0.515	49.14	89.10	39.96	****	0.92
133	18	1362	1.95	18.30	28.40	2.09	0	0	34	92	0.515	31.20	66.00	34.80	0.76	0.80
133	19	1363	1.95	18.30	15.47	3.70	0	0	36	88	0.481	17.16	42.90	25.74	0.85	0.61
133	20	1364	1.95	18.30	5.73	15.72	0	0	51	82	0.562	1.56	26.40	24.84	0.88	0.62
133	21	1365	1.95	18.30	5.73	36.00	0	0	58	78	0.561	0.0	23.10	23.10	****	0.59
133	22	1366	1.95	18.30	5.73	36.00	0	0	59	75	0.516	0.0	23.10	23.10	****	0.60
133	23	1367	1.95	18.30	5.73	36.00	0	0	62	72	0.490	0.0	23.10	23.10	****	0.62
133	24	1368	1.95	18.30	5.73	36.00	0	0	70	70	0.517	0.0	23.10	23.10	****	0.63
134	1	1369	1.95	18.50	5.73	36.00	0	0	80	70	0.591	0.0	23.10	23.10	****	0.63
134	2	1370	1.95	18.50	5.73	36.00	0	0	85	68	0.586	0.0	23.10	23.10	****	0.64
134	3	1371	1.95	18.50	5.73	36.00	0	0	91	67	0.607	0.0	23.10	23.10	****	0.64
134	4	1372	1.95	18.50	5.73	36.00	0	0	93	66	0.599	0.0	23.10	23.10	****	0.65
134	5	1373	1.95	18.50	5.73	36.00	0	0	96	66	0.618	0.0	23.10	23.10	****	0.65
134	6	1374	1.95	18.50	5.73	36.00	0	0	97	65	0.603	0.0	23.10	23.10	****	0.65
134	7	1375	1.95	18.50	5.73	18.20	0	0	98	65	0.610	0.78	29.70	28.92	0.86	0.82
134	8	1376	1.95	18.50	14.84	3.85	0	0	99	67	0.660	13.26	42.90	29.64	0.81	0.82
134	9	1377	1.95	18.50	27.75	2.14	0	0	90	75	0.787	30.42	72.60	42.18	0.76	****
134	10	1378	1.95	18.50	40.84	1.53	0	0	72	76	0.652	46.80	95.70	48.90	0.72	****
134	11	1379	1.95	18.50	53.92	1.24	0	0	60	80	0.619	60.84	115.50	54.66	0.70	****
134	12	1380	1.95	18.50	66.61	1.09	0	0	48	85	0.583	70.98	135.30	64.32	0.68	****
134	13	1381	1.95	18.50	77.26	1.02	0	0	42	89	0.579	75.66	135.30	59.64	0.67	****
134	14	1382	1.95	18.50	77.68	1.02	0	0	42	91	0.616	75.66	135.30	59.64	0.67	****
134	15	1383	1.95	18.50	67.29	1.08	0	0	36	92	0.545	72.54	125.40	52.86	0.69	****
134	16	1384	1.95	18.50	54.65	1.22	0	0	35	93	0.546	63.18	115.50	52.32	0.71	****
134	17	1385	1.95	18.50	41.58	1.50	0	0	36	94	0.580	50.70	92.40	41.70	0.75	0.95
134	18	1386	1.95	18.50	28.48	2.09	0	0	38	92	0.575	35.10	66.00	30.90	0.80	0.71
134	19	1387	1.95	18.50	15.55	3.68	0	0	39	90	0.555	15.60	42.90	27.30	0.83	0.64
134	20	1388	1.95	18.50	5.73	15.36	0	0	45	85	0.546	2.34	26.40	24.06	0.90	0.58
134	21	1389	1.95	18.50	5.73	36.00	0	0	52	81	0.554	0.0	23.10	23.10	****	0.58
134	22	1390	1.95	18.50	5.73	36.00	0	0	60	78	0.580	0.0	23.10	23.10	****	0.59
134	23	1391	1.95	18.50	5.73	36.00	0	0	68	76	0.615	0.0	23.10	23.10	****	0.60
134	24	1392	1.95	18.50	5.73	36.00	0	0	67	75	0.586	0.0	23.10	23.10	****	0.60
135	1	1393	1.95	18.80	5.73	36.00	0	0	72	72	0.570	0.0	23.10	23.10	****	0.62
135	2	1394	1.95	18.80	5.73	36.00	0	0	80	70	0.591	0.0	23.10	23.10	****	0.63
135	3	1395	1.95	18.80	5.73	36.00	0	0	85	70	0.628	0.0	23.10	23.10	****	0.63
135	4	1396	1.95	18.80	5.73	36.00	0	0	87	68	0.600	0.0	23.10	23.10	****	0.64
135	5	1397	1.95	18.80	5.73	36.00	0	0	92	68	0.635	0.0	23.10	23.10	****	0.64
135	6	1398	1.95	18.80	5.73	36.00	0	0	95	67	0.634	0.0	23.10	23.10	****	0.64
135	7	1399	1.95	18.80	5.73	17.52	0	0	98	67	0.654	0.78	29.70	28.92	0.86	0.80
135	8	1400	1.95	18.80	14.97	3.82	0	0	98	68	0.676	13.26	42.90	29.64	0.81	0.82

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
135	9	1401	1.95	18.80	27.87	2.13	0	0	85	75	0.744	28.86	72.60	43.74	0.74	****
135	10	1402	1.95	18.80	40.95	1.52	0	0	75	77	0.701	45.24	92.40	47.16	0.71	****
135	11	1403	1.95	18.80	54.04	1.23	0	0	68	79	0.679	58.50	112.20	53.70	0.68	****
135	12	1404	1.95	18.80	66.76	1.09	0	0	60	85	0.728	68.64	125.40	56.76	0.66	****
135	13	1405	1.95	18.80	77.51	1.02	2	2	50	90	0.711	71.76	128.70	56.94	****	****
135	14	1406	1.95	18.80	77.93	1.02	3	3	48	91	0.704	73.32	125.40	52.08	****	****
135	15	1407	1.95	18.80	67.45	1.08	2	2	42	92	0.636	72.54	132.00	59.46	****	****
135	16	1408	1.95	18.80	54.77	1.22	2	2	43	93	0.671	61.62	112.20	50.58	****	****
135	17	1409	1.95	18.80	41.69	1.50	7	5	44	90	0.626	31.20	66.00	34.80	****	0.82
135	18	1410	1.95	18.80	28.60	2.08	9	7	46	89	0.634	13.26	46.20	32.94	****	0.78
135	19	1411	1.95	18.80	15.69	3.65	8	6	54	84	0.634	10.14	36.30	26.16	****	0.64
135	20	1412	1.95	18.80	5.73	14.85	7	4	60	81	0.640	2.34	23.10	20.76	****	0.52
135	21	1413	1.95	18.80	5.73	36.00	5	3	68	78	0.658	0.0	23.10	23.10	****	0.59
135	22	1414	1.95	18.80	5.73	36.00	3	2	72	77	0.673	0.0	23.10	23.10	****	0.60
135	23	1415	1.95	18.80	5.73	36.00	3	2	72	76	0.652	0.0	23.10	23.10	****	0.60
135	24	1416	1.95	18.80	5.73	36.00	0	0	70	76	0.633	0.0	23.10	23.10	****	0.60
136	1	1417	1.95	19.00	5.73	36.00	0	0	73	74	0.618	0.0	23.10	23.10	****	0.61
136	2	1418	1.95	19.00	5.73	36.00	0	0	80	72	0.633	0.0	23.10	23.10	****	0.62
136	3	1419	1.95	19.00	5.73	36.00	0	0	85	70	0.628	0.0	23.10	23.10	****	0.63
136	4	1420	1.95	19.00	5.73	36.00	0	0	88	70	0.650	0.0	23.10	23.10	****	0.63
136	5	1421	1.95	19.00	5.73	36.00	0	0	92	68	0.635	0.0	23.10	23.10	****	0.64
136	6	1422	1.95	19.00	5.73	36.00	0	0	95	67	0.634	0.0	23.10	23.10	****	0.64
136	7	1423	1.95	19.00	5.73	17.09	0	0	96	67	0.640	1.56	29.70	28.14	0.89	0.78
136	8	1424	1.95	19.00	15.06	3.79	0	0	93	69	0.664	12.48	42.90	30.42	0.79	0.83
136	9	1425	1.95	19.00	27.95	2.12	0	0	85	73	0.695	28.86	72.60	43.74	0.74	****
136	10	1426	1.95	19.00	41.03	1.52	0	0	75	76	0.679	45.24	95.70	50.46	0.71	****
136	11	1427	1.95	19.00	54.12	1.23	0	0	65	80	0.671	59.28	115.50	56.22	0.68	****
136	12	1428	1.95	19.00	66.86	1.09	0	0	52	84	0.611	67.08	******	******	0.65	****
136	13	1429	1.95	19.00	77.67	1.02	0	0	48	88	0.641	74.10	******	******	0.65	****
136	14	1430	1.95	19.00	78.10	1.02	0	0	46	90	0.654	75.66	******	******	0.67	****
136	15	1431	1.95	19.00	67.55	1.08	5	3	42	90	0.597	70.20	******	******	****	****
136	16	1432	1.95	19.00	54.85	1.22	8	5	41	92	0.621	59.28	******	******	****	****
136	17	1433	1.95	19.00	41.77	1.50	7	3	41	92	0.621	46.02	******	******	****	****
136	18	1434	1.95	19.00	28.68	2.08	7	3	41	92	0.621	35.10	******	******	****	****
136	19	1435	1.95	19.00	15.77	3.63	7	3	43	87	0.556	13.26	42.90	29.64	****	0.71
136	20	1436	1.95	19.00	5.73	14.53	8	5	52	85	0.631	0.78	26.40	25.62	****	0.62
136	21	1437	1.95	19.00	5.73	36.00	10	8	90	72	0.712	0.0	******	******	****	****
136	22	1438	1.95	19.00	5.73	36.00	8	6	100	69	0.714	0.0	******	******	****	****
136	23	1439	1.95	19.00	5.73	36.00	4	3	100	68	0.690	0.0	******	******	****	****
136	24	1440	1.95	19.00	5.73	36.00	0	0	100	68	0.690	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
137	1	1441	1.95	19.20	5.73	36.00	4	3	100	68	0.690	0.0	33.00	33.00	****	0.91
137	2	1442	1.95	19.20	5.73	36.00	8	6	100	68	0.690	0.0	33.00	33.00	****	0.91
137	3	1443	1.95	19.20	5.73	36.00	9	7	100	68	0.690	0.0	33.00	33.00	****	0.91
137	4	1444	1.95	19.20	5.73	36.00	9	7	100	68	0.690	0.0	33.00	33.00	****	0.91
137	5	1445	1.95	19.20	5.73	36.00	8	6	100	67	0.667	0.0	33.00	33.00	****	0.92
137	6	1446	1.95	19.20	5.73	36.00	8	6	100	67	0.667	0.0	33.00	33.00	****	0.92
137	7	1447	1.95	19.20	5.73	16.67	10	10	100	67	0.667	0.78	33.00	32.22	****	0.90
137	8	1448	1.95	19.20	15.14	3.77	10	10	100	68	0.690	4.68	39.60	34.92	****	0.96
137	9	1449	1.95	19.20	28.03	2.12	10	10	99	70	0.732	9.36	46.20	36.84	****	****
137	10	1450	1.95	19.20	41.11	1.52	10	9	92	72	0.728	18.72	59.40	40.68	****	****
137	11	1451	1.95	19.20	54.20	1.23	10	9	88	76	0.796	35.10	85.80	50.70	****	****
137	12	1452	1.95	19.20	66.96	1.09	9	8	80	78	0.774	39.00	85.80	46.80	****	****
137	13	1453	1.95	19.20	77.84	1.02	9	8	75	82	0.826	******	118.80	******	****	****
137	14	1454	1.95	19.20	78.27	1.02	9	8	55	85	0.668	******	******	******	****	****
137	15	1455	1.95	19.20	67.65	1.08	7	6	60	84	0.705	46.80	******	******	****	****
137	16	1456	1.95	19.20	54.93	1.22	10	9	55	82	0.606	27.30	******	******	****	****
137	17	1457	1.95	19.20	41.84	1.50	10	10	60	75	0.525	4.68	******	******	****	****
137	18	1458	1.95	19.20	28.76	2.07	10	10	96	71	0.733	2.34	33.00	30.66	****	0.83
137	19	1459	1.95	19.20	15.86	3.61	9	8	98	72	0.775	9.36	36.30	26.94	****	0.72
137	20	1460	1.95	19.20	5.73	14.22	9	8	97	71	0.741	1.56	33.00	31.44	****	0.85
137	21	1461	1.95	19.20	5.73	36.00	7	6	97	71	0.741	0.0	33.00	33.00	****	0.89
137	22	1462	1.95	19.20	5.73	36.00	8	8	97	70	0.717	0.0	33.00	33.00	****	0.90
137	23	1463	1.95	19.20	5.73	36.00	8	8	97	70	0.717	0.0	33.00	33.00	****	0.90
137	24	1464	1.95	19.20	5.73	36.00	4	2	97	70	0.717	0.0	33.00	33.00	****	0.90
138	1	1465	1.95	19.40	5.73	36.00	3	1	98	69	0.700	0.0	31.26	31.26	****	0.86
138	2	1466	1.95	19.40	5.73	36.00	2	1	98	68	0.676	0.0	31.26	31.26	****	0.86
138	3	1467	1.95	19.40	5.73	36.00	6	5	98	68	0.676	0.0	31.26	31.26	****	0.86
138	4	1468	1.95	19.40	5.73	36.00	6	5	98	68	0.676	0.0	31.26	31.26	****	0.86
138	5	1469	1.95	19.40	5.73	36.00	8	3	98	67	0.654	0.0	31.26	31.26	****	0.87
138	6	1470	1.95	19.40	5.73	36.00	10	3	98	67	0.654	0.0	31.26	31.26	****	0.87
138	7	1471	1.95	19.40	5.73	16.27	7	2	98	68	0.676	0.0	33.78	33.78	****	0.93
138	8	1472	1.95	19.40	15.23	3.75	7	2	98	68	0.676	10.92	49.50	38.58	****	****
138	9	1473	1.95	19.40	28.11	2.11	8	7	90	74	0.761	28.08	72.60	44.52	****	****
138	10	1474	1.95	19.40	41.18	1.52	6	6	82	76	0.742	39.78	89.10	49.32	****	****
138	11	1475	1.95	19.40	54.28	1.23	6	6	73	78	0.706	49.92	102.30	52.38	****	****
138	12	1476	1.95	19.40	67.06	1.09	6	6	65	82	0.716	68.64	125.40	56.76	****	****
138	13	1477	1.95	19.40	78.00	1.02	8	8	63	82	0.694	******	108.90	******	****	****
138	14	1478	1.95	19.40	78.44	1.02	7	7	62	82	0.683	******	108.90	******	****	****
138	15	1479	1.95	19.40	67.75	1.08	9	7	60	82	0.661	60.84	112.20	51.36	****	****
138	16	1480	1.95	19.40	55.01	1.22	9	7	60	82	0.661	50.70	99.00	48.30	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
138	17	1481	1.95	19.40	41.92	1.49	8	5	62	80	0.640	46.80	75.90	29.10	****	0.73
138	18	1482	1.95	19.40	28.84	2.07	8	6	64	78	0.619	37.44	59.40	21.96	****	0.56
138	19	1483	1.95	19.40	15.95	3.59	8	6	68	74	0.575	24.96	39.60	14.64	****	0.39
138	20	1484	1.95	19.40	5.73	13.92	6	3	74	73	0.605	14.04	29.70	15.66	****	0.42
138	21	1485	1.95	19.40	5.73	36.00	8	4	78	71	0.596	0.0	29.70	29.70	****	0.80
138	22	1486	1.95	19.40	5.73	36.00	9	4	82	70	0.606	0.0	31.26	31.26	****	0.85
138	23	1487	1.95	19.40	5.73	36.00	6	2	84	70	0.621	0.0	31.26	31.26	****	0.85
138	24	1488	1.95	19.40	5.73	36.00	7	3	86	69	0.614	0.0	31.26	31.26	****	0.86
139	1	1489	1.95	19.60	5.73	36.00	9	4	90	68	0.621	0.0	******	******	****	****
139	2	1490	1.95	19.60	5.73	36.00	9	4	92	66	0.592	0.0	******	******	****	****
139	3	1491	1.95	19.60	5.73	36.00	6	2	93	66	0.599	0.0	******	******	****	****
139	4	1492	1.95	19.60	5.73	36.00	8	3	94	65	0.585	0.0	******	******	****	****
139	5	1493	1.95	19.60	5.73	36.00	5	2	95	65	0.591	0.0	******	******	****	****
139	6	1494	1.95	19.60	5.73	36.00	7	3	96	65	0.597	0.0	******	******	****	****
139	7	1495	1.95	19.60	5.73	15.89	8	5	95	66	0.612	******	33.00	******	****	****
139	8	1496	1.95	19.60	15.32	3.73	9	6	90	70	0.665	******	46.20	******	****	****
139	9	1497	1.95	19.60	28.19	2.11	9	8	80	72	0.633	******	66.00	******	****	****
139	10	1498	1.95	19.60	41.26	1.51	9	8	70	76	0.633	******	75.90	******	****	****
139	11	1499	1.95	19.60	54.35	1.23	9	9	62	78	0.600	******	89.10	******	****	****
139	12	1500	1.95	19.60	67.15	1.08	9	8	58	78	0.561	******	85.80	******	****	****
139	13	1501	1.95	19.60	78.16	1.02	8	6	50	84	0.587	******	118.80	******	****	****
139	14	1502	1.95	19.60	78.61	1.02	8	5	52	82	0.573	******	125.40	******	****	****
139	15	1503	1.95	19.60	67.85	1.08	8	5	50	83	0.569	******	102.30	******	****	****
139	16	1504	1.95	19.60	55.09	1.22	8	5	48	84	0.564	******	102.30	******	****	****
139	17	1505	1.95	19.60	41.99	1.49	8	6	52	80	0.537	******	75.90	******	****	****
139	18	1506	1.95	19.60	28.92	2.06	7	6	54	81	0.576	******	56.10	******	****	****
139	19	1507	1.95	19.60	16.03	3.58	5	5	56	76	0.507	******	42.90	******	****	****
139	20	1508	1.95	19.60	5.73	13.64	3	3	60	73	0.491	******	29.70	******	****	****
139	21	1509	1.95	19.60	5.73	36.00	5	5	68	70	0.503	0.0	******	******	****	****
139	22	1510	1.95	19.60	5.73	36.00	4	4	72	69	0.514	0.0	******	******	****	****
139	23	1511	1.95	19.60	5.73	36.00	3	3	79	68	0.545	0.0	******	******	****	****
139	24	1512	1.95	19.60	5.73	36.00	2	2	82	67	0.547	0.0	******	******	****	****
140	1	1513	1.95	19.80	5.73	36.00	2	2	85	67	0.567	0.0	******	******	****	****
140	2	1514	1.95	19.80	5.73	36.00	3	3	87	66	0.560	0.0	******	******	****	****
140	3	1515	1.95	19.80	5.73	36.00	4	2	90	65	0.560	0.0	******	******	****	****
140	4	1516	1.95	19.80	5.73	36.00	3	2	92	65	0.572	0.0	******	******	****	****
140	5	1517	1.95	19.80	5.73	36.00	2	1	94	64	0.564	0.0	******	******	****	****
140	6	1518	1.95	19.80	5.73	36.00	1	1	95	63	0.551	0.0	******	******	****	****
140	7	1519	1.95	19.80	5.73	15.45	1	1	96	64	0.576	******	29.70	******	****	****
140	8	1520	1.95	19.80	15.43	3.71	1	1	91	69	0.650	******	46.20	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
140	9	1521	1.95	19.80	28.29	2.10	8	4	75	75	0.656	******	82.50	******	****	****
140	10	1522	1.95	19.80	41.35	1.51	8	4	70	77	0.654	******	99.00	******	****	****
140	11	1523	1.95	19.80	54.45	1.23	8	3	63	80	0.650	******	115.50	******	****	****
140	12	1524	1.95	19.80	67.27	1.08	5	3	50	83	0.569	******	125.40	******	****	****
140	13	1525	1.95	19.80	78.34	1.02	3	1	48	85	0.583	******	141.90	******	****	****
140	14	1526	1.95	19.80	78.77	1.02	2	1	46	87	0.595	******	138.60	******	****	****
140	15	1527	1.95	19.80	67.92	1.08	2	1	43	88	0.574	73.32	132.00	58.68	****	****
140	16	1528	1.95	19.80	55.14	1.22	4	2	43	89	0.593	64.74	118.80	54.06	****	****
140	17	1529	1.95	19.80	42.05	1.49	4	2	47	88	0.627	48.36	89.10	40.74	****	0.97
140	18	1530	1.95	19.80	28.97	2.06	4	2	50	84	0.587	25.74	59.40	33.66	****	0.82
140	19	1531	1.95	19.80	16.10	3.56	4	2	55	80	0.568	12.48	42.90	30.42	****	0.77
140	20	1532	1.95	19.80	5.73	13.42	3	1	65	75	0.569	0.78	26.40	25.62	****	0.67
140	21	1533	1.95	19.80	5.73	36.00	3	1	75	73	0.613	0.0	23.10	23.10	****	0.61
140	22	1534	1.95	19.80	5.73	36.00	3	1	80	71	0.611	0.0	23.10	23.10	****	0.62
140	23	1535	1.95	19.80	5.73	36.00	3	1	86	70	0.636	0.0	23.10	23.10	****	0.63
140	24	1536	1.95	19.80	5.73	36.00	0	0	90	68	0.621	0.0	23.10	23.10	****	0.64
141	1	1537	1.95	20.00	5.73	36.00	3	1	92	68	0.635	0.0	23.10	23.10	****	0.64
141	2	1538	1.95	20.00	5.73	36.00	3	1	94	67	0.627	0.0	23.10	23.10	****	0.64
141	3	1539	1.95	20.00	5.73	36.00	0	0	95	66	0.612	0.0	23.10	23.10	****	0.65
141	4	1540	1.95	20.00	5.73	36.00	0	0	97	65	0.603	0.0	23.10	23.10	****	0.65
141	5	1541	1.95	20.00	5.73	36.00	0	0	98	64	0.588	0.0	23.10	23.10	****	0.66
141	6	1542	1.95	20.00	5.73	36.00	0	0	98	63	0.568	0.0	23.10	23.10	****	0.66
141	7	1543	1.95	20.00	5.73	15.10	0	0	98	65	0.610	7.80	26.40	18.60	0.97	0.52
141	8	1544	1.95	20.00	15.51	3.69	0	0	92	69	0.657	25.74	49.50	23.76	0.95	0.65
141	9	1545	1.95	20.00	28.37	2.10	2	1	78	75	0.682	41.34	79.20	37.86	****	0.99
141	10	1546	1.95	20.00	41.43	1.51	0	0	71	77	0.664	56.94	102.30	45.36	0.82	****
141	11	1547	1.95	20.00	54.53	1.23	0	0	60	80	0.619	69.42	118.80	49.38	0.77	****
141	12	1548	1.95	20.00	67.36	1.08	0	0	51	85	0.619	75.66	135.30	59.64	0.72	****
141	13	1549	1.95	20.00	78.50	1.02	0	0	45	88	0.601	78.00	141.90	63.90	0.69	****
141	14	1550	1.95	20.00	78.93	1.02	0	0	40	90	0.569	75.66	135.30	59.64	0.67	****
141	15	1551	1.95	20.00	68.02	1.08	0	0	38	92	0.575	67.86	128.70	60.84	0.65	****
141	16	1552	1.95	20.00	55.22	1.22	0	0	36	92	0.545	56.94	112.20	55.26	0.65	****
141	17	1553	1.95	20.00	42.12	1.49	0	0	35	92	0.530	42.12	92.40	50.28	0.66	****
141	18	1554	1.95	20.00	29.05	2.05	0	0	36	90	0.512	24.96	62.70	37.74	0.67	0.88
141	19	1555	1.95	20.00	16.18	3.54	0	0	39	85	0.473	7.80	42.90	35.10	0.67	0.85
141	20	1556	1.95	20.00	5.73	13.15	0	0	45	79	0.450	0.78	26.40	25.62	0.81	0.65
141	21	1557	1.95	20.00	5.73	36.00	0	0	57	74	0.482	0.0	23.10	23.10	****	0.61
141	22	1558	1.95	20.00	5.73	36.00	0	0	70	73	0.573	0.0	23.10	23.10	****	0.61
141	23	1559	1.95	20.00	5.73	36.00	0	0	80	70	0.591	0.0	23.10	23.10	****	0.63
141	24	1560	1.95	20.00	5.73	36.00	0	0	88	70	0.650	0.0	23.10	23.10	****	0.63

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
142	1	1561	1.95	20.20	5.73	36.00	0	0	95	69	0.678	0.0	23.10	23.10	****	0.63
142	2	1562	1.95	20.20	5.73	36.00	0	0	96	68	0.662	0.0	26.40	26.40	****	0.73
142	3	1563	1.95	20.20	5.73	36.00	0	0	96	68	0.662	0.0	26.40	26.40	****	0.73
142	4	1564	1.95	20.20	5.73	36.00	0	0	97	67	0.647	0.0	26.40	26.40	****	0.73
142	5	1565	1.95	20.20	5.73	36.00	4	2	99	66	0.638	0.0	26.40	26.40	****	0.74
142	6	1566	1.95	20.20	5.73	36.00	6	2	98	67	0.654	0.0	26.40	26.40	****	0.73
142	7	1567	1.95	20.20	5.73	14.77	5	2	98	68	0.676	3.90	33.00	29.10	****	0.80
142	8	1568	1.95	20.20	15.60	3.67	5	3	93	70	0.687	19.50	42.90	23.40	****	0.64
142	9	1569	1.95	20.20	28.44	2.09	1	1	85	77	0.795	36.66	66.00	29.34	****	0.76
142	10	1570	1.95	20.20	41.50	1.51	0	0	70	80	0.722	53.82	95.70	41.88	0.79	****
142	11	1571	1.95	20.20	54.61	1.23	0	0	57	84	0.670	63.96	115.50	51.54	0.72	****
142	12	1572	1.95	20.20	67.46	1.08	3	2	53	87	0.685	62.40	118.80	56.40	****	****
142	13	1573	1.95	20.20	78.66	1.02	3	2	49	88	0.654	65.52	112.20	46.68	****	****
142	14	1574	1.95	20.20	79.10	1.02	3	2	45	88	0.601	54.60	108.90	54.30	****	****
142	15	1575	1.95	20.20	68.11	1.08	6	6	45	88	0.601	48.36	99.00	50.64	****	****
142	16	1576	1.95	20.20	55.29	1.22	5	5	46	88	0.614	42.90	89.10	46.20	****	****
142	17	1577	1.95	20.20	42.19	1.49	3	3	48	87	0.621	35.10	******	******	****	****
142	18	1578	1.95	20.20	29.13	2.05	0	0	49	86	0.614	18.72	******	******	0.58	****
142	19	1579	1.95	20.20	16.27	3.53	0	0	53	82	0.584	3.90	******	******	0.55	****
142	20	1580	1.95	20.20	5.73	12.89	0	0	60	79	0.599	0.0	******	******	****	****
142	21	1581	1.95	20.20	5.73	36.00	0	0	70	76	0.633	0.0	******	******	****	****
142	22	1582	1.95	20.20	5.73	36.00	0	0	78	74	0.660	0.0	******	******	****	****
142	23	1583	1.95	20.20	5.73	36.00	0	0	82	74	0.694	0.0	******	******	****	****
142	24	1584	1.95	20.20	5.73	36.00	0	0	86	72	0.680	0.0	******	******	****	****
143	1	1585	1.95	20.40	5.73	36.00	0	0	92	70	0.680	0.0	26.40	26.40	****	0.72
143	2	1586	1.95	20.40	5.73	36.00	0	0	94	69	0.671	0.0	26.40	26.40	****	0.72
143	3	1587	1.95	20.40	5.73	36.00	10	2	95	69	0.678	0.0	26.40	26.40	****	0.72
143	4	1588	1.95	20.40	5.73	36.00	10	3	97	68	0.669	0.0	26.40	26.40	****	0.73
143	5	1589	1.95	20.40	5.73	36.00	10	3	98	67	0.654	0.0	26.40	26.40	****	0.73
143	6	1590	1.95	20.40	5.73	36.00	2	1	98	67	0.654	0.0	26.40	26.40	****	0.73
143	7	1591	1.95	20.40	5.73	14.38	2	1	98	68	0.676	8.58	29.70	21.12	****	0.58
143	8	1592	1.95	20.40	15.71	3.65	0	0	91	70	0.672	25.74	42.90	17.16	0.95	0.47
143	9	1593	1.95	20.40	28.54	2.08	5	5	82	75	0.717	42.12	82.50	40.38	****	****
143	10	1594	1.95	20.40	41.60	1.50	7	7	71	78	0.687	45.24	******	******	****	****
143	11	1595	1.95	20.40	54.70	1.22	8	7	60	80	0.619	46.80	******	******	****	****
143	12	1596	1.95	20.40	67.57	1.08	6	5	50	84	0.587	******	******	******	****	****
143	13	1597	1.95	20.40	78.83	1.02	6	5	45	85	0.546	******	******	******	****	****
143	14	1598	1.95	20.40	79.25	1.02	6	5	45	88	0.601	******	******	******	****	****
143	15	1599	1.95	20.40	68.19	1.08	6	6	45	88	0.601	74.10	******	******	****	****
143	16	1600	1.95	20.40	55.35	1.21	6	3	46	87	0.595	50.70	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
143	17	1601	1.95	20.40	42.24	1.48	7	3	46	87	0.595	34.32	******	******	****	****
143	18	1602	1.95	20.40	29.18	2.04	10	4	46	86	0.576	23.40	62.70	39.30	****	0.95
143	19	1603	1.95	20.40	16.34	3.51	10	4	46	83	0.523	7.80	42.90	35.10	****	0.87
143	20	1604	1.95	20.40	5.73	12.69	10	3	51	79	0.509	0.78	29.70	28.92	****	0.73
143	21	1605	1.95	20.40	5.73	36.00	10	3	64	76	0.579	0.0	26.40	26.40	****	0.69
143	22	1606	1.95	20.40	5.73	36.00	6	2	71	74	0.601	0.0	26.40	26.40	****	0.70
143	23	1607	1.95	20.40	5.73	36.00	3	1	79	72	0.625	0.0	26.40	26.40	****	0.71
143	24	1608	1.95	20.40	5.73	36.00	3	1	86	70	0.636	0.0	******	******	****	****
144	1	1609	1.94	20.60	5.73	36.00	0	0	90	69	0.643	0.0	27.18	27.18	****	0.74
144	2	1610	1.94	20.60	5.73	36.00	0	0	92	68	0.635	0.0	27.18	27.18	****	0.75
144	3	1611	1.94	20.60	5.73	36.00	0	0	93	68	0.642	0.0	27.18	27.18	****	0.75
144	4	1612	1.94	20.60	5.73	36.00	9	0	96	68	0.662	0.0	27.18	27.18	****	0.75
144	5	1613	1.94	20.60	5.73	36.00	9	7	96	68	0.662	0.0	27.18	27.18	****	0.75
144	6	1614	1.94	20.60	5.73	36.00	10	10	95	68	0.655	0.0	29.70	29.70	****	0.82
144	7	1615	1.94	20.60	5.73	14.02	10	4	95	69	0.678	7.02	33.00	25.98	****	0.71
144	8	1616	1.94	20.60	15.81	3.62	10	10	95	73	0.777	13.26	46.20	32.94	****	0.87
144	9	1617	1.94	20.60	28.64	2.08	10	10	87	75	0.761	14.82	52.80	37.98	****	0.99
144	10	1618	1.94	20.60	41.69	1.50	10	10	85	76	0.769	17.94	46.20	28.26	****	0.73
144	11	1619	1.94	20.60	54.79	1.22	10	10	80	74	0.677	11.70	******	******	****	****
144	12	1620	1.94	20.60	67.68	1.08	10	10	95	70	0.702	7.02	******	******	****	****
144	13	1621	1.94	20.60	79.00	1.02	10	10	99	70	0.732	10.92	******	******	****	****
144	14	1622	1.94	20.60	79.40	1.02	10	10	99	71	0.756	14.82	******	******	****	****
144	15	1623	1.94	20.60	68.26	1.08	10	10	98	72	0.775	10.92	******	******	****	****
144	16	1624	1.94	20.60	55.40	1.21	10	10	98	71	0.749	6.24	******	******	****	****
144	17	1625	1.94	20.60	42.29	1.48	10	10	98	70	0.724	3.12	******	******	****	****
144	18	1626	1.94	20.60	29.24	2.04	10	10	99	70	0.732	1.56	******	******	****	****
144	19	1627	1.94	20.60	16.40	3.50	10	10	99	69	0.707	0.78	******	******	****	****
144	20	1628	1.94	20.60	5.73	12.49	10	10	100	68	0.690	0.0	******	******	****	****
144	21	1629	1.94	20.60	5.73	36.00	10	10	100	66	0.644	0.0	******	******	****	****
144	22	1630	1.94	20.60	5.73	36.00	10	10	100	66	0.644	0.0	******	******	****	****
144	23	1631	1.94	20.60	5.73	36.00	10	10	100	68	0.690	0.0	******	******	****	****
144	24	1632	1.94	20.60	5.73	36.00	10	10	100	68	0.690	0.0	******	******	****	****
145	1	1633	1.94	20.80	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
145	2	1634	1.94	20.80	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
145	3	1635	1.94	20.80	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
145	4	1636	1.94	20.80	5.73	36.00	10	10	100	70	0.739	0.0	******	******	****	****
145	5	1637	1.94	20.80	5.73	36.00	10	10	100	70	0.739	0.0	******	******	****	****
145	6	1638	1.94	20.80	5.73	36.00	9	9	100	70	0.739	0.0	******	******	****	****
145	7	1639	1.94	20.80	5.73	13.67	10	10	100	70	0.739	******	******	******	****	****
145	8	1640	1.94	20.80	15.92	3.60	10	10	97	68	0.669	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
145	9	1641	1.94	20.80	28.74	2.07	10	10	98	68	0.676	******	******	******	****	****
145	10	1642	1.94	20.80	41.78	1.50	10	10	98	70	0.724	******	******	******	****	****
145	11	1643	1.94	20.80	54.89	1.22	10	10	92	72	0.728	******	69.30	******	****	****
145	12	1644	1.94	20.80	67.79	1.08	8	8	82	75	0.717	******	105.60	******	****	****
145	13	1645	1.94	20.80	79.17	1.02	8	8	73	78	0.706	******	115.50	******	****	****
145	14	1646	1.94	20.80	79.54	1.02	9	9	65	80	0.671	******	112.20	******	****	****
145	15	1647	1.94	20.80	68.33	1.08	8	7	62	82	0.683	******	112.20	******	****	****
145	16	1648	1.94	20.80	55.45	1.21	8	7	61	82	0.672	40.17	99.00	58.83	****	****
145	17	1649	1.94	20.80	42.34	1.48	6	6	61	82	0.672	44.07	82.50	38.43	****	0.95
145	18	1650	1.94	20.80	29.30	2.04	3	3	60	81	0.640	23.01	59.40	36.39	****	0.91
145	19	1651	1.94	20.80	16.47	3.49	3	3	64	80	0.660	15.21	49.50	34.29	****	0.86
145	20	1652	1.94	20.80	5.73	12.31	3	3	72	76	0.652	1.17	29.70	28.53	****	0.74
145	21	1653	1.94	20.80	5.73	36.00	2	2	80	75	0.700	0.0	30.09	30.09	****	0.79
145	22	1654	1.94	20.80	5.73	36.00	2	2	85	72	0.672	0.0	26.79	26.79	****	0.72
145	23	1655	1.94	20.80	5.73	36.00	2	2	91	70	0.672	0.0	23.49	23.49	****	0.64
145	24	1656	1.94	20.80	5.73	36.00	4	3	95	69	0.678	0.0	23.49	23.49	****	0.64
146	1	1657	1.94	21.00	5.73	36.00	3	1	96	68	0.662	0.0	26.40	26.40	****	0.73
146	2	1658	1.94	21.00	5.73	36.00	3	1	97	68	0.669	0.0	26.40	26.40	****	0.73
146	3	1659	1.94	21.00	5.73	36.00	3	2	97	68	0.669	0.0	26.40	26.40	****	0.73
146	4	1660	1.94	21.00	5.73	36.00	5	4	98	68	0.676	0.0	29.70	29.70	****	0.82
146	5	1661	1.94	21.00	5.73	36.00	8	6	98	68	0.676	0.0	33.00	33.00	****	0.91
146	6	1662	1.94	21.00	5.73	36.00	9	9	98	68	0.676	0.0	33.00	33.00	****	0.91
146	7	1663	1.94	21.00	5.73	13.33	7	7	98	68	0.676	0.78	39.60	38.82	****	****
146	8	1664	1.94	21.00	16.03	3.58	9	8	98	70	0.724	15.60	49.50	33.90	****	0.92
146	9	1665	1.94	21.00	28.84	2.07	10	9	92	75	0.805	20.28	59.40	39.12	****	****
146	10	1666	1.94	21.00	41.87	1.50	10	9	86	76	0.778	24.18	66.00	41.82	****	****
146	11	1667	1.94	21.00	54.98	1.22	8	6	75	80	0.774	42.90	99.00	56.10	****	****
146	12	1668	1.94	21.00	67.90	1.08	7	5	62	82	0.683	59.28	108.90	49.62	****	****
146	13	1669	1.94	21.00	79.34	1.02	7	5	58	85	0.704	68.64	******	******	****	****
146	14	1670	1.94	21.00	79.69	1.02	7	5	56	86	0.702	74.10	******	******	****	****
146	15	1671	1.94	21.00	68.40	1.07	5	4	53	86	0.664	62.40	******	******	****	****
146	16	1672	1.94	21.00	55.50	1.21	5	4	52	86	0.652	62.40	******	******	****	****
146	17	1673	1.94	21.00	42.39	1.48	4	3	53	86	0.664	43.68	******	******	****	****
146	18	1674	1.94	21.00	29.35	2.03	4	2	55	85	0.668	28.86	******	******	****	****
146	19	1675	1.94	21.00	16.53	3.47	6	2	60	80	0.619	6.24	******	******	****	****
146	20	1676	1.94	21.00	5.73	12.13	7	2	70	77	0.654	0.78	******	******	****	****
146	21	1677	1.94	21.00	5.73	36.00	5	2	76	75	0.665	0.0	******	******	****	****
146	22	1678	1.94	21.00	5.73	36.00	4	1	85	74	0.719	0.0	******	******	****	****
146	23	1679	1.94	21.00	5.73	36.00	3	1	92	72	0.728	0.0	23.10	23.10	****	0.62
146	24	1680	1.94	21.00	5.73	36.00	3	1	94	71	0.718	0.0	23.10	23.10	****	0.62

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
147	1	1681	1.94	21.10	5.73	36.00	4	1	96	70	0.709	0.0	23.10	23.10	****	0.63
147	2	1682	1.94	21.10	5.73	36.00	5	2	98	69	0.700	0.0	23.10	23.10	****	0.63
147	3	1683	1.94	21.10	5.73	36.00	1	1	99	69	0.707	0.0	26.40	26.40	****	0.72
147	4	1684	1.94	21.10	5.73	36.00	0	0	99	69	0.707	0.0	26.40	26.40	****	0.72
147	5	1685	1.94	21.10	5.73	36.00	0	0	99	68	0.683	0.0	29.70	29.70	****	0.82
147	6	1686	1.94	21.10	5.73	36.00	0	0	99	68	0.683	0.0	29.70	29.70	****	0.82
147	7	1687	1.94	21.10	5.73	13.14	0	0	99	69	0.707	0.78	36.30	35.52	0.81	0.97
147	8	1688	1.94	21.10	16.09	3.56	0	0	99	72	0.783	17.16	62.70	45.54	0.84	****
147	9	1689	1.94	21.10	28.90	2.06	3	3	92	76	0.833	30.42	82.50	52.08	****	****
147	10	1690	1.94	21.10	41.93	1.49	4	4	75	80	0.774	46.02	105.60	59.58	****	****
147	11	1691	1.94	21.10	55.04	1.22	4	4	62	84	0.728	62.40	122.10	59.70	****	****
147	12	1692	1.94	21.10	67.96	1.08	4	4	56	84	0.658	66.30	102.30	36.00	****	0.88
147	13	1693	1.94	21.10	79.43	1.02	3	3	54	88	0.721	******	132.00	******	****	****
147	14	1694	1.94	21.10	79.75	1.02	4	4	52	88	0.694	62.40	99.00	36.60	****	0.87
147	15	1695	1.94	21.10	68.42	1.07	3	3	48	89	0.661	66.30	115.50	49.20	****	****
147	16	1696	1.94	21.10	55.51	1.21	2	2	47	91	0.689	63.18	99.00	35.82	****	0.83
147	17	1697	1.94	21.10	42.40	1.48	2	2	47	90	0.668	46.80	66.00	19.20	****	0.45
147	18	1698	1.94	21.10	29.37	2.03	1	1	48	90	0.683	25.74	49.50	23.76	****	0.56
147	19	1699	1.94	21.10	16.55	3.47	2	1	55	85	0.668	8.58	29.70	21.12	****	0.51
147	20	1700	1.94	21.10	5.73	12.06	5	4	58	82	0.639	0.78	23.10	22.32	****	0.55
147	21	1701	1.94	21.10	5.73	36.00	4	3	70	80	0.722	0.0	23.10	23.10	****	0.58
147	22	1702	1.94	21.10	5.73	36.00	3	2	76	79	0.759	0.0	23.10	23.10	****	0.59
147	23	1703	1.94	21.10	5.73	36.00	3	2	80	78	0.774	0.0	23.10	23.10	****	0.59
147	24	1704	1.94	21.10	5.73	36.00	0	0	80	76	0.724	0.0	23.10	23.10	****	0.60
148	1	1705	1.94	21.30	5.73	36.00	8	8	88	74	0.744	0.0	******	******	****	****
148	2	1706	1.94	21.30	5.73	36.00	8	8	88	74	0.744	0.0	******	******	****	****
148	3	1707	1.94	21.30	5.73	36.00	9	9	90	73	0.736	0.0	******	******	****	****
148	4	1708	1.94	21.30	5.73	36.00	8	7	92	73	0.753	0.0	******	******	****	****
148	5	1709	1.94	21.30	5.73	36.00	7	6	93	72	0.736	0.0	******	******	****	****
148	6	1710	1.94	21.30	5.73	36.00	3	1	96	71	0.733	0.0	******	******	****	****
148	7	1711	1.94	21.30	5.73	12.83	0	0	97	71	0.741	0.78	******	******	0.81	****
148	8	1712	1.94	21.30	16.20	3.54	2	2	97	73	0.793	15.60	42.90	27.30	****	0.72
148	9	1713	1.94	21.30	29.00	2.06	8	8	90	78	0.870	31.20	59.40	28.20	****	0.72
148	10	1714	1.94	21.30	42.02	1.49	5	5	86	79	0.859	35.10	69.30	34.20	****	0.87
148	11	1715	1.94	21.30	55.14	1.22	4	4	76	82	0.838	52.26	75.90	23.64	****	0.59
148	12	1716	1.94	21.30	68.07	1.08	3	3	70	82	0.771	45.24	95.70	50.46	****	****
148	13	1717	1.94	21.30	79.60	1.02	7	6	63	87	0.815	******	115.50	******	****	****
148	14	1718	1.94	21.30	79.89	1.02	10	10	70	86	0.877	******	******	******	****	****
148	15	1719	1.94	21.30	68.48	1.07	10	10	98	71	0.749	1.56	46.20	44.64	****	****
148	16	1720	1.94	21.30	55.56	1.21	10	10	99	72	0.783	0.0	52.80	52.80	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
148	17	1721	1.94	21.30	42.45	1.48	10	10	99	73	0.810	0.0	52.80	52.80	****	****
148	18	1722	1.94	21.30	29.42	2.03	10	10	99	74	0.838	7.80	******	******	****	****
148	19	1723	1.94	21.30	16.62	3.46	10	10	99	75	0.866	7.80	******	******	****	****
148	20	1724	1.94	21.30	5.73	11.88	9	8	95	73	0.777	0.78	******	******	****	****
148	21	1725	1.94	21.30	5.73	36.00	7	5	97	71	0.741	0.0	******	******	****	****
148	22	1726	1.94	21.30	5.73	36.00	10	10	99	70	0.732	0.0	******	******	****	****
148	23	1727	1.94	21.30	5.73	36.00	10	10	99	71	0.756	0.0	******	******	****	****
148	24	1728	1.94	21.30	5.73	36.00	8	8	99	72	0.783	0.0	******	******	****	****
149	1	1729	1.94	21.50	5.73	36.00	8	8	98	72	0.775	0.0	******	******	****	****
149	2	1730	1.94	21.50	5.73	36.00	8	8	98	72	0.775	0.0	******	******	****	****
149	3	1731	1.94	21.50	5.73	36.00	9	9	98	72	0.775	0.0	******	******	****	****
149	4	1732	1.94	21.50	5.73	36.00	9	9	98	72	0.775	0.0	******	******	****	****
149	5	1733	1.94	21.50	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
149	6	1734	1.94	21.50	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
149	7	1735	1.94	21.50	5.73	12.53	10	10	98	72	0.775	0.0	******	******	****	****
149	8	1736	1.94	21.50	16.31	3.52	10	10	98	72	0.775	4.68	******	******	****	****
149	9	1737	1.94	21.50	29.09	2.05	10	10	96	74	0.812	9.36	******	******	****	****
149	10	1738	1.94	21.50	42.12	1.49	10	10	92	75	0.805	14.82	******	******	****	****
149	11	1739	1.94	21.50	55.23	1.22	10	10	85	78	0.822	34.32	******	******	****	****
149	12	1740	1.94	21.50	68.18	1.08	10	10	75	80	0.774	21.84	******	******	****	****
149	13	1741	1.94	21.50	79.77	1.02	10	10	90	71	0.688	4.68	******	******	****	****
149	14	1742	1.94	21.50	80.03	1.01	10	10	97	71	0.741	2.34	******	******	****	****
149	15	1743	1.94	21.50	68.55	1.07	10	10	97	71	0.741	9.36	******	******	****	****
149	16	1744	1.94	21.50	55.61	1.21	10	10	98	70	0.724	13.26	******	******	****	****
149	17	1745	1.94	21.50	42.50	1.48	10	10	98	70	0.724	14.82	******	******	****	****
149	18	1746	1.94	21.50	29.47	2.02	10	10	99	70	0.732	6.24	******	******	****	****
149	19	1747	1.94	21.50	16.68	3.44	10	10	99	70	0.732	0.78	******	******	****	****
149	20	1748	1.94	21.50	5.73	11.71	10	10	99	70	0.732	0.0	******	******	****	****
149	21	1749	1.94	21.50	5.73	36.00	10	10	99	70	0.732	0.0	******	******	****	****
149	22	1750	1.94	21.50	5.73	36.00	10	10	99	70	0.732	0.0	******	******	****	****
149	23	1751	1.94	21.50	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
149	24	1752	1.94	21.50	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
150	1	1753	1.94	21.70	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
150	2	1754	1.94	21.70	5.73	36.00	9	8	100	69	0.714	0.0	******	******	****	****
150	3	1755	1.94	21.70	5.73	36.00	8	7	100	69	0.714	0.0	******	******	****	****
150	4	1756	1.94	21.70	5.73	36.00	8	7	100	69	0.714	0.0	******	******	****	****
150	5	1757	1.94	21.70	5.73	36.00	10	10	100	69	0.714	0.0	******	******	****	****
150	6	1758	1.94	21.70	5.73	36.00	7	6	100	69	0.714	0.0	******	******	****	****
150	7	1759	1.94	21.70	5.73	12.25	10	9	100	70	0.739	0.78	******	******	****	****
150	8	1760	1.94	21.70	16.41	3.50	10	10	100	71	0.764	5.46	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
150	9	1761	1.94	21.70	29.19	2.04	10	10	99	72	0.783	8.58	******	******	****	****
150	10	1762	1.94	21.70	42.20	1.49	10	0	93	75	0.814	21.84	******	******	****	****
150	11	1763	1.94	21.70	55.32	1.21	8	6	80	78	0.774	40.56	******	******	****	****
150	12	1764	1.94	21.70	68.28	1.08	5	4	70	81	0.746	******	******	******	****	****
150	13	1765	1.94	21.70	79.93	1.02	6	5	62	83	0.706	******	******	******	****	****
150	14	1766	1.94	21.70	80.17	1.01	8	8	62	83	0.706	******	******	******	****	****
150	15	1767	1.94	21.70	68.61	1.07	9	7	64	82	0.705	13.26	******	******	****	****
150	16	1768	1.94	21.70	55.66	1.21	8	6	80	78	0.774	14.04	******	******	****	****
150	17	1769	1.94	21.70	42.55	1.48	8	5	95	74	0.804	7.80	******	******	****	****
150	18	1770	1.94	21.70	29.53	2.02	8	6	88	76	0.796	15.60	******	******	****	****
150	19	1771	1.94	21.70	16.75	3.43	8	5	82	76	0.742	4.68	******	******	****	****
150	20	1772	1.94	21.70	5.73	11.54	3	2	81	76	0.733	0.78	******	******	****	****
150	21	1773	1.94	21.70	5.73	36.00	5	3	85	73	0.695	0.0	******	******	****	****
150	22	1774	1.94	21.70	5.73	36.00	4	2	90	72	0.712	0.0	******	******	****	****
150	23	1775	1.94	21.70	5.73	36.00	3	1	92	72	0.728	0.0	******	******	****	****
150	24	1776	1.94	21.70	5.73	36.00	0	0	94	71	0.718	0.0	******	******	****	****
151	1	1777	1.94	21.90	5.73	36.00	0	0	97	70	0.717	0.0	******	******	****	****
151	2	1778	1.94	21.90	5.73	36.00	0	0	98	69	0.700	0.0	******	******	****	****
151	3	1779	1.94	21.90	5.73	36.00	0	0	98	69	0.700	0.0	******	******	****	****
151	4	1780	1.94	21.90	5.73	36.00	5	5	98	70	0.724	0.0	******	******	****	****
151	5	1781	1.94	21.90	5.73	36.00	0	0	98	69	0.700	0.0	******	******	****	****
151	6	1782	1.94	21.90	5.73	36.00	0	0	98	68	0.676	0.0	******	******	****	****
151	7	1783	1.94	21.90	5.73	11.93	0	0	99	68	0.683	******	******	******	****	****
151	8	1784	1.94	21.90	16.54	3.47	5	5	99	70	0.732	******	******	******	****	****
151	9	1785	1.94	21.90	29.31	2.04	5	5	85	75	0.744	******	******	******	****	****
151	10	1786	1.94	21.90	42.32	1.48	5	5	70	76	0.633	******	******	******	****	****
151	11	1787	1.94	21.90	55.43	1.21	6	6	68	78	0.658	******	******	******	****	****
151	12	1788	1.94	21.90	68.40	1.07	7	5	70	80	0.722	******	******	******	****	****
151	13	1789	1.94	21.90	80.11	1.01	7	5	70	80	0.722	******	******	******	****	****
151	14	1790	1.94	21.90	80.29	1.01	3	3	90	78	0.870	******	******	******	****	****
151	15	1791	1.94	21.90	68.65	1.07	3	3	70	80	0.722	******	******	******	****	****
151	16	1792	1.94	21.90	55.68	1.21	5	3	55	86	0.689	******	******	******	****	****
151	17	1793	1.94	21.90	42.57	1.48	7	3	53	85	0.643	******	******	******	****	****
151	18	1794	1.94	21.90	29.56	2.02	4	1	60	84	0.705	******	******	******	****	****
151	19	1795	1.94	21.90	16.79	3.42	8	2	60	82	0.661	******	******	******	****	****
151	20	1796	1.94	21.90	5.73	11.42	6	2	64	78	0.619	******	******	******	****	****
151	21	1797	1.94	21.90	5.73	36.00	5	1	73	75	0.639	0.0	******	******	****	****
151	22	1798	1.94	21.90	5.73	36.00	4	1	80	74	0.677	0.0	******	******	****	****
151	23	1799	1.94	21.90	5.73	36.00	3	1	87	72	0.688	0.0	******	******	****	****
151	24	1800	1.94	21.90	5.73	36.00	4	1	91	71	0.695	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
152	1	1801	1.94	22.00	5.73	36.00	4	1	95	70	0.702	0.0	******	******	****	****
152	2	1802	1.94	22.00	5.73	36.00	0	0	96	69	0.685	0.0	******	******	****	****
152	3	1803	1.94	22.00	5.73	36.00	0	0	96	69	0.685	0.0	******	******	****	****
152	4	1804	1.94	22.00	5.73	36.00	0	0	97	69	0.693	0.0	******	******	****	****
152	5	1805	1.94	22.00	5.73	36.00	3	2	98	69	0.700	0.0	******	******	****	****
152	6	1806	1.94	22.00	5.73	36.00	10	4	98	68	0.676	0.0	******	******	****	****
152	7	1807	1.94	22.00	5.73	11.78	7	4	98	70	0.724	******	******	******	****	****
152	8	1808	1.94	22.00	16.61	3.46	5	2	98	70	0.724	******	******	******	****	****
152	9	1809	1.94	22.00	29.37	2.03	6	6	90	77	0.0	******	******	******	****	****
152	10	1810	1.94	22.00	42.37	1.48	8	8	80	80	0.0	******	******	******	****	****
152	11	1811	1.94	22.00	55.48	1.21	6	6	70	83	0.0	44.46	******	******	****	****
152	12	1812	1.94	22.00	68.46	1.07	7	7	65	84	0.0	******	******	******	****	****
152	13	1813	1.94	22.00	80.20	1.01	6	6	80	82	0.0	******	******	******	****	****
152	14	1814	1.94	22.00	80.35	1.01	10	9	65	85	0.0	62.40	******	******	****	****
152	15	1815	1.94	22.00	68.67	1.07	10	9	95	76	0.0	23.40	******	******	****	****
152	16	1816	1.94	22.00	55.69	1.21	10	10	98	76	0.0	10.14	******	******	****	****
152	17	1817	1.94	22.00	42.58	1.48	10	10	98	72	0.0	4.68	******	******	****	****
152	18	1818	1.94	22.00	29.57	2.02	10	10	99	72	0.0	1.56	******	******	****	****
152	19	1819	1.94	22.00	16.81	3.42	8	7	100	72	0.0	2.34	******	******	****	****
152	20	1820	1.94	22.00	5.73	11.36	6	5	100	72	0.0	0.0	******	******	****	****
152	21	1821	1.94	22.00	5.73	36.00	6	4	100	70	0.0	0.0	******	******	****	****
152	22	1822	1.94	22.00	5.73	36.00	4	3	100	70	0.0	0.0	******	******	****	****
152	23	1823	1.94	22.00	5.73	36.00	4	3	100	70	0.0	0.0	******	******	****	****
152	24	1824	1.94	22.00	5.73	36.00	3	2	100	70	0.0	0.0	******	******	****	****
153	1	1825	1.94	22.10	5.73	36.00	3	1	100	69	0.714	0.0	******	******	****	****
153	2	1826	1.94	22.10	5.73	36.00	3	1	100	68	0.690	0.0	******	******	****	****
153	3	1827	1.94	22.10	5.73	36.00	0	0	100	68	0.690	0.0	******	******	****	****
153	4	1828	1.94	22.10	5.73	36.00	4	3	100	68	0.690	0.0	******	******	****	****
153	5	1829	1.94	22.10	5.73	36.00	0	0	100	68	0.690	0.0	******	******	****	****
153	6	1830	1.94	22.10	5.73	36.00	5	4	100	68	0.690	0.0	******	******	****	****
153	7	1831	1.94	22.10	5.73	11.59	4	4	100	70	0.739	******	******	******	****	****
153	8	1832	1.94	22.10	16.69	3.44	2	1	100	72	0.791	******	46.20	******	****	****
153	9	1833	1.94	22.10	29.44	2.03	4	2	87	75	0.761	******	72.60	******	****	****
153	10	1834	1.94	22.10	42.45	1.48	5	4	76	78	0.735	******	89.10	******	****	****
153	11	1835	1.94	22.10	55.56	1.21	5	4	70	80	0.722	******	99.00	******	****	****
153	12	1836	1.94	22.10	68.55	1.07	7	7	65	82	0.716	******	112.20	******	****	****
153	13	1837	1.94	22.10	80.30	1.01	6	6	62	83	0.706	******	99.00	******	****	****
153	14	1838	1.94	22.10	80.39	1.01	6	6	60	84	0.705	******	118.80	******	****	****
153	15	1839	1.94	22.10	68.67	1.07	6	6	55	85	0.668	******	92.40	******	****	****
153	16	1840	1.94	22.10	55.69	1.21	4	3	50	85	0.607	******	85.80	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
153	17	1841	1.94	22.10	42.58	1.48	2	2	48	86	0.601	******	56.10	******	****	****
153	18	1842	1.94	22.10	29.57	2.02	7	2	46	85	0.558	******	52.80	******	****	****
153	19	1843	1.94	22.10	16.81	3.42	9	3	50	80	0.516	******	23.10	******	****	****
153	20	1844	1.94	22.10	5.73	11.34	0	0	58	76	0.525	******	6.60	******	****	****
153	21	1845	1.94	22.10	5.73	36.00	0	0	61	74	0.516	0.0	******	******	****	****
153	22	1846	1.94	22.10	5.73	36.00	0	0	70	72	0.554	0.0	******	******	****	****
153	23	1847	1.94	22.10	5.73	36.00	0	0	77	71	0.588	0.0	******	******	****	****
153	24	1848	1.94	22.10	5.73	36.00	0	0	84	70	0.621	0.0	******	******	****	****
154	1	1849	1.94	22.30	5.73	36.00	0	0	90	69	0.643	0.0	3.30	3.30	****	0.09
154	2	1850	1.94	22.30	5.73	36.00	0	0	94	68	0.649	0.0	3.30	3.30	****	0.09
154	3	1851	1.94	22.30	5.73	36.00	0	0	95	68	0.655	0.0	3.30	3.30	****	0.09
154	4	1852	1.94	22.30	5.73	36.00	0	0	95	67	0.634	0.0	3.30	3.30	****	0.09
154	5	1853	1.94	22.30	5.73	36.00	0	0	97	66	0.625	0.0	3.30	3.30	****	0.09
154	6	1854	1.94	22.30	5.73	36.00	2	1	98	66	0.631	0.0	16.50	16.50	****	0.46
154	7	1855	1.94	22.30	5.73	11.30	8	2	98	68	0.676	0.78	33.00	32.22	****	0.89
154	8	1856	1.94	22.30	16.82	3.42	9	4	94	72	0.744	12.48	36.30	23.82	****	0.64
154	9	1857	1.94	22.30	29.56	2.02	9	5	80	76	0.724	28.86	66.00	37.14	****	0.96
154	10	1858	1.94	22.30	42.56	1.48	9	6	70	78	0.677	43.68	62.70	19.02	****	0.49
154	11	1859	1.94	22.30	55.67	1.21	7	6	63	80	0.650	46.02	79.20	33.18	****	0.84
154	12	1860	1.94	22.30	68.67	1.07	9	7	60	82	0.661	57.72	85.80	28.08	****	0.70
154	13	1861	1.94	22.30	80.48	1.01	8	7	57	84	0.670	******	69.30	******	****	****
154	14	1862	1.94	22.30	80.51	1.01	8	7	53	84	0.623	******	115.50	******	****	****
154	15	1863	1.94	22.30	68.71	1.07	8	4	51	85	0.619	******	85.80	******	****	****
154	16	1864	1.94	22.30	55.71	1.21	9	5	50	85	0.607	53.82	79.20	25.38	****	0.62
154	17	1865	1.94	22.30	42.60	1.47	10	10	50	84	0.587	34.32	36.30	1.98	****	0.05
154	18	1866	1.94	22.30	29.60	2.02	10	10	52	82	0.573	35.88	29.70	******	****	****
154	19	1867	1.94	22.30	16.85	3.41	10	10	60	80	0.619	17.16	16.50	******	****	****
154	20	1868	1.94	22.30	5.73	11.23	10	10	68	78	0.658	3.12	9.90	6.78	****	0.17
154	21	1869	1.94	22.30	5.73	36.00	10	10	75	76	0.679	0.0	6.60	6.60	****	0.17
154	22	1870	1.94	22.30	5.73	36.00	10	10	76	75	0.665	0.0	6.60	6.60	****	0.17
154	23	1871	1.94	22.30	5.73	36.00	8	7	80	74	0.677	0.0	6.60	6.60	****	0.17
154	24	1872	1.94	22.30	5.73	36.00	10	10	85	74	0.719	0.0	6.60	6.60	****	0.17
155	1	1873	1.94	22.40	5.73	36.00	10	10	84	74	0.711	0.0	******	******	****	****
155	2	1874	1.94	22.40	5.73	36.00	10	10	85	74	0.719	0.0	******	******	****	****
155	3	1875	1.94	22.40	5.73	36.00	10	10	86	73	0.703	0.0	******	******	****	****
155	4	1876	1.94	22.40	5.73	36.00	10	10	86	72	0.680	0.0	******	******	****	****
155	5	1877	1.94	22.40	5.73	36.00	10	10	88	72	0.696	0.0	******	******	****	****
155	6	1878	1.94	22.40	5.73	36.00	10	10	90	72	0.712	0.0	******	******	****	****
155	7	1879	1.94	22.40	5.73	11.12	10	10	90	73	0.736	******	9.90	******	****	****
155	8	1880	1.94	22.40	16.90	3.40	10	10	90	74	0.761	******	19.80	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
155	9	1881	1.94	22.40	29.64	2.01	10	10	88	77	0.823	******	36.30	******	****	****
155	10	1882	1.94	22.40	42.64	1.47	10	10	80	79	0.799	******	52.80	******	****	****
155	11	1883	1.94	22.40	55.75	1.21	10	10	84	79	0.839	******	56.10	******	****	****
155	12	1884	1.94	22.40	68.75	1.07	10	10	85	79	0.849	******	******	******	****	****
155	13	1885	1.94	22.40	80.58	1.01	10	10	90	74	0.761	******	******	******	****	****
155	14	1886	1.94	22.40	80.55	1.01	10	10	98	72	0.775	******	******	******	****	****
155	15	1887	1.94	22.40	68.70	1.07	10	10	98	72	0.775	******	******	******	****	****
155	16	1888	1.94	22.40	55.70	1.21	10	10	98	72	0.775	******	******	******	****	****
155	17	1889	1.94	22.40	42.59	1.48	10	10	98	74	0.829	******	******	******	****	****
155	18	1890	1.94	22.40	29.59	2.02	10	10	98	74	0.829	******	******	******	****	****
155	19	1891	1.94	22.40	16.85	3.41	10	8	97	74	0.821	******	******	******	****	****
155	20	1892	1.94	22.40	5.73	11.21	10	10	98	73	0.802	******	******	******	****	****
155	21	1893	1.94	22.40	5.73	36.00	10	10	98	73	0.802	0.0	******	******	****	****
155	22	1894	1.94	22.40	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****
155	23	1895	1.94	22.40	5.73	36.00	8	6	99	73	0.810	0.0	******	******	****	****
155	24	1896	1.94	22.40	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
156	1	1897	1.94	22.50	5.73	36.00	10	8	99	72	0.783	0.0	******	******	****	****
156	2	1898	1.94	22.50	5.73	36.00	8	7	99	72	0.783	0.0	******	******	****	****
156	3	1899	1.94	22.50	5.73	36.00	10	8	99	71	0.756	0.0	******	******	****	****
156	4	1900	1.94	22.50	5.73	36.00	10	9	99	70	0.732	0.0	******	******	****	****
156	5	1901	1.94	22.50	5.73	36.00	9	6	99	68	0.683	0.0	******	******	****	****
156	6	1902	1.94	22.50	5.73	36.00	10	5	99	68	0.683	0.0	******	******	****	****
156	7	1903	1.94	22.50	5.73	10.98	10	9	98	68	0.676	******	******	******	****	****
156	8	1904	1.94	22.50	16.96	3.39	10	9	92	70	0.680	******	******	******	****	****
156	9	1905	1.94	22.50	29.70	2.01	10	9	85	74	0.719	******	******	******	****	****
156	10	1906	1.94	22.50	42.69	1.47	10	9	73	76	0.661	******	******	******	****	****
156	11	1907	1.94	22.50	55.80	1.21	9	7	64	78	0.619	******	******	******	****	****
156	12	1908	1.94	22.50	68.81	1.07	9	7	62	80	0.640	******	******	******	****	****
156	13	1909	1.94	22.50	80.67	1.01	8	6	58	82	0.639	******	******	******	****	****
156	14	1910	1.94	22.50	80.60	1.01	9	7	53	84	0.623	******	******	******	****	****
156	15	1911	1.94	22.50	68.72	1.07	8	6	55	84	0.646	******	******	******	****	****
156	16	1912	1.94	22.50	55.71	1.21	7	5	50	84	0.587	******	******	******	****	****
156	17	1913	1.94	22.50	42.60	1.47	5	2	44	84	0.517	******	******	******	****	****
156	18	1914	1.94	22.50	29.61	2.02	5	2	46	84	0.540	******	******	******	****	****
156	19	1915	1.94	22.50	16.87	3.41	4	2	46	82	0.507	******	******	******	****	****
156	20	1916	1.94	22.50	5.73	11.15	6	3	60	78	0.580	******	******	******	****	****
156	21	1917	1.94	22.50	5.73	36.00	6	3	67	75	0.586	0.0	******	******	****	****
156	22	1918	1.94	22.50	5.73	36.00	6	3	77	74	0.651	0.0	******	******	****	****
156	23	1919	1.94	22.50	5.73	36.00	6	2	83	72	0.657	0.0	******	******	****	****
156	24	1920	1.94	22.50	5.73	36.00	6	2	87	71	0.665	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
157	1	1921	1.94	22.60	5.73	36.00	4	3	93	70	0.687	0.0	******	******	****	****
157	2	1922	1.94	22.60	5.73	36.00	3	2	94	69	0.671	0.0	******	******	****	****
157	3	1923	1.94	22.60	5.73	36.00	0	0	97	67	0.647	0.0	******	******	****	****
157	4	1924	1.94	22.60	5.73	36.00	0	0	97	67	0.647	0.0	******	******	****	****
157	5	1925	1.94	22.60	5.73	36.00	0	0	97	66	0.625	0.0	******	******	****	****
157	6	1926	1.94	22.60	5.73	36.00	0	0	98	64	0.588	0.0	******	******	****	****
157	7	1927	1.94	22.60	5.73	10.82	0	0	99	65	0.616	******	******	******	****	****
157	8	1928	1.94	22.60	17.05	3.37	0	0	92	68	0.635	******	******	******	****	****
157	9	1929	1.94	22.60	29.78	2.01	5	5	75	74	0.634	******	******	******	****	****
157	10	1930	1.94	22.60	42.77	1.47	8	8	70	75	0.612	******	******	******	****	****
157	11	1931	1.94	22.60	55.88	1.21	10	9	70	73	0.573	******	******	******	****	****
157	12	1932	1.94	22.60	68.89	1.07	8	7	88	72	0.696	******	******	******	****	****
157	13	1933	1.94	22.60	80.77	1.01	8	8	80	76	0.724	******	******	******	****	****
157	14	1934	1.94	22.60	80.64	1.01	8	8	70	78	0.677	******	******	******	****	****
157	15	1935	1.94	22.60	68.71	1.07	8	8	58	80	0.599	******	******	******	****	****
157	16	1936	1.94	22.60	55.70	1.21	7	7	56	82	0.617	******	******	******	****	****
157	17	1937	1.94	22.60	42.59	1.48	4	3	52	83	0.592	******	******	******	****	****
157	18	1938	1.94	22.60	29.60	2.02	2	2	51	82	0.562	******	******	******	****	****
157	19	1939	1.94	22.60	16.88	3.41	1	0	52	80	0.537	******	******	******	****	****
157	20	1940	1.94	22.60	5.73	11.13	0	0	52	75	0.455	******	******	******	****	****
157	21	1941	1.94	22.60	5.73	36.00	0	0	65	73	0.532	0.0	******	******	****	****
157	22	1942	1.94	22.60	5.73	36.00	0	0	72	71	0.550	0.0	******	******	****	****
157	23	1943	1.94	22.60	5.73	36.00	0	0	80	70	0.591	0.0	******	******	****	****
157	24	1944	1.94	22.60	5.73	36.00	0	0	83	68	0.573	0.0	******	******	****	****
158	1	1945	1.94	22.70	5.73	36.00	0	0	87	67	0.580	0.0	******	******	****	****
158	2	1946	1.94	22.70	5.73	36.00	0	0	92	66	0.592	0.0	******	******	****	****
158	3	1947	1.94	22.70	5.73	36.00	0	0	94	65	0.585	0.0	******	******	****	****
158	4	1948	1.94	22.70	5.73	36.00	0	0	95	64	0.570	0.0	******	******	****	****
158	5	1949	1.94	22.70	5.73	36.00	7	7	97	64	0.582	0.0	******	******	****	****
158	6	1950	1.94	22.70	5.73	36.00	4	4	96	64	0.576	0.0	******	******	****	****
158	7	1951	1.94	22.70	5.73	10.69	2	2	95	64	0.570	******	******	******	****	****
158	8	1952	1.94	22.70	17.11	3.36	2	2	95	69	0.678	******	******	******	****	****
158	9	1953	1.94	22.70	29.84	2.00	0	0	82	72	0.649	******	******	******	****	****
158	10	1954	1.94	22.70	42.82	1.47	5	3	70	76	0.633	******	******	******	****	****
158	11	1955	1.94	22.70	55.93	1.21	8	7	60	78	0.580	******	******	******	****	****
158	12	1956	1.94	22.70	68.95	1.07	5	4	56	80	0.578	******	******	******	****	****
158	13	1957	1.94	22.70	80.86	1.01	5	4	53	80	0.547	******	******	******	****	****
158	14	1958	1.94	22.70	80.69	1.01	5	4	50	82	0.551	******	******	******	****	****
158	15	1959	1.94	22.70	68.73	1.07	5	4	46	84	0.540	******	******	******	****	****
158	16	1960	1.94	22.70	55.71	1.21	5	4	45	84	0.529	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
158	17	1961	1.94	22.70	42.60	1.47	5	4	45	84	0.529	******	******	******	****	****
158	18	1962	1.94	22.70	29.62	2.02	5	4	46	83	0.523	******	******	******	****	****
158	19	1963	1.94	22.70	16.90	3.40	5	4	50	70	0.369	******	******	******	****	****
158	20	1964	1.94	22.70	5.73	11.08	8	6	53	67	0.354	******	******	******	****	****
158	21	1965	1.94	22.70	5.73	36.00	7	5	72	73	0.589	0.0	******	******	****	****
158	22	1966	1.94	22.70	5.73	36.00	3	2	80	70	0.591	0.0	******	******	****	****
158	23	1967	1.94	22.70	5.73	36.00	3	2	85	68	0.586	0.0	******	******	****	****
158	24	1968	1.94	22.70	5.73	36.00	3	2	90	67	0.600	0.0	******	******	****	****
159	1	1969	1.94	22.80	5.73	36.00	0	0	91	67	0.607	0.0	******	******	****	****
159	2	1970	1.94	22.80	5.73	36.00	0	0	95	66	0.612	0.0	******	******	****	****
159	3	1971	1.94	22.80	5.73	36.00	0	0	96	65	0.597	0.0	******	******	****	****
159	4	1972	1.94	22.80	5.73	36.00	0	0	97	65	0.603	0.0	******	******	****	****
159	5	1973	1.94	22.80	5.73	36.00	3	1	96	64	0.576	0.0	******	******	****	****
159	6	1974	1.94	22.80	5.73	36.00	0	0	96	64	0.576	0.0	******	******	****	****
159	7	1975	1.94	22.80	5.73	10.53	0	0	96	64	0.576	******	******	******	****	****
159	8	1976	1.94	22.80	17.20	3.35	0	0	91	66	0.586	******	******	******	****	****
159	9	1977	1.94	22.80	29.92	2.00	0	0	87	70	0.643	******	******	******	****	****
159	10	1978	1.94	22.80	42.90	1.47	0	0	70	73	0.573	******	******	******	****	****
159	11	1979	1.94	22.80	56.01	1.20	0	0	62	77	0.580	******	******	******	****	****
159	12	1980	1.94	22.80	69.03	1.07	3	3	53	80	0.547	******	******	******	****	****
159	13	1981	1.94	22.80	80.97	1.01	6	6	50	83	0.569	******	******	******	****	****
159	14	1982	1.94	22.80	80.73	1.01	5	5	47	84	0.552	******	******	******	****	****
159	15	1983	1.94	22.80	68.72	1.07	7	7	44	86	0.551	******	******	******	****	****
159	16	1984	1.94	22.80	55.69	1.21	6	6	46	84	0.540	******	******	******	****	****
159	17	1985	1.94	22.80	42.59	1.48	4	4	52	83	0.592	******	******	******	****	****
159	18	1986	1.94	22.80	29.61	2.02	7	6	50	82	0.551	******	******	******	****	****
159	19	1987	1.94	22.80	16.90	3.40	3	2	50	82	0.551	******	******	******	****	****
159	20	1988	1.94	22.80	5.73	11.06	3	2	54	80	0.557	******	******	******	****	****
159	21	1989	1.94	22.80	5.73	36.00	0	0	62	76	0.561	0.0	******	******	****	****
159	22	1990	1.94	22.80	5.73	36.00	0	0	69	75	0.604	0.0	******	******	****	****
159	23	1991	1.94	22.80	5.73	36.00	0	0	73	74	0.618	0.0	******	******	****	****
159	24	1992	1.94	22.80	5.73	36.00	0	0	77	72	0.609	0.0	******	******	****	****
160	1	1993	1.94	22.90	5.73	36.00	0	0	83	70	0.613	0.0	******	******	****	****
160	2	1994	1.94	22.90	5.73	36.00	0	0	92	68	0.635	0.0	******	******	****	****
160	3	1995	1.94	22.90	5.73	36.00	0	0	95	67	0.634	0.0	******	******	****	****
160	4	1996	1.94	22.90	5.73	36.00	0	0	97	66	0.625	0.0	******	******	****	****
160	5	1997	1.94	22.90	5.73	36.00	0	0	98	65	0.610	0.0	******	******	****	****
160	6	1998	1.94	22.90	5.73	36.00	0	0	99	64	0.594	0.0	******	******	****	****
160	7	1999	1.94	22.90	5.73	10.37	0	0	98	66	0.631	******	******	******	****	****
160	8	2000	1.94	22.90	17.28	3.33	0	0	95	68	0.655	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
160	9	2001	1.94	22.90	30.00	1.99	4	4	90	72	0.712	******	******	******	****	****
160	10	2002	1.94	22.90	42.98	1.46	4	4	75	75	0.656	******	******	******	****	****
160	11	2003	1.94	22.90	56.08	1.20	4	4	70	77	0.654	******	******	******	****	****
160	12	2004	1.94	22.90	69.11	1.07	5	5	60	80	0.619	******	******	******	****	****
160	13	2005	1.94	22.90	81.07	1.01	4	4	55	83	0.626	******	******	******	****	****
160	14	2006	1.94	22.90	80.77	1.01	6	6	52	84	0.611	******	******	******	****	****
160	15	2007	1.94	22.90	68.72	1.07	5	5	50	86	0.626	******	******	******	****	****
160	16	2008	1.94	22.90	55.68	1.21	4	4	48	86	0.601	******	******	******	****	****
160	17	2009	1.94	22.90	42.58	1.48	3	3	46	87	0.595	******	******	******	****	****
160	18	2010	1.94	22.90	29.61	2.02	1	1	44	88	0.587	******	******	******	****	****
160	19	2011	1.94	22.90	16.90	3.40	1	1	47	86	0.589	******	******	******	****	****
160	20	2012	1.94	22.90	5.73	11.04	2	2	55	82	0.606	******	******	******	****	****
160	21	2013	1.94	22.90	5.73	36.00	5	4	73	77	0.683	0.0	******	******	****	****
160	22	2014	1.94	22.90	5.73	36.00	0	0	75	76	0.679	0.0	******	******	****	****
160	23	2015	1.94	22.90	5.73	36.00	0	0	82	73	0.671	0.0	******	******	****	****
160	24	2016	1.94	22.90	5.73	36.00	0	0	87	72	0.688	0.0	******	******	****	****
161	1	2017	1.94	23.00	5.73	36.00	0	0	89	70	0.658	0.0	******	******	****	****
161	2	2018	1.94	23.00	5.73	36.00	0	0	92	70	0.680	0.0	******	******	****	****
161	3	2019	1.94	23.00	5.73	36.00	0	0	95	69	0.678	0.0	******	******	****	****
161	4	2020	1.94	23.00	5.73	36.00	0	0	96	68	0.662	0.0	******	******	****	****
161	5	2021	1.94	23.00	5.73	36.00	0	0	97	68	0.669	0.0	******	******	****	****
161	6	2022	1.94	23.00	5.73	36.00	5	2	98	68	0.676	0.0	******	******	****	****
161	7	2023	1.94	23.00	5.73	10.22	5	2	99	68	0.683	******	******	******	****	****
161	8	2024	1.94	23.00	17.36	3.32	3	1	99	70	0.732	******	******	******	****	****
161	9	2025	1.94	23.00	30.08	1.99	6	2	85	76	0.769	******	******	******	****	****
161	10	2026	1.94	23.00	43.05	1.46	7	4	65	80	0.671	******	******	******	****	****
161	11	2027	1.94	23.00	56.16	1.20	8	5	50	83	0.569	******	******	******	****	****
161	12	2028	1.94	23.00	69.19	1.07	9	7	48	85	0.583	******	******	******	****	****
161	13	2029	1.94	23.00	81.17	1.01	8	6	50	85	0.607	******	******	******	****	****
161	14	2030	1.94	23.00	80.80	1.01	10	7	49	88	0.654	******	******	******	****	****
161	15	2031	1.94	23.00	68.71	1.07	10	7	44	88	0.587	******	******	******	****	****
161	16	2032	1.94	23.00	55.67	1.21	8	6	44	88	0.587	******	******	******	****	****
161	17	2033	1.94	23.00	42.57	1.48	9	8	45	86	0.564	******	******	******	****	****
161	18	2034	1.94	23.00	29.60	2.02	9	8	53	84	0.623	******	******	******	****	****
161	19	2035	1.94	23.00	16.90	3.40	9	8	64	82	0.705	******	******	******	****	****
161	20	2036	1.94	23.00	5.73	11.02	9	8	70	80	0.722	******	******	******	****	****
161	21	2037	1.94	23.00	5.73	36.00	9	8	74	78	0.716	0.0	******	******	****	****
161	22	2038	1.94	23.00	5.73	36.00	9	8	76	78	0.735	0.0	******	******	****	****
161	23	2039	1.94	23.00	5.73	36.00	9	7	77	76	0.697	0.0	******	******	****	****
161	24	2040	1.94	23.00	5.73	36.00	10	10	75	75	0.656	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
162	1	2041	1.94	23.10	5.73	36.00	10	10	75	74	0.634	0.0	******	******	****	****
162	2	2042	1.94	23.10	5.73	36.00	10	10	77	74	0.651	0.0	******	******	****	****
162	3	2043	1.94	23.10	5.73	36.00	10	10	77	74	0.651	0.0	******	******	****	****
162	4	2044	1.94	23.10	5.73	36.00	10	10	85	74	0.719	0.0	******	******	****	****
162	5	2045	1.94	23.10	5.73	36.00	10	10	88	73	0.720	0.0	******	******	****	****
162	6	2046	1.94	23.10	5.73	36.00	10	9	90	73	0.736	0.0	******	******	****	****
162	7	2047	1.94	23.10	5.73	10.07	10	10	92	73	0.753	******	******	******	****	****
162	8	2048	1.94	23.10	17.45	3.30	10	10	92	74	0.778	******	******	******	****	****
162	9	2049	1.94	23.10	30.16	1.98	10	10	91	76	0.824	******	******	******	****	****
162	10	2050	1.94	23.10	43.13	1.46	8	6	88	78	0.851	******	******	******	****	****
162	11	2051	1.94	23.10	56.23	1.20	5	4	79	80	0.815	******	******	******	****	****
162	12	2052	1.94	23.10	69.27	1.07	5	5	65	84	0.764	******	******	******	****	****
162	13	2053	1.94	23.10	81.27	1.01	5	4	57	86	0.714	******	******	******	****	****
162	14	2054	1.94	23.10	80.83	1.01	5	4	50	88	0.667	******	******	******	****	****
162	15	2055	1.94	23.10	68.70	1.07	6	4	48	90	0.683	******	******	******	****	****
162	16	2056	1.94	23.10	55.66	1.21	8	6	50	90	0.711	******	******	******	****	****
162	17	2057	1.94	23.10	42.56	1.48	6	6	65	82	0.716	******	******	******	****	****
162	18	2058	1.94	23.10	29.59	2.02	8	8	89	72	0.704	******	******	******	****	****
162	19	2059	1.94	23.10	16.90	3.40	4	3	95	73	0.777	******	******	******	****	****
162	20	2060	1.94	23.10	5.73	11.00	0	0	95	74	0.804	******	******	******	****	****
162	21	2061	1.94	23.10	5.73	36.00	0	0	95	72	0.751	0.0	******	******	****	****
162	22	2062	1.94	23.10	5.73	36.00	0	0	96	71	0.733	0.0	******	******	****	****
162	23	2063	1.94	23.10	5.73	36.00	0	0	97	70	0.717	0.0	******	******	****	****
162	24	2064	1.94	23.10	5.73	36.00	0	0	97	70	0.717	0.0	******	******	****	****
163	1	2065	1.94	23.20	5.73	36.00	0	0	98	69	0.700	0.0	******	******	****	****
163	2	2066	1.94	23.20	5.73	36.00	0	0	99	69	0.707	0.0	******	******	****	****
163	3	2067	1.94	23.20	5.73	36.00	0	0	99	68	0.683	0.0	******	******	****	****
163	4	2068	1.94	23.20	5.73	36.00	0	0	99	68	0.683	0.0	******	******	****	****
163	5	2069	1.94	23.20	5.73	36.00	0	0	99	68	0.683	0.0	******	******	****	****
163	6	2070	1.94	23.20	5.73	36.00	0	0	99	68	0.683	0.0	******	******	****	****
163	7	2071	1.94	23.20	5.73	9.93	0	0	98	68	0.676	******	******	******	****	****
163	8	2072	1.94	23.20	17.53	3.29	0	0	96	70	0.709	******	******	******	****	****
163	9	2073	1.94	23.20	30.23	1.98	0	0	88	75	0.770	******	******	******	****	****
163	10	2074	1.94	23.20	43.20	1.46	3	3	78	78	0.754	******	******	******	****	****
163	11	2075	1.94	23.20	56.31	1.20	7	6	70	81	0.746	******	******	******	****	****
163	12	2076	1.94	23.20	69.35	1.07	5	4	60	84	0.705	******	******	******	****	****
163	13	2077	1.94	23.20	81.38	1.01	5	4	58	86	0.727	******	******	******	****	****
163	14	2078	1.94	23.20	80.86	1.01	5	4	53	86	0.664	******	******	******	****	****
163	15	2079	1.94	23.20	68.70	1.07	8	5	51	88	0.681	******	******	******	****	****
163	16	2080	1.94	23.20	55.65	1.21	6	5	49	88	0.654	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
163	17	2081	1.94	23.20	42.55	1.48	7	3	50	89	0.689	******	******	******	****	****
163	18	2082	1.94	23.20	29.59	2.02	5	2	50	89	0.689	******	******	******	****	****
163	19	2083	1.94	23.20	16.90	3.40	8	7	50	89	0.689	******	******	******	****	****
163	20	2084	1.94	23.20	5.73	10.98	3	1	53	87	0.685	******	******	******	****	****
163	21	2085	1.94	23.20	5.73	36.00	0	0	72	82	0.793	0.0	******	******	****	****
163	22	2086	1.94	23.20	5.73	36.00	0	0	81	78	0.783	0.0	******	******	****	****
163	23	2087	1.94	23.20	5.73	36.00	0	0	88	76	0.796	0.0	******	******	****	****
163	24	2088	1.94	23.20	5.73	36.00	0	0	92	76	0.833	0.0	******	******	****	****
164	1	2089	1.94	23.20	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
164	2	2090	1.94	23.20	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
164	3	2091	1.94	23.20	5.73	36.00	0	0	97	73	0.793	0.0	******	******	****	****
164	4	2092	1.94	23.20	5.73	36.00	0	0	98	72	0.775	0.0	******	******	****	****
164	5	2093	1.94	23.20	5.73	36.00	0	0	98	71	0.749	0.0	******	******	****	****
164	6	2094	1.94	23.20	5.73	36.00	4	4	99	70	0.732	0.0	******	******	****	****
164	7	2095	1.94	23.20	5.73	9.87	0	0	99	70	0.732	******	******	******	****	****
164	8	2096	1.94	23.20	17.57	3.28	0	0	99	70	0.732	******	******	******	****	****
164	9	2097	1.94	23.20	30.28	1.98	0	0	85	75	0.744	******	******	******	****	****
164	10	2098	1.94	23.20	43.25	1.46	0	0	72	79	0.719	******	******	******	****	****
164	11	2099	1.94	23.20	56.35	1.20	5	5	63	83	0.717	******	******	******	****	****
164	12	2100	1.94	23.20	69.39	1.07	5	5	53	85	0.643	******	******	******	****	****
164	13	2101	1.94	23.20	81.41	1.01	5	5	50	88	0.667	******	******	******	****	****
164	14	2102	1.94	23.20	80.83	1.01	5	5	46	90	0.654	******	******	******	****	****
164	15	2103	1.94	23.20	68.65	1.07	5	5	47	92	0.712	******	******	******	****	****
164	16	2104	1.94	23.20	55.60	1.21	3	3	50	92	0.757	******	******	******	****	****
164	17	2105	1.94	23.20	42.50	1.48	4	4	48	92	0.727	******	******	******	****	****
164	18	2106	1.94	23.20	29.54	2.02	8	6	48	92	0.727	******	******	******	****	****
164	19	2107	1.94	23.20	16.86	3.41	9	8	50	90	0.711	******	******	******	****	****
164	20	2108	1.94	23.20	5.73	11.06	7	7	53	89	0.730	******	******	******	****	****
164	21	2109	1.94	23.20	5.73	36.00	10	10	63	85	0.765	0.0	******	******	****	****
164	22	2110	1.94	23.20	5.73	36.00	10	10	93	80	0.960	0.0	******	******	****	****
164	23	2111	1.94	23.20	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
164	24	2112	1.94	23.20	5.73	36.00	8	7	99	73	0.810	0.0	******	******	****	****
165	1	2113	1.94	23.30	5.73	36.00	7	6	99	72	0.783	0.0	******	******	****	****
165	2	2114	1.94	23.30	5.73	36.00	6	2	100	72	0.791	0.0	******	******	****	****
165	3	2115	1.94	23.30	5.73	36.00	6	2	99	72	0.783	0.0	******	******	****	****
165	4	2116	1.94	23.30	5.73	36.00	5	2	99	72	0.783	0.0	******	******	****	****
165	5	2117	1.94	23.30	5.73	36.00	5	5	98	71	0.749	0.0	******	******	****	****
165	6	2118	1.94	23.30	5.73	36.00	9	8	96	70	0.709	0.0	******	******	****	****
165	7	2119	1.94	23.30	5.73	9.73	8	7	96	69	0.685	******	******	******	****	****
165	8	2120	1.94	23.30	17.66	3.26	7	6	94	70	0.695	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
165	9	2121	1.94	23.30	30.36	1.97	6	5	88	70	0.650	******	******	******	****	****
165	10	2122	1.94	23.30	43.32	1.45	7	5	82	73	0.671	******	******	******	****	****
165	11	2123	1.94	23.30	56.43	1.20	8	5	74	77	0.692	******	******	******	****	****
165	12	2124	1.94	23.30	69.47	1.07	8	8	65	80	0.671	******	******	******	****	****
165	13	2125	1.94	23.30	81.51	1.01	8	6	62	84	0.728	******	******	******	****	****
165	14	2126	1.94	23.30	80.86	1.01	10	8	62	84	0.728	******	******	******	****	****
165	15	2127	1.94	23.30	68.64	1.07	10	10	63	84	0.740	******	******	******	****	****
165	16	2128	1.94	23.30	55.59	1.21	10	10	70	83	0.797	******	******	******	****	****
165	17	2129	1.94	23.30	42.49	1.48	8	6	89	76	0.805	******	******	******	****	****
165	18	2130	1.94	23.30	29.54	2.02	10	8	87	76	0.787	******	******	******	****	****
165	19	2131	1.94	23.30	16.86	3.41	8	6	89	75	0.779	******	******	******	****	****
165	20	2132	1.94	23.30	5.73	11.05	3	2	89	74	0.753	******	******	******	****	****
165	21	2133	1.94	23.30	5.73	36.00	3	2	90	73	0.736	0.0	******	******	****	****
165	22	2134	1.94	23.30	5.73	36.00	3	1	92	72	0.728	0.0	******	******	****	****
165	23	2135	1.94	23.30	5.73	36.00	9	8	93	71	0.711	0.0	******	******	****	****
165	24	2136	1.94	23.30	5.73	36.00	3	2	95	70	0.702	0.0	******	******	****	****
166	1	2137	1.94	23.40	5.73	36.00	5	3	95	70	0.702	0.0	******	******	****	****
166	2	2138	1.94	23.40	5.73	36.00	10	10	96	70	0.709	0.0	******	******	****	****
166	3	2139	1.94	23.40	5.73	36.00	10	10	98	70	0.724	0.0	******	******	****	****
166	4	2140	1.94	23.40	5.73	36.00	10	10	99	70	0.732	0.0	******	******	****	****
166	5	2141	1.94	23.40	5.73	36.00	10	10	99	70	0.732	0.0	******	******	****	****
166	6	2142	1.94	23.40	5.73	36.00	10	10	100	70	0.739	0.0	******	******	****	****
166	7	2143	1.94	23.40	5.73	9.60	8	7	***	70	0.0	0.0	******	******	****	****
166	8	2144	1.94	23.40	17.74	3.25	4	3	***	74	0.0	7.80	******	******	****	****
166	9	2145	1.94	23.40	30.43	1.97	5	4	86	76	0.778	20.28	******	******	****	****
166	10	2146	1.94	23.40	43.40	1.45	7	5	80	79	0.799	******	******	******	****	****
166	11	2147	1.94	23.40	56.50	1.20	7	6	69	82	0.760	******	******	******	****	****
166	12	2148	1.94	23.40	69.55	1.07	7	6	65	84	0.764	******	******	******	****	****
166	13	2149	1.94	23.40	81.61	1.01	7	6	60	86	0.752	******	******	******	****	****
166	14	2150	1.94	23.40	80.89	1.01	7	5	55	86	0.689	******	******	******	****	****
166	15	2151	1.94	23.40	68.64	1.07	7	5	52	88	0.694	******	******	******	****	****
166	16	2152	1.94	23.40	55.58	1.21	6	6	51	88	0.681	******	******	******	****	****
166	17	2153	1.94	23.40	42.48	1.48	3	1	56	86	0.702	27.30	******	******	****	****
166	18	2154	1.94	23.40	29.53	2.02	6	2	56	86	0.702	19.50	******	******	****	****
166	19	2155	1.94	23.40	16.86	3.41	6	2	63	84	0.740	8.58	******	******	****	****
166	20	2156	1.94	23.40	5.73	11.02	6	1	69	80	0.712	0.0	******	******	****	****
166	21	2157	1.94	23.40	5.73	36.00	6	2	75	78	0.725	0.0	******	******	****	****
166	22	2158	1.94	23.40	5.73	36.00	3	1	82	76	0.742	0.0	******	******	****	****
166	23	2159	1.94	23.40	5.73	36.00	3	1	88	74	0.744	0.0	******	******	****	****
166	24	2160	1.94	23.40	5.73	36.00	2	1	91	72	0.720	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
167	1	2161	1.94	23.40	5.73	36.00	2	1	93	73	0.761	0.0	******	******	****	****
167	2	2162	1.94	23.40	5.73	36.00	2	1	94	72	0.744	0.0	******	******	****	****
167	3	2163	1.94	23.40	5.73	36.00	0	0	96	72	0.759	0.0	******	******	****	****
167	4	2164	1.94	23.40	5.73	36.00	0	0	97	71	0.741	0.0	******	******	****	****
167	5	2165	1.94	23.40	5.73	36.00	0	0	98	70	0.724	0.0	******	******	****	****
167	6	2166	1.94	23.40	5.73	36.00	2	2	99	70	0.732	0.0	******	******	****	****
167	7	2167	1.94	23.40	5.73	9.53	0	0	99	72	0.783	1.56	******	******	0.81	****
167	8	2168	1.94	23.40	17.78	3.24	0	0	98	74	0.829	16.38	******	******	0.79	****
167	9	2169	1.94	23.40	30.48	1.96	4	4	86	79	0.859	26.52	******	******	****	****
167	10	2170	1.94	23.40	43.44	1.45	5	5	80	80	0.826	******	******	******	****	****
167	11	2171	1.94	23.40	56.54	1.20	3	3	73	84	0.858	******	******	******	****	****
167	12	2172	1.94	23.40	69.59	1.07	7	4	62	85	0.753	******	******	******	****	****
167	13	2173	1.94	23.40	81.65	1.01	7	5	55	88	0.734	******	******	******	****	****
167	14	2174	1.94	23.40	80.85	1.01	9	8	53	90	0.754	******	******	******	****	****
167	15	2175	1.94	23.40	68.59	1.07	4	4	70	84	0.822	******	******	******	****	****
167	16	2176	1.94	23.40	55.53	1.21	5	3	69	84	0.811	******	******	******	****	****
167	17	2177	1.94	23.40	42.44	1.48	4	3	61	88	0.814	******	******	******	****	****
167	18	2178	1.94	23.40	29.49	2.02	4	4	62	86	0.777	21.84	******	******	****	****
167	19	2179	1.94	23.40	16.82	3.42	5	2	67	83	0.762	3.90	******	******	****	****
167	20	2180	1.94	23.40	5.73	11.10	1	1	73	80	0.753	1.56	******	******	****	****
167	21	2181	1.94	23.40	5.73	36.00	6	6	78	78	0.754	0.0	******	******	****	****
167	22	2182	1.94	23.40	5.73	36.00	3	3	83	78	0.803	0.0	******	******	****	****
167	23	2183	1.94	23.40	5.73	36.00	0	0	87	77	0.813	0.0	******	******	****	****
167	24	2184	1.94	23.40	5.73	36.00	0	0	91	76	0.824	0.0	******	******	****	****
168	1	2185	1.94	23.50	5.73	36.00	0	0	94	74	0.795	0.0	******	******	****	****
168	2	2186	1.94	23.50	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
168	3	2187	1.94	23.50	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
168	4	2188	1.94	23.50	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
168	5	2189	1.94	23.50	5.73	36.00	3	3	98	72	0.775	0.0	******	******	****	****
168	6	2190	1.94	23.50	5.73	36.00	3	3	99	72	0.783	0.0	******	******	****	****
168	7	2191	1.94	23.50	5.73	9.40	6	6	99	73	0.810	9.36	******	******	****	****
168	8	2192	1.94	23.50	17.86	3.23	3	1	99	75	0.866	24.96	******	******	****	****
168	9	2193	1.94	23.50	30.56	1.96	7	6	92	80	0.949	******	******	******	****	****
168	10	2194	1.94	23.50	43.52	1.45	7	6	76	82	0.838	******	******	******	****	****
168	11	2195	1.94	23.50	56.62	1.20	5	5	70	85	0.850	******	******	******	****	****
168	12	2196	1.94	23.50	69.67	1.07	5	5	60	89	0.827	******	******	******	****	****
168	13	2197	1.94	23.50	81.75	1.01	6	6	53	90	0.754	******	******	******	****	****
168	14	2198	1.94	23.50	80.88	1.01	5	5	52	92	0.787	******	******	******	****	****
168	15	2199	1.94	23.50	68.58	1.07	4	4	50	91	0.733	******	******	******	****	****
168	16	2200	1.94	23.50	55.52	1.21	5	4	53	91	0.778	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
168	17	2201	1.94	23.50	42.42	1.48	4	4	57	88	0.761	******	******	******	****	****
168	18	2202	1.94	23.50	29.48	2.02	3	2	62	87	0.802	******	******	******	****	****
168	19	2203	1.94	23.50	16.81	3.42	1	1	63	86	0.789	4.68	******	******	****	****
168	20	2204	1.94	23.50	5.73	11.09	1	1	66	83	0.751	0.0	******	******	****	****
168	21	2205	1.94	23.50	5.73	36.00	0	0	74	80	0.764	0.0	******	******	****	****
168	22	2206	1.94	23.50	5.73	36.00	0	0	80	79	0.799	0.0	******	******	****	****
168	23	2207	1.94	23.50	5.73	36.00	0	0	85	78	0.822	0.0	******	******	****	****
168	24	2208	1.94	23.50	5.73	36.00	0	0	91	76	0.824	0.0	******	******	****	****
169	1	2209	1.94	23.50	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
169	2	2210	1.94	23.50	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
169	3	2211	1.94	23.50	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
169	4	2212	1.94	23.50	5.73	36.00	0	0	99	73	0.810	0.0	******	******	****	****
169	5	2213	1.94	23.50	5.73	36.00	0	0	100	72	0.791	0.0	******	******	****	****
169	6	2214	1.94	23.50	5.73	36.00	0	0	100	72	0.791	0.0	******	******	****	****
169	7	2215	1.94	23.50	5.73	9.35	0	0	100	72	0.791	0.78	******	******	0.75	****
169	8	2216	1.94	23.50	17.90	3.22	1	1	100	74	0.846	******	******	******	****	****
169	9	2217	1.94	23.50	30.60	1.96	2	2	83	79	0.829	******	******	******	****	****
169	10	2218	1.94	23.50	43.56	1.45	6	6	70	82	0.771	******	******	******	****	****
169	11	2219	1.94	23.50	56.66	1.20	6	6	60	85	0.728	******	******	******	****	****
169	12	2220	1.94	23.50	69.71	1.07	6	6	53	88	0.708	******	******	******	****	****
169	13	2221	1.94	23.50	81.78	1.01	6	4	51	90	0.725	******	******	******	****	****
169	14	2222	1.94	23.50	80.84	1.01	6	4	47	92	0.712	******	******	******	****	****
169	15	2223	1.94	23.50	68.54	1.07	5	5	44	94	0.708	******	******	******	****	****
169	16	2224	1.94	23.50	55.47	1.21	5	5	44	94	0.708	******	******	******	****	****
169	17	2225	1.94	23.50	42.38	1.48	4	3	45	94	0.724	******	******	******	****	****
169	18	2226	1.94	23.50	29.44	2.03	0	0	45	93	0.702	24.18	******	******	0.65	****
169	19	2227	1.94	23.50	16.78	3.42	0	0	47	92	0.712	10.92	******	******	0.72	****
169	20	2228	1.94	23.50	5.73	11.16	0	0	53	87	0.685	0.78	******	******	0.79	****
169	21	2229	1.94	23.50	5.73	36.00	0	0	74	83	0.842	0.0	******	******	****	****
169	22	2230	1.94	23.50	5.73	36.00	4	1	76	81	0.810	0.0	******	******	****	****
169	23	2231	1.94	23.50	5.73	36.00	0	0	80	80	0.826	0.0	******	******	****	****
169	24	2232	1.94	23.50	5.73	36.00	0	0	86	78	0.832	0.0	******	******	****	****
170	1	2233	1.93	23.50	5.73	36.00	0	0	91	76	0.824	0.0	******	******	****	****
170	2	2234	1.93	23.50	5.73	36.00	0	0	91	76	0.824	0.0	******	******	****	****
170	3	2235	1.93	23.50	5.73	36.00	0	0	93	74	0.787	0.0	******	******	****	****
170	4	2236	1.93	23.50	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
170	5	2237	1.93	23.50	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
170	6	2238	1.93	23.50	5.73	36.00	3	1	96	73	0.785	0.0	******	******	****	****
170	7	2239	1.93	23.50	5.73	9.29	0	0	96	74	0.812	10.14	******	******	0.99	****
170	8	2240	1.93	23.50	17.95	3.21	0	0	96	75	0.840	27.30	******	******	0.92	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
170	9	2241	1.93	23.50	30.64	1.96	0	0	88	80	0.908	46.02	******	******	0.88	****
170	10	2242	1.93	23.50	43.61	1.45	0	0	80	84	0.940	60.84	******	******	0.83	****
170	11	2243	1.93	23.50	56.70	1.20	1	1	69	87	0.892	74.88	******	******	****	****
170	12	2244	1.93	23.50	69.75	1.07	6	6	62	90	0.882	******	******	******	****	****
170	13	2245	1.93	23.50	81.82	1.01	6	6	57	92	0.863	******	******	******	****	****
170	14	2246	1.93	23.50	80.81	1.01	6	6	52	94	0.837	******	******	******	****	****
170	15	2247	1.93	23.50	68.50	1.07	7	6	50	96	0.856	******	******	******	****	****
170	16	2248	1.93	23.50	55.43	1.21	8	7	50	96	0.856	45.24	******	******	****	****
170	17	2249	1.93	23.50	42.34	1.48	9	8	70	88	0.934	10.14	******	******	****	****
170	18	2250	1.93	23.50	29.40	2.03	9	8	95	74	0.804	7.80	******	******	****	****
170	19	2251	1.93	23.50	16.73	3.43	9	7	98	74	0.829	3.90	******	******	****	****
170	20	2252	1.93	23.50	5.73	11.24	8	3	98	75	0.857	0.78	******	******	****	****
170	21	2253	1.93	23.50	5.73	36.00	7	2	99	75	0.866	0.0	******	******	****	****
170	22	2254	1.93	23.50	5.73	36.00	8	3	100	76	0.905	0.0	******	******	****	****
170	23	2255	1.93	23.50	5.73	36.00	8	2	100	76	0.905	0.0	******	******	****	****
170	24	2256	1.93	23.50	5.73	36.00	7	3	100	76	0.905	0.0	******	******	****	****
171	1	2257	1.93	23.40	5.73	36.00	4	1	100	76	0.905	0.0	******	******	****	****
171	2	2258	1.93	23.40	5.73	36.00	2	1	100	76	0.905	0.0	******	******	****	****
171	3	2259	1.93	23.40	5.73	36.00	0	0	100	76	0.905	0.0	******	******	****	****
171	4	2260	1.93	23.40	5.73	36.00	0	0	100	76	0.905	0.0	******	******	****	****
171	5	2261	1.93	23.40	5.73	36.00	0	0	100	75	0.875	0.0	******	******	****	****
171	6	2262	1.93	23.40	5.73	36.00	5	5	100	75	0.875	0.0	******	******	****	****
171	7	2263	1.93	23.40	5.73	9.30	8	8	100	75	0.875	6.24	******	******	****	****
171	8	2264	1.93	23.40	17.95	3.21	9	9	100	76	0.905	16.38	******	******	****	****
171	9	2265	1.93	23.40	30.65	1.95	5	5	100	80	1.032	37.44	******	******	****	****
171	10	2266	1.93	23.40	43.62	1.45	0	0	90	84	1.057	53.04	******	******	0.75	****
171	11	2267	1.93	23.40	56.72	1.19	0	0	72	87	0.931	70.98	******	******	0.77	****
171	12	2268	1.93	23.40	69.76	1.07	4	4	62	90	0.882	******	******	******	****	****
171	13	2269	1.93	23.40	81.78	1.01	6	6	58	92	0.878	******	******	******	****	****
171	14	2270	1.93	23.40	80.71	1.01	7	7	55	93	0.859	******	******	******	****	****
171	15	2271	1.93	23.40	68.42	1.07	9	7	70	82	0.771	******	******	******	****	****
171	16	2272	1.93	23.40	55.35	1.21	8	7	72	83	0.819	6.24	******	******	****	****
171	17	2273	1.93	23.40	42.26	1.48	9	7	70	82	0.771	6.24	******	******	****	****
171	18	2274	1.93	23.40	29.32	2.03	10	9	72	82	0.793	6.24	******	******	****	****
171	19	2275	1.93	23.40	16.65	3.45	10	10	73	82	0.804	2.34	******	******	****	****
171	20	2276	1.93	23.40	5.73	11.43	10	9	76	80	0.784	0.0	******	******	****	****
171	21	2277	1.93	23.40	5.73	36.00	10	8	86	80	0.888	0.0	******	******	****	****
171	22	2278	1.93	23.40	5.73	36.00	10	8	85	78	0.822	0.0	******	******	****	****
171	23	2279	1.93	23.40	5.73	36.00	10	8	80	78	0.774	0.0	******	******	****	****
171	24	2280	1.93	23.40	5.73	36.00	10	6	87	76	0.787	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
172	1	2281	1.93	23.40	5.73	36.00	6	2	93	74	0.787	0.0	******	******	****	****
172	2	2282	1.93	23.40	5.73	36.00	7	2	95	74	0.804	0.0	******	******	****	****
172	3	2283	1.93	23.40	5.73	36.00	4	1	96	74	0.812	0.0	******	******	****	****
172	4	2284	1.93	23.40	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
172	5	2285	1.93	23.40	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
172	6	2286	1.93	23.40	5.73	36.00	2	1	98	73	0.802	0.0	******	******	****	****
172	7	2287	1.93	23.40	5.73	9.22	2	1	98	73	0.802	9.75	******	******	****	****
172	8	2288	1.93	23.40	18.01	3.20	0	0	98	76	0.887	28.47	******	******	0.93	****
172	9	2289	1.93	23.40	30.71	1.95	0	0	91	79	0.909	27.69	******	******	0.68	****
172	10	2290	1.93	23.40	43.68	1.45	0	0	82	83	0.933	64.35	******	******	0.86	****
172	11	2291	1.93	23.40	56.78	1.19	2	2	76	86	0.952	76.83	******	******	****	****
172	12	2292	1.93	23.40	69.83	1.06	2	2	65	90	0.924	******	******	******	****	****
172	13	2293	1.93	23.40	81.83	1.01	2	2	60	92	0.908	******	******	******	****	****
172	14	2294	1.93	23.40	80.65	1.01	3	3	57	94	0.918	******	******	******	****	****
172	15	2295	1.93	23.40	68.36	1.08	3	3	53	95	0.880	******	******	******	****	****
172	16	2296	1.93	23.40	55.29	1.22	7	6	51	94	0.821	42.51	******	******	****	****
172	17	2297	1.93	23.40	42.20	1.49	8	7	51	93	0.796	15.21	******	******	****	****
172	18	2298	1.93	23.40	29.25	2.04	10	9	70	85	0.850	13.65	******	******	****	****
172	19	2299	1.93	23.40	16.59	3.46	9	7	71	86	0.890	13.65	******	******	****	****
172	20	2300	1.93	23.40	5.73	11.55	8	7	72	85	0.874	0.39	******	******	****	****
172	21	2301	1.93	23.40	5.73	36.00	7	6	80	82	0.882	0.0	******	******	****	****
172	22	2302	1.93	23.40	5.73	36.00	7	6	85	80	0.877	0.0	******	******	****	****
172	23	2303	1.93	23.40	5.73	36.00	3	3	90	79	0.899	0.0	******	******	****	****
172	24	2304	1.93	23.40	5.73	36.00	3	3	90	78	0.870	0.0	******	******	****	****
173	1	2305	1.93	23.30	5.73	36.00	3	1	89	78	0.861	0.0	******	******	****	****
173	2	2306	1.93	23.30	5.73	36.00	2	1	90	76	0.814	0.0	******	******	****	****
173	3	2307	1.93	23.30	5.73	36.00	0	0	94	75	0.822	0.0	******	******	****	****
173	4	2308	1.93	23.30	5.73	36.00	0	0	97	75	0.849	0.0	******	******	****	****
173	5	2309	1.93	23.30	5.73	36.00	2	2	98	74	0.829	0.0	******	******	****	****
173	6	2310	1.93	23.30	5.73	36.00	6	2	98	74	0.829	0.0	******	******	****	****
173	7	2311	1.93	23.30	5.73	9.23	8	3	98	74	0.829	11.31	******	******	****	****
173	8	2312	1.93	23.30	18.01	3.20	7	2	94	76	0.851	25.35	******	******	****	****
173	9	2313	1.93	23.30	30.72	1.95	4	1	90	79	0.899	******	******	******	****	****
173	10	2314	1.93	23.30	43.69	1.45	5	3	86	82	0.948	57.33	******	******	****	****
173	11	2315	1.93	23.30	56.80	1.19	4	2	78	84	0.916	68.25	******	******	****	****
173	12	2316	1.93	23.30	69.83	1.06	6	2	68	89	0.937	******	******	******	****	****
173	13	2317	1.93	23.30	81.79	1.01	8	5	60	93	0.937	******	******	******	****	****
173	14	2318	1.93	23.30	80.56	1.01	9	6	49	92	0.742	33.93	******	******	****	****
173	15	2319	1.93	23.30	68.28	1.08	9	8	65	86	0.814	18.33	******	******	****	****
173	16	2320	1.93	23.30	55.21	1.22	8	7	73	82	0.804	5.07	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
173	17	2321	1.93	23.30	42.12	1.49	8	7	79	80	0.815	5.07	******	******	****	****
173	18	2322	1.93	23.30	29.17	2.04	9	8	81	79	0.809	6.63	******	******	****	****
173	19	2323	1.93	23.30	16.50	3.48	10	10	80	80	0.826	4.29	******	******	****	****
173	20	2324	1.93	23.30	5.73	11.74	10	10	79	79	0.789	0.39	******	******	****	****
173	21	2325	1.93	23.30	5.73	36.00	10	10	81	78	0.783	0.0	******	******	****	****
173	22	2326	1.93	23.30	5.73	36.00	8	6	88	77	0.823	0.0	******	******	****	****
173	23	2327	1.93	23.30	5.73	36.00	4	3	90	76	0.814	0.0	******	******	****	****
173	24	2328	1.93	23.30	5.73	36.00	4	2	94	76	0.851	0.0	******	******	****	****
174	1	2329	1.93	23.30	5.73	36.00	3	1	98	74	0.829	0.0	******	******	****	****
174	2	2330	1.93	23.30	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
174	3	2331	1.93	23.30	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
174	4	2332	1.93	23.30	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
174	5	2333	1.93	23.30	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
174	6	2334	1.93	23.30	5.73	36.00	4	1	99	73	0.810	0.0	******	******	****	****
174	7	2335	1.93	23.30	5.75	9.18	7	2	99	74	0.838	8.97	******	******	****	****
174	8	2336	1.93	23.30	18.05	3.20	3	1	98	76	0.887	26.91	******	******	****	****
174	9	2337	1.93	23.30	30.76	1.95	0	0	80	80	0.826	38.61	******	******	0.80	****
174	10	2338	1.93	23.30	43.74	1.44	0	0	70	82	0.771	58.89	******	******	0.81	****
174	11	2339	1.93	23.30	56.84	1.19	2	2	65	86	0.814	72.15	******	******	****	****
174	12	2340	1.93	23.30	69.88	1.06	5	4	59	89	0.813	******	******	******	****	****
174	13	2341	1.93	23.30	81.82	1.01	7	7	53	91	0.778	******	******	******	****	****
174	14	2342	1.93	23.30	80.52	1.01	7	6	52	92	0.787	******	******	******	****	****
174	15	2343	1.93	23.30	68.24	1.08	6	6	50	93	0.780	******	******	******	****	****
174	16	2344	1.93	23.30	55.17	1.22	5	5	48	94	0.773	62.01	******	******	****	****
174	17	2345	1.93	23.30	42.08	1.49	5	5	49	96	0.839	46.41	******	******	****	****
174	18	2346	1.93	23.30	29.13	2.05	7	6	65	85	0.789	9.75	******	******	****	****
174	19	2347	1.93	23.30	16.46	3.49	8	8	89	76	0.805	1.95	******	******	****	****
174	20	2348	1.93	23.30	5.73	11.82	10	8	89	75	0.779	0.39	******	******	****	****
174	21	2349	1.93	23.30	5.73	36.00	10	8	95	73	0.777	0.0	******	******	****	****
174	22	2350	1.93	23.30	5.73	36.00	10	8	95	73	0.777	0.0	******	******	****	****
174	23	2351	1.93	23.30	5.73	36.00	10	8	95	73	0.777	0.0	******	******	****	****
174	24	2352	1.93	23.30	5.73	36.00	10	10	93	73	0.761	0.0	******	******	****	****
175	1	2353	1.93	23.20	5.73	36.00	10	9	94	73	0.769	0.0	******	******	****	****
175	2	2354	1.93	23.20	5.73	36.00	8	7	96	72	0.759	0.0	******	******	****	****
175	3	2355	1.93	23.20	5.73	36.00	9	4	97	72	0.767	0.0	******	******	****	****
175	4	2356	1.93	23.20	5.73	36.00	9	3	98	72	0.775	0.0	******	******	****	****
175	5	2357	1.93	23.20	5.73	36.00	7	3	98	71	0.749	0.0	******	******	****	****
175	6	2358	1.93	23.20	5.73	36.00	8	4	98	70	0.724	0.0	******	******	****	****
175	7	2359	1.93	23.20	5.74	9.19	10	9	99	72	0.783	9.75	******	******	****	****
175	8	2360	1.93	23.20	18.05	3.20	10	8	98	74	0.829	12.09	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
175	9	2361	1.93	23.20	30.77	1.95	8	7	96	75	0.840	19.89	******	******	****	****
175	10	2362	1.93	23.20	43.75	1.44	9	4	83	79	0.829	47.19	******	******	****	****
175	11	2363	1.93	23.20	56.85	1.19	9	7	75	82	0.826	56.55	******	******	****	****
175	12	2364	1.93	23.20	69.88	1.06	10	7	70	84	0.822	48.75	******	******	****	****
175	13	2365	1.93	23.20	81.78	1.01	10	5	70	88	0.934	******	******	******	****	****
175	14	2366	1.93	23.20	80.42	1.01	7	3	63	89	0.868	******	******	******	****	****
175	15	2367	1.93	23.20	68.16	1.08	7	3	62	90	0.882	******	******	******	****	****
175	16	2368	1.93	23.20	55.10	1.22	8	4	61	90	0.867	65.13	******	******	****	****
175	17	2369	1.93	23.20	42.00	1.49	9	6	60	89	0.827	33.15	******	******	****	****
175	18	2370	1.93	23.20	29.05	2.05	10	7	67	86	0.840	8.19	******	******	****	****
175	19	2371	1.93	23.20	16.38	3.50	10	8	72	85	0.874	5.07	******	******	****	****
175	20	2372	1.93	23.20	5.73	12.03	10	10	77	84	0.905	0.39	******	******	****	****
175	21	2373	1.93	23.20	5.73	36.00	10	9	83	82	0.915	0.0	******	******	****	****
175	22	2374	1.93	23.20	5.73	36.00	10	10	89	80	0.918	0.0	******	******	****	****
175	23	2375	1.93	23.20	5.73	36.00	9	9	85	78	0.822	0.0	******	******	****	****
175	24	2376	1.93	23.20	5.73	36.00	10	10	90	74	0.761	0.0	******	******	****	****
176	1	2377	1.93	23.20	5.73	36.00	8	6	99	72	0.783	0.0	******	******	****	****
176	2	2378	1.93	23.20	5.73	36.00	8	6	100	72	0.791	0.0	******	******	****	****
176	3	2379	1.93	23.20	5.73	36.00	9	8	100	72	0.791	0.0	******	******	****	****
176	4	2380	1.93	23.20	5.73	36.00	10	10	100	73	0.818	0.0	******	******	****	****
176	5	2381	1.93	23.20	5.73	36.00	10	10	100	73	0.818	0.0	******	******	****	****
176	6	2382	1.93	23.20	5.73	36.00	10	10	100	73	0.818	0.0	******	******	****	****
176	7	2383	1.93	23.20	5.80	9.11	10	9	100	74	0.846	4.68	******	******	****	****
176	8	2384	1.93	23.20	18.11	3.18	10	10	100	77	0.935	14.04	******	******	****	****
176	9	2385	1.93	23.20	30.83	1.94	7	5	94	80	0.970	37.44	******	******	****	****
176	10	2386	1.93	23.20	43.81	1.44	8	5	87	80	0.898	48.36	******	******	****	****
176	11	2387	1.93	23.20	56.92	1.19	9	6	80	83	0.910	51.48	******	******	****	****
176	12	2388	1.93	23.20	69.95	1.06	10	10	72	84	0.846	37.44	******	******	****	****
176	13	2389	1.93	23.20	81.83	1.01	10	10	98	76	0.887	15.60	******	******	****	****
176	14	2390	1.93	23.20	80.37	1.01	10	10	100	75	0.875	6.24	******	******	****	****
176	15	2391	1.93	23.20	68.10	1.08	10	10	100	74	0.846	2.34	******	******	****	****
176	16	2392	1.93	23.20	55.03	1.22	10	10	100	73	0.818	6.24	******	******	****	****
176	17	2393	1.93	23.20	41.94	1.49	10	10	100	74	0.846	15.60	******	******	****	****
176	18	2394	1.93	23.20	28.99	2.06	10	10	100	74	0.846	2.34	******	******	****	****
176	19	2395	1.93	23.20	16.32	3.52	10	10	100	72	0.791	0.0	******	******	****	****
176	20	2396	1.93	23.20	5.73	12.16	10	10	100	72	0.791	0.0	******	******	****	****
176	21	2397	1.93	23.20	5.73	36.00	10	9	100	72	0.791	0.0	******	******	****	****
176	22	2398	1.93	23.20	5.73	36.00	10	7	100	72	0.791	0.0	******	******	****	****
176	23	2399	1.93	23.20	5.73	36.00	10	10	100	72	0.791	0.0	******	******	****	****
176	24	2400	1.93	23.20	5.73	36.00	10	10	100	72	0.791	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
177	1	2401	1.93	23.20	5.73	36.00	7	7	100	72	0.791	0.0	******	******	****	****
177	2	2402	1.93	23.20	5.73	36.00	7	4	100	73	0.818	0.0	******	******	****	****
177	3	2403	1.93	23.20	5.73	36.00	10	9	100	73	0.818	0.0	******	******	****	****
177	4	2404	1.93	23.20	5.73	36.00	9	7	100	73	0.818	0.0	******	******	****	****
177	5	2405	1.93	23.20	5.73	36.00	5	3	100	73	0.818	0.0	******	******	****	****
177	6	2406	1.93	23.20	5.73	36.00	8	7	100	73	0.818	0.0	******	******	****	****
177	7	2407	1.93	23.20	5.84	9.05	10	10	100	74	0.846	7.02	******	******	****	****
177	8	2408	1.93	23.20	18.16	3.18	9	8	100	75	0.875	4.68	******	******	****	****
177	9	2409	1.93	23.20	30.88	1.94	6	3	98	76	0.887	37.44	******	******	****	****
177	10	2410	1.93	23.20	43.86	1.44	10	10	93	80	0.960	37.44	******	******	****	****
177	11	2411	1.93	23.20	56.96	1.19	10	9	93	80	0.960	33.54	******	******	****	****
177	12	2412	1.93	23.20	69.99	1.06	10	10	97	76	0.878	17.94	******	******	****	****
177	13	2413	1.93	23.20	81.86	1.01	8	6	100	74	0.846	30.42	******	******	****	****
177	14	2414	1.93	23.20	80.33	1.01	6	3	90	78	0.870	******	******	******	****	****
177	15	2415	1.93	23.20	68.05	1.08	9	7	80	83	0.910	******	******	******	****	****
177	16	2416	1.93	23.20	54.99	1.22	10	9	73	85	0.886	40.56	******	******	****	****
177	17	2417	1.93	23.20	41.89	1.49	10	10	90	80	0.929	10.14	******	******	****	****
177	18	2418	1.93	23.20	28.95	2.06	10	9	92	78	0.890	11.70	******	******	****	****
177	19	2419	1.93	23.20	16.27	3.53	10	8	95	77	0.888	5.46	******	******	****	****
177	20	2420	1.93	23.20	5.73	12.25	7	4	96	77	0.898	0.0	******	******	****	****
177	21	2421	1.93	23.20	5.73	36.00	3	2	96	76	0.869	0.0	******	******	****	****
177	22	2422	1.93	23.20	5.73	36.00	3	2	96	76	0.869	0.0	******	******	****	****
177	23	2423	1.93	23.20	5.73	36.00	7	6	97	76	0.878	0.0	******	******	****	****
177	24	2424	1.93	23.20	5.73	36.00	3	2	97	76	0.878	0.0	******	******	****	****
178	1	2425	1.93	23.20	5.73	36.00	3	2	98	76	0.887	0.0	******	******	****	****
178	2	2426	1.93	23.20	5.73	36.00	7	6	99	76	0.896	0.0	******	******	****	****
178	3	2427	1.93	23.20	5.73	36.00	3	2	99	75	0.866	0.0	******	******	****	****
178	4	2428	1.93	23.20	5.73	36.00	1	1	99	74	0.838	0.0	******	******	****	****
178	5	2429	1.93	23.20	5.73	36.00	7	6	99	74	0.838	0.0	******	******	****	****
178	6	2430	1.93	23.20	5.73	36.00	8	4	100	74	0.846	0.0	******	******	****	****
178	7	2431	1.93	23.20	5.88	9.00	10	10	100	74	0.846	1.56	******	******	****	****
178	8	2432	1.93	23.20	18.20	3.17	9	6	100	71	0.764	10.14	******	******	****	****
178	9	2433	1.93	23.20	30.92	1.94	10	9	98	74	0.829	31.20	******	******	****	****
178	10	2434	1.93	23.20	43.90	1.44	10	9	95	79	0.949	49.14	******	******	****	****
178	11	2435	1.93	23.20	57.01	1.19	9	7	90	82	0.992	42.90	******	******	****	****
178	12	2436	1.93	23.20	70.03	1.06	8	7	88	80	0.908	******	******	******	****	****
178	13	2437	1.93	23.20	81.89	1.01	6	6	70	87	0.905	******	******	******	****	****
178	14	2438	1.93	23.20	80.30	1.01	4	3	68	88	0.908	******	******	******	****	****
178	15	2439	1.93	23.20	68.01	1.08	5	4	64	88	0.854	******	******	******	****	****
178	16	2440	1.93	23.20	54.94	1.22	4	3	63	88	0.841	54.60	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
178	17	2441	1.93	23.20	41.85	1.50	3	3	64	88	0.854	46.80	******	******	****	****
178	18	2442	1.93	23.20	28.90	2.06	6	6	64	88	0.854	27.30	******	******	****	****
178	19	2443	1.93	23.20	16.23	3.53	8	5	72	86	0.902	10.92	******	******	****	****
178	20	2444	1.93	23.20	5.73	12.35	8	6	80	83	0.910	0.78	******	******	****	****
178	21	2445	1.93	23.20	5.73	36.00	10	10	87	80	0.898	0.0	******	******	****	****
178	22	2446	1.93	23.20	5.73	36.00	4	2	97	70	0.717	0.0	******	******	****	****
178	23	2447	1.93	23.20	5.73	36.00	5	3	99	70	0.732	0.0	******	******	****	****
178	24	2448	1.93	23.20	5.73	36.00	7	4	99	70	0.732	0.0	******	******	****	****
179	1	2449	1.93	23.20	5.73	36.00	7	6	99	70	0.732	0.0	******	******	****	****
179	2	2450	1.93	23.20	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
179	3	2451	1.93	23.20	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****
179	4	2452	1.93	23.20	5.73	36.00	10	10	99	74	0.838	0.0	******	******	****	****
179	5	2453	1.93	23.20	5.73	36.00	10	10	97	73	0.793	0.0	******	******	****	****
179	6	2454	1.93	23.20	5.73	36.00	8	6	97	73	0.793	0.0	******	******	****	****
179	7	2455	1.93	23.20	5.92	8.95	9	6	97	73	0.793	7.41	******	******	****	****
179	8	2456	1.93	23.20	18.24	3.16	9	8	97	74	0.821	21.45	******	******	****	****
179	9	2457	1.93	23.20	30.96	1.94	8	3	96	77	0.898	41.73	******	******	****	****
179	10	2458	1.93	23.20	43.94	1.44	9	8	85	79	0.849	52.65	******	******	****	****
179	11	2459	1.93	23.20	57.05	1.19	9	4	80	80	0.826	******	******	******	****	****
179	12	2460	1.93	23.20	70.07	1.06	9	7	75	82	0.826	******	******	******	****	****
179	13	2461	1.93	23.20	81.92	1.01	9	6	70	85	0.850	******	******	******	****	****
179	14	2462	1.93	23.20	80.26	1.01	9	6	68	86	0.852	******	******	******	****	****
179	15	2463	1.93	23.20	67.97	1.08	10	8	65	86	0.814	******	******	******	****	****
179	16	2464	1.93	23.20	54.90	1.22	10	8	65	86	0.814	34.71	******	******	****	****
179	17	2465	1.93	23.20	41.81	1.50	10	9	70	85	0.850	27.69	******	******	****	****
179	18	2466	1.93	23.20	28.86	2.06	10	8	81	84	0.952	19.11	******	******	****	****
179	19	2467	1.93	23.20	16.19	3.54	10	8	82	84	0.963	15.99	******	******	****	****
179	20	2468	1.93	23.20	5.73	12.44	10	7	86	81	0.917	3.51	******	******	****	****
179	21	2469	1.93	23.20	5.73	36.00	9	7	93	79	0.929	0.0	******	******	****	****
179	22	2470	1.93	23.20	5.73	36.00	9	7	90	78	0.870	0.0	******	******	****	****
179	23	2471	1.93	23.20	5.73	36.00	5	3	90	76	0.814	0.0	******	******	****	****
179	24	2472	1.93	23.20	5.73	36.00	3	2	92	74	0.778	0.0	******	******	****	****
180	1	2473	1.93	23.10	5.73	36.00	2	1	93	74	0.787	0.0	******	******	****	****
180	2	2474	1.93	23.10	5.73	36.00	3	1	95	73	0.777	0.0	******	******	****	****
180	3	2475	1.93	23.10	5.73	36.00	3	1	96	72	0.759	0.0	******	******	****	****
180	4	2476	1.93	23.10	5.73	36.00	4	1	97	72	0.767	0.0	******	******	****	****
180	5	2477	1.93	23.10	5.73	36.00	4	2	98	71	0.749	0.0	******	******	****	****
180	6	2478	1.93	23.10	5.73	36.00	0	0	98	71	0.749	0.0	******	******	****	****
180	7	2479	1.93	23.10	5.91	8.96	3	1	***	71	0.0	4.29	******	******	****	****
180	8	2480	1.93	23.10	18.24	3.16	3	1	***	72	0.0	18.33	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
180	9	2481	1.93	23.10	30.97	1.94	7	3	86	74	0.728	33.93	******	******	****	****
180	10	2482	1.93	23.10	43.96	1.44	8	6	80	78	0.774	51.09	******	******	****	****
180	11	2483	1.93	23.10	57.06	1.19	8	7	71	80	0.733	******	******	******	****	****
180	12	2484	1.93	23.10	70.08	1.06	8	7	65	82	0.716	******	******	******	****	****
180	13	2485	1.93	23.10	81.88	1.01	8	8	62	84	0.728	******	******	******	****	****
180	14	2486	1.93	23.10	80.16	1.01	8	8	59	84	0.693	******	******	******	****	****
180	15	2487	1.93	23.10	67.89	1.08	8	8	56	85	0.680	53.43	******	******	****	****
180	16	2488	1.93	23.10	54.83	1.22	8	8	52	85	0.631	48.75	******	******	****	****
180	17	2489	1.93	23.10	41.73	1.50	9	8	56	84	0.658	41.73	******	******	****	****
180	18	2490	1.93	23.10	28.78	2.07	8	7	56	84	0.658	30.81	******	******	****	****
180	19	2491	1.93	23.10	16.11	3.56	8	5	58	81	0.618	16.77	******	******	****	****
180	20	2492	1.93	23.10	5.73	12.66	8	7	62	78	0.600	1.95	******	******	****	****
180	21	2493	1.93	23.10	5.73	36.00	7	3	68	75	0.595	0.0	******	******	****	****
180	22	2494	1.93	23.10	5.73	36.00	7	3	73	73	0.597	0.0	******	******	****	****
180	23	2495	1.93	23.10	5.73	36.00	4	1	75	71	0.573	0.0	******	******	****	****
180	24	2496	1.93	23.10	5.73	36.00	2	1	80	70	0.591	0.0	******	******	****	****
181	1	2497	1.93	23.10	5.73	36.00	0	0	85	69	0.607	0.0	******	******	****	****
181	2	2498	1.93	23.10	5.73	36.00	2	2	88	68	0.607	0.0	******	******	****	****
181	3	2499	1.93	23.10	5.73	36.00	2	2	90	68	0.621	0.0	******	******	****	****
181	4	2500	1.93	23.10	5.73	36.00	0	0	92	68	0.635	0.0	******	******	****	****
181	5	2501	1.93	23.10	5.73	36.00	0	0	93	68	0.642	0.0	******	******	****	****
181	6	2502	1.93	23.10	5.73	36.00	1	1	95	68	0.655	0.0	******	******	****	****
181	7	2503	1.93	23.10	5.95	8.91	8	6	96	68	0.662	3.12	******	******	****	****
181	8	2504	1.93	23.10	18.28	3.16	3	2	96	68	0.662	11.70	******	******	****	****
181	9	2505	1.93	23.10	31.02	1.93	8	6	96	74	0.812	32.76	******	******	****	****
181	10	2506	1.93	23.10	44.00	1.44	4	4	83	78	0.803	31.98	******	******	****	****
181	11	2507	1.93	23.10	57.11	1.19	5	5	72	81	0.768	******	******	******	****	****
181	12	2508	1.93	23.10	70.13	1.06	6	5	62	85	0.753	******	******	******	****	****
181	13	2509	1.93	23.10	81.91	1.01	5	5	56	87	0.724	******	******	******	****	****
181	14	2510	1.93	23.10	80.13	1.01	5	5	52	89	0.717	******	******	******	****	****
181	15	2511	1.93	23.10	67.84	1.08	4	4	49	90	0.697	******	******	******	****	****
181	16	2512	1.93	23.10	54.78	1.22	3	3	49	90	0.697	51.48	******	******	****	****
181	17	2513	1.93	23.10	41.69	1.50	0	0	49	90	0.697	47.58	******	******	0.72	****
181	18	2514	1.93	23.10	28.74	2.07	0	0	49	90	0.697	41.34	******	******	0.87	****
181	19	2515	1.93	23.10	16.06	3.57	0	0	49	89	0.675	21.84	******	******	0.90	****
181	20	2516	1.93	23.10	5.73	12.77	0	0	54	84	0.634	3.90	******	******	0.92	****
181	21	2517	1.93	23.10	5.73	36.00	0	0	67	78	0.648	0.0	******	******	****	****
181	22	2518	1.93	23.10	5.73	36.00	0	0	75	76	0.679	0.0	******	******	****	****
181	23	2519	1.93	23.10	5.73	36.00	0	0	82	74	0.694	0.0	******	******	****	****
181	24	2520	1.93	23.10	5.73	36.00	0	0	85	72	0.672	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
182	1	2521	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	2	2522	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	3	2523	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	4	2524	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	5	2525	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	6	2526	1.93	23.10	5.73	36.00	0	0	***	***	0.0	0.0	******	******	****	****
182	7	2527	1.93	23.10	5.99	8.86	0	0	***	***	0.0	3.90	******	******	0.88	****
182	8	2528	1.93	23.10	18.32	3.15	0	0	90	72	0.712	20.28	******	******	0.83	****
182	9	2529	1.93	23.10	31.06	1.93	0	0	71	77	0.664	39.00	******	******	0.80	****
182	10	2530	1.93	23.10	44.04	1.44	0	0	62	80	0.640	56.94	******	******	0.78	****
182	11	2531	1.93	23.10	57.15	1.19	0	0	60	83	0.683	72.54	******	******	0.78	****
182	12	2532	1.93	23.10	70.17	1.06	0	0	55	85	0.668	81.12	******	******	0.76	****
182	13	2533	1.93	23.10	81.94	1.01	0	0	53	88	0.708	******	******	******	****	****
182	14	2534	1.93	23.10	80.09	1.01	1	0	51	90	0.725	******	******	******	****	****
182	15	2535	1.93	23.10	67.80	1.08	1	0	50	91	0.733	81.12	******	******	****	****
182	16	2536	1.93	23.10	54.74	1.22	3	1	49	92	0.742	70.98	******	******	****	****
182	17	2537	1.93	23.10	41.65	1.50	3	1	49	92	0.742	56.16	******	******	****	****
182	18	2538	1.93	23.10	28.70	2.07	2	0	49	92	0.742	38.22	******	******	****	****
182	19	2539	1.93	23.10	16.02	3.58	0	0	55	90	0.782	18.72	******	******	0.86	****
182	20	2540	1.93	23.10	5.73	12.86	0	0	73	86	0.915	3.12	******	******	0.90	****
182	21	2541	1.93	23.10	5.73	36.00	0	0	80	82	0.882	0.0	******	******	****	****
182	22	2542	1.93	23.10	5.73	36.00	0	0	90	80	0.929	0.0	******	******	****	****
182	23	2543	1.93	23.10	5.73	36.00	0	0	93	89	1.282	0.0	******	******	****	****
182	24	2544	1.93	23.10	5.73	36.00	0	0	95	88	1.268	0.0	******	******	****	****
183	1	2545	1.93	23.00	5.73	36.00	0	0	96	77	0.898	0.0	******	******	****	****
183	2	2546	1.93	23.00	5.73	36.00	0	0	97	76	0.878	0.0	******	******	****	****
183	3	2547	1.93	23.00	5.73	36.00	0	0	98	76	0.887	0.0	******	******	****	****
183	4	2548	1.93	23.00	5.73	36.00	0	0	98	76	0.887	0.0	******	******	****	****
183	5	2549	1.93	23.00	5.73	36.00	3	1	98	76	0.887	0.0	******	******	****	****
183	6	2550	1.93	23.00	5.73	36.00	8	3	98	75	0.857	0.0	******	******	****	****
183	7	2551	1.93	23.00	5.99	8.87	8	3	98	76	0.887	3.12	******	******	****	****
183	8	2552	1.93	23.00	18.32	3.15	8	3	97	78	0.938	14.82	******	******	****	****
183	9	2553	1.93	23.00	31.06	1.93	8	2	85	82	0.937	34.32	******	******	****	****
183	10	2554	1.93	23.00	44.05	1.44	5	2	70	86	0.877	49.92	******	******	****	****
183	11	2555	1.93	23.00	57.16	1.19	4	1	62	88	0.828	68.64	******	******	****	****
183	12	2556	1.93	23.00	70.17	1.06	6	2	55	91	0.807	81.12	******	******	****	****
183	13	2557	1.93	23.00	81.90	1.01	7	2	53	93	0.827	******	******	******	****	****
183	14	2558	1.93	23.00	79.99	1.01	8	4	52	94	0.837	******	******	******	****	****
183	15	2559	1.93	23.00	67.72	1.08	10	6	60	92	0.908	51.48	******	******	****	****
183	16	2560	1.93	23.00	54.66	1.22	8	5	64	86	0.802	26.52	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
183	17	2561	1.93	23.00	41.57	1.50	10	8	70	84	0.822	14.04	******	******	****	****
183	18	2562	1.93	23.00	28.61	2.08	10	8	74	83	0.842	13.26	******	******	****	****
183	19	2563	1.93	23.00	15.94	3.60	8	6	76	84	0.893	16.38	******	******	****	****
183	20	2564	1.93	23.00	5.73	13.10	0	0	86	82	0.948	3.12	******	******	0.90	****
183	21	2565	1.93	23.00	5.73	36.00	0	0	90	80	0.929	0.0	******	******	****	****
183	22	2566	1.93	23.00	5.73	36.00	0	0	89	78	0.861	0.0	******	******	****	****
183	23	2567	1.93	23.00	5.73	36.00	0	0	90	78	0.870	0.0	******	******	****	****
183	24	2568	1.93	23.00	5.73	36.00	5	2	92	77	0.860	0.0	******	******	****	****
184	1	2569	1.93	23.00	5.73	36.00	8	3	95	77	0.888	0.0	******	******	****	****
184	2	2570	1.93	23.00	5.73	36.00	8	3	95	76	0.860	0.0	******	******	****	****
184	3	2571	1.93	23.00	5.73	36.00	9	4	97	75	0.849	0.0	******	******	****	****
184	4	2572	1.93	23.00	5.73	36.00	7	3	98	75	0.857	0.0	******	******	****	****
184	5	2573	1.93	23.00	5.73	36.00	9	4	98	75	0.857	0.0	******	******	****	****
184	6	2574	1.93	23.00	5.73	36.00	9	4	98	74	0.829	0.0	******	******	****	****
184	7	2575	1.93	23.00	6.03	8.81	9	4	98	74	0.829	3.12	******	******	****	****
184	8	2576	1.93	23.00	18.37	3.14	9	4	98	76	0.887	14.82	******	******	****	****
184	9	2577	1.93	23.00	31.11	1.93	7	3	90	78	0.870	30.42	******	******	****	****
184	10	2578	1.93	23.00	44.10	1.43	7	4	78	84	0.916	47.58	******	******	****	****
184	11	2579	1.93	23.00	57.21	1.19	7	4	66	87	0.853	60.84	******	******	****	****
184	12	2580	1.93	23.00	70.22	1.06	7	4	63	89	0.868	65.52	******	******	****	****
184	13	2581	1.93	23.00	81.93	1.01	8	6	80	89	1.102	35.88	******	******	****	****
184	14	2582	1.93	23.00	79.96	1.01	10	8	70	86	0.877	******	******	******	****	****
184	15	2583	1.93	23.00	67.68	1.08	9	5	68	90	0.967	******	******	******	****	****
184	16	2584	1.93	23.00	54.62	1.23	10	8	70	80	0.722	25.74	******	******	****	****
184	17	2585	1.93	23.00	41.52	1.51	10	9	90	76	0.814	13.26	******	******	****	****
184	18	2586	1.93	23.00	28.57	2.08	10	9	91	76	0.824	0.78	******	******	****	****
184	19	2587	1.93	23.00	15.90	3.60	10	9	88	76	0.796	2.34	******	******	****	****
184	20	2588	1.93	23.00	5.73	13.21	10	10	90	75	0.787	1.56	******	******	****	****
184	21	2589	1.93	23.00	5.73	36.00	10	10	92	74	0.778	0.0	******	******	****	****
184	22	2590	1.93	23.00	5.73	36.00	10	10	94	74	0.795	0.0	******	******	****	****
184	23	2591	1.93	23.00	5.73	36.00	9	9	96	74	0.812	0.0	******	******	****	****
184	24	2592	1.93	23.00	5.73	36.00	9	9	98	73	0.802	0.0	******	******	****	****
185	1	2593	1.93	22.90	5.73	36.00	7	4	99	72	0.783	0.0	******	******	****	****
185	2	2594	1.93	22.90	5.73	36.00	7	4	99	72	0.783	0.0	******	******	****	****
185	3	2595	1.93	22.90	5.73	36.00	7	4	99	72	0.783	0.0	******	******	****	****
185	4	2596	1.93	22.90	5.73	36.00	4	4	99	72	0.783	0.0	******	******	****	****
185	5	2597	1.93	22.90	5.73	36.00	7	6	98	71	0.749	0.0	******	******	****	****
185	6	2598	1.93	22.90	5.73	36.00	6	4	95	71	0.726	0.0	******	******	****	****
185	7	2599	1.93	22.90	6.02	8.83	3	1	97	70	0.717	3.90	******	******	****	****
185	8	2600	1.93	22.90	18.37	3.14	0	0	93	72	0.736	15.60	******	******	0.76	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL	OP	RHM	TEM	VPRES	SWRADT	TLRADT	LWRADT	TRAN	EMSV
							*	*	*	*		*	*			
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
185	9	2601	1.93	22.90	31.11	1.93	0	0	91	77	0.851	32.76	******	******	0.73	****
185	10	2602	1.93	22.90	44.11	1.43	3	3	85	80	0.877	******	******	******	****	****
185	11	2603	1.93	22.90	57.22	1.19	1	1	70	84	0.822	65.52	******	******	****	****
185	12	2604	1.93	22.90	70.22	1.06	3	3	66	86	0.827	******	******	******	****	****
185	13	2605	1.93	22.90	81.88	1.01	3	3	62	89	0.854	******	******	******	****	****
185	14	2606	1.93	22.90	79.86	1.02	5	5	60	89	0.827	******	******	******	****	****
185	15	2607	1.93	22.90	67.60	1.08	4	3	59	90	0.839	******	******	******	****	****
185	16	2608	1.93	22.90	54.55	1.23	8	7	59	90	0.839	55.38	******	******	****	****
185	17	2609	1.93	22.90	41.45	1.51	8	7	62	88	0.828	34.32	******	******	****	****
185	18	2610	1.93	22.90	28.49	2.09	8	7	63	87	0.815	18.72	******	******	****	****
185	19	2611	1.93	22.90	15.81	3.62	9	7	65	86	0.814	14.82	******	******	****	****
185	20	2612	1.93	22.90	5.73	13.45	9	5	70	85	0.850	3.12	******	******	****	****
185	21	2613	1.93	22.90	5.73	36.00	8	4	80	80	0.826	0.0	******	******	****	****
185	22	2614	1.93	22.90	5.73	36.00	7	3	86	79	0.859	0.0	******	******	****	****
185	23	2615	1.93	22.90	5.73	36.00	7	3	91	78	0.880	0.0	******	******	****	****
185	24	2616	1.93	22.90	5.73	36.00	7	3	93	77	0.870	0.0	******	******	****	****
186	1	2617	1.93	22.90	5.73	36.00	7	3	93	76	0.842	0.0	******	******	****	****
186	2	2618	1.93	22.90	5.73	36.00	7	3	93	76	0.842	0.0	******	******	****	****
186	3	2619	1.93	22.90	5.73	36.00	7	3	93	75	0.814	0.0	******	******	****	****
186	4	2620	1.93	22.90	5.73	36.00	8	5	93	74	0.787	0.0	******	******	****	****
186	5	2621	1.93	22.90	5.73	36.00	7	4	95	74	0.804	0.0	******	******	****	****
186	6	2622	1.93	22.90	5.73	36.00	10	8	96	73	0.785	0.0	******	******	****	****
186	7	2623	1.93	22.90	6.04	8.80	10	10	97	73	0.793	0.78	******	******	****	****
186	8	2624	1.93	22.90	18.39	3.14	10	9	97	74	0.821	7.02	******	******	****	****
186	9	2625	1.93	22.90	31.14	1.93	10	10	93	78	0.899	17.16	******	******	****	****
186	10	2626	1.93	22.90	44.13	1.43	10	10	92	79	0.919	******	******	******	****	****
186	11	2627	1.93	22.90	57.24	1.19	10	10	85	80	0.877	******	******	******	****	****
186	12	2628	1.93	22.90	70.24	1.06	9	9	75	83	0.853	37.44	******	******	****	****
186	13	2629	1.93	22.90	81.90	1.01	10	10	95	80	0.980	******	******	******	****	****
186	14	2630	1.93	22.90	79.84	1.02	10	10	100	71	0.764	14.82	******	******	****	****
186	15	2631	1.93	22.90	67.58	1.08	10	9	100	72	0.791	12.48	******	******	****	****
186	16	2632	1.93	22.90	54.52	1.23	10	7	100	72	0.791	18.72	******	******	****	****
186	17	2633	1.93	22.90	41.43	1.51	10	8	93	78	0.899	42.90	******	******	****	****
186	18	2634	1.93	22.90	28.47	2.09	10	7	92	79	0.919	28.86	******	******	****	****
186	19	2635	1.93	22.90	15.79	3.63	10	6	72	82	0.793	24.96	******	******	****	****
186	20	2636	1.93	22.90	5.73	13.51	7	3	76	80	0.784	3.12	******	******	****	****
186	21	2637	1.93	22.90	5.73	36.00	4	2	86	77	0.804	0.0	******	******	****	****
186	22	2638	1.93	22.90	5.73	36.00	2	1	91	76	0.824	0.0	******	******	****	****
186	23	2639	1.93	22.90	5.73	36.00	2	1	96	75	0.840	0.0	******	******	****	****
186	24	2640	1.93	22.90	5.73	36.00	3	1	97	75	0.849	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
187	1	2641	1.93	22.80	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
187	2	2642	1.93	22.80	5.73	36.00	0	0	99	73	0.810	0.0	******	******	****	****
187	3	2643	1.93	22.80	5.73	36.00	0	0	99	72	0.783	0.0	******	******	****	****
187	4	2644	1.93	22.80	5.73	36.00	0	0	99	72	0.783	0.0	******	******	****	****
187	5	2645	1.93	22.80	5.73	36.00	3	1	100	72	0.791	0.0	******	******	****	****
187	6	2646	1.93	22.80	5.73	36.00	3	1	100	72	0.791	0.0	******	******	****	****
187	7	2647	1.93	22.80	6.03	8.81	5	3	100	72	0.791	3.12	******	******	****	****
187	8	2648	1.93	22.80	18.39	3.14	7	5	100	74	0.846	20.28	******	******	****	****
187	9	2649	1.93	22.80	31.14	1.93	7	5	***	***	0.0	29.64	******	******	****	****
187	10	2650	1.93	22.80	44.14	1.43	8	6	***	***	0.0	50.70	******	******	****	****
187	11	2651	1.93	22.80	57.25	1.19	8	7	***	***	0.0	69.42	******	******	****	****
187	12	2652	1.93	22.80	70.25	1.06	8	4	68	83	0.774	******	******	******	****	****
187	13	2653	1.93	22.80	81.85	1.01	8	6	63	85	0.765	******	******	******	****	****
187	14	2654	1.93	22.80	79.74	1.02	8	5	61	88	0.814	******	******	******	****	****
187	15	2655	1.93	22.80	67.50	1.08	9	4	59	87	0.763	63.18	******	******	****	****
187	16	2656	1.93	22.80	54.45	1.23	8	3	52	89	0.717	67.08	******	******	****	****
187	17	2657	1.93	22.80	41.35	1.51	8	3	50	89	0.689	55.38	******	******	****	****
187	18	2658	1.93	22.80	28.39	2.09	9	4	50	89	0.689	28.86	******	******	****	****
187	19	2659	1.93	22.80	15.71	3.65	9	6	56	86	0.702	6.24	******	******	****	****
187	20	2660	1.93	22.80	5.73	13.77	10	8	60	85	0.728	0.0	******	******	****	****
187	21	2661	1.93	22.80	5.73	36.00	7	4	80	80	0.826	0.0	******	******	****	****
187	22	2662	1.93	22.80	5.73	36.00	6	2	82	78	0.793	0.0	******	******	****	****
187	23	2663	1.93	22.80	5.73	36.00	3	2	87	77	0.813	0.0	******	******	****	****
187	24	2664	1.93	22.80	5.73	36.00	4	3	92	76	0.833	0.0	******	******	****	****
188	1	2665	1.93	22.70	5.73	36.00	0	0	92	76	0.833	0.0	******	******	****	****
188	2	2666	1.93	22.70	5.73	36.00	0	0	95	76	0.860	0.0	******	******	****	****
188	3	2667	1.93	22.70	5.73	36.00	0	0	97	75	0.849	0.0	******	******	****	****
188	4	2668	1.93	22.70	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
188	5	2669	1.93	22.70	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
188	6	2670	1.93	22.70	5.73	36.00	5	2	98	73	0.802	0.0	******	******	****	****
188	7	2671	1.93	22.70	6.02	8.82	5	2	98	72	0.775	3.12	******	******	****	****
188	8	2672	1.93	22.70	18.39	3.14	4	1	99	73	0.810	20.28	******	******	****	****
188	9	2673	1.93	22.70	31.15	1.93	5	2	93	77	0.870	38.22	******	******	****	****
188	10	2674	1.93	22.70	44.15	1.43	5	4	80	80	0.826	49.92	******	******	****	****
188	11	2675	1.93	22.70	57.26	1.19	6	4	65	84	0.764	70.98	******	******	****	****
188	12	2676	1.93	22.70	70.25	1.06	7	3	60	87	0.776	******	******	******	****	****
188	13	2677	1.93	22.70	81.80	1.01	7	5	53	88	0.708	******	******	******	****	****
188	14	2678	1.93	22.70	79.64	1.02	8	6	50	92	0.757	******	******	******	****	****
188	15	2679	1.93	22.70	67.42	1.08	8	3	48	92	0.727	******	******	******	****	****
188	16	2680	1.93	22.70	54.37	1.23	9	3	48	92	0.727	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
188	17	2681	1.93	22.70	41.27	1.51	8	4	44	94	0.708	******	******	******	****	****
188	18	2682	1.93	22.70	28.31	2.10	7	3	45	93	0.702	******	******	******	****	****
188	19	2683	1.93	22.70	15.62	3.66	8	5	47	91	0.689	******	******	******	****	****
188	20	2684	1.93	22.70	5.73	14.03	9	6	60	86	0.752	******	******	******	****	****
188	21	2685	1.93	22.70	5.73	36.00	9	7	72	84	0.846	0.0	******	******	****	****
188	22	2686	1.93	22.70	5.73	36.00	8	5	61	82	0.672	0.0	******	******	****	****
188	23	2687	1.93	22.70	5.73	36.00	5	4	80	77	0.748	0.0	******	******	****	****
188	24	2688	1.93	22.70	5.73	36.00	0	0	80	77	0.748	0.0	******	******	****	****
189	1	2689	1.93	22.60	5.73	36.00	0	0	83	76	0.751	0.0	******	******	****	****
189	2	2690	1.93	22.60	5.73	36.00	0	0	83	75	0.726	0.0	******	******	****	****
189	3	2691	1.93	22.60	5.73	36.00	0	0	89	74	0.753	0.0	******	******	****	****
189	4	2692	1.93	22.60	5.73	36.00	0	0	90	73	0.736	0.0	******	******	****	****
189	5	2693	1.93	22.60	5.73	36.00	0	0	93	72	0.736	0.0	******	******	****	****
189	6	2694	1.93	22.60	5.73	36.00	4	1	98	72	0.775	0.0	******	******	****	****
189	7	2695	1.93	22.60	6.01	8.83	4	1	97	72	0.767	******	******	******	****	****
189	8	2696	1.93	22.60	18.39	3.14	4	1	97	73	0.793	******	******	******	****	****
189	9	2697	1.93	22.60	31.16	1.93	4	2	95	77	0.888	******	******	******	****	****
189	10	2698	1.93	22.60	44.16	1.43	5	3	85	81	0.906	******	******	******	****	****
189	11	2699	1.93	22.60	57.27	1.19	5	4	72	85	0.874	******	******	******	****	****
189	12	2700	1.93	22.60	70.25	1.06	5	5	68	88	0.908	******	******	******	****	****
189	13	2701	1.93	22.60	81.75	1.01	7	6	63	90	0.896	******	******	******	****	****
189	14	2702	1.93	22.60	79.54	1.02	8	7	70	90	0.995	******	******	******	****	****
189	15	2703	1.93	22.60	67.34	1.08	10	8	60	91	0.880	******	******	******	****	****
189	16	2704	1.93	22.60	54.30	1.23	10	8	60	82	0.661	******	******	******	****	****
189	17	2705	1.93	22.60	41.20	1.52	10	7	99	72	0.783	******	******	******	****	****
189	18	2706	1.93	22.60	28.23	2.11	10	6	99	72	0.783	******	******	******	****	****
189	19	2707	1.93	22.60	15.54	3.68	10	6	95	78	0.919	******	******	******	****	****
189	20	2708	1.93	22.60	5.73	14.31	7	3	88	79	0.879	******	******	******	****	****
189	21	2709	1.93	22.60	5.73	36.00	6	2	95	76	0.860	0.0	******	******	****	****
189	22	2710	1.93	22.60	5.73	36.00	4	1	98	76	0.887	0.0	******	******	****	****
189	23	2711	1.93	22.60	5.73	36.00	0	0	98	75	0.857	0.0	******	******	****	****
189	24	2712	1.93	22.60	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
190	1	2713	1.93	22.50	5.73	36.00	**	**	99	74	0.838	0.0	******	******	****	****
190	2	2714	1.93	22.50	5.73	36.00	**	**	99	73	0.810	0.0	******	******	****	****
190	3	2715	1.93	22.50	5.73	36.00	**	**	99	73	0.810	0.0	******	******	****	****
190	4	2716	1.93	22.50	5.73	36.00	**	**	99	73	0.810	0.0	******	******	****	****
190	5	2717	1.93	22.50	5.73	36.00	**	**	99	73	0.810	0.0	******	******	****	****
190	6	2718	1.93	22.50	5.73	36.00	**	**	99	73	0.810	0.0	******	******	****	****
190	7	2719	1.93	22.50	5.99	8.87	**	**	99	73	0.810	******	******	******	****	****
190	8	2720	1.93	22.50	18.37	3.14	**	**	98	74	0.829	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
190	9	2721	1.93	22.50	31.14	1.93	**	**	94	76	0.851	******	******	******	****	****
190	10	2722	1.93	22.50	44.15	1.43	**	**	86	80	0.888	******	******	******	****	****
190	11	2723	1.93	22.50	57.26	1.19	**	**	80	84	0.940	******	******	******	****	****
190	12	2724	1.93	22.50	70.23	1.06	**	**	80	84	0.940	******	******	******	****	****
190	13	2725	1.93	22.50	81.69	1.01	**	**	70	87	0.905	******	******	******	****	****
190	14	2726	1.93	22.50	79.46	1.02	**	**	70	88	0.934	******	******	******	****	****
190	15	2727	1.93	22.50	67.28	1.08	**	**	68	88	0.908	******	******	******	****	****
190	16	2728	1.93	22.50	54.24	1.23	**	**	63	90	0.896	******	******	******	****	****
190	17	2729	1.93	22.50	41.14	1.52	**	**	65	88	0.868	******	******	******	****	****
190	18	2730	1.93	22.50	28.17	2.11	**	**	69	86	0.865	******	******	******	****	****
190	19	2731	1.93	22.50	15.47	3.70	**	**	97	74	0.821	******	******	******	****	****
190	20	2732	1.93	22.50	5.73	14.53	**	**	100	73	0.818	******	******	******	****	****
190	21	2733	1.93	22.50	5.73	36.00	**	**	100	73	0.818	0.0	******	******	****	****
190	22	2734	1.93	22.50	5.73	36.00	**	**	100	73	0.818	0.0	******	******	****	****
190	23	2735	1.93	22.50	5.73	36.00	**	**	100	74	0.846	0.0	******	******	****	****
190	24	2736	1.93	22.50	5.73	36.00	**	**	100	74	0.846	0.0	******	******	****	****
191	1	2737	1.93	22.40	5.73	36.00	9	7	98	73	0.802	0.0	******	******	****	****
191	2	2738	1.93	22.40	5.73	36.00	9	7	98	72	0.775	0.0	******	******	****	****
191	3	2739	1.93	22.40	5.73	36.00	9	8	99	72	0.783	0.0	******	******	****	****
191	4	2740	1.93	22.40	5.73	36.00	9	8	100	72	0.791	0.0	******	******	****	****
191	5	2741	1.93	22.40	5.73	36.00	10	10	100	73	0.818	0.0	******	******	****	****
191	6	2742	1.93	22.40	5.73	36.00	10	10	100	73	0.818	0.0	******	******	****	****
191	7	2743	1.93	22.40	5.96	8.90	7	6	100	73	0.818	******	******	******	****	****
191	8	2744	1.93	22.40	18.35	3.15	7	6	100	73	0.818	******	******	******	****	****
191	9	2745	1.93	22.40	31.13	1.93	6	5	96	75	0.840	******	******	******	****	****
191	10	2746	1.93	22.40	44.14	1.43	7	6	83	78	0.803	******	******	******	****	****
191	11	2747	1.93	22.40	57.25	1.19	5	4	78	82	0.860	******	******	******	****	****
191	12	2748	1.93	22.40	70.22	1.06	6	5	72	84	0.846	******	******	******	****	****
191	13	2749	1.93	22.40	81.62	1.01	8	6	67	87	0.866	******	******	******	****	****
191	14	2750	1.93	22.40	79.38	1.02	9	8	63	89	0.868	******	******	******	****	****
191	15	2751	1.93	22.40	67.22	1.08	10	10	95	78	0.919	******	******	******	****	****
191	16	2752	1.93	22.40	54.19	1.23	10	9	95	80	0.980	******	******	******	****	****
191	17	2753	1.93	22.40	41.08	1.52	10	8	99	68	0.683	******	******	******	****	****
191	18	2754	1.93	22.40	28.11	2.11	10	8	99	70	0.732	******	******	******	****	****
191	19	2755	1.93	22.40	15.41	3.71	10	9	99	71	0.756	******	******	******	****	****
191	20	2756	1.93	22.40	5.73	14.76	9	4	98	72	0.775	******	******	******	****	****
191	21	2757	1.93	22.40	5.73	36.00	8	6	99	71	0.756	0.0	******	******	****	****
191	22	2758	1.93	22.40	5.73	36.00	8	3	99	70	0.732	0.0	******	******	****	****
191	23	2759	1.93	22.40	5.73	36.00	8	3	100	70	0.739	0.0	******	******	****	****
191	24	2760	1.93	22.40	5.73	36.00	8	3	100	70	0.739	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
192	1	2761	1.93	22.20	5.73	36.00	7	3	98	70	0.724	0.0	******	******	****	****
192	2	2762	1.93	22.20	5.73	36.00	7	3	98	70	0.724	0.0	******	******	****	****
192	3	2763	1.93	22.20	5.73	36.00	7	3	99	70	0.732	0.0	******	******	****	****
192	4	2764	1.93	22.20	5.73	36.00	7	3	99	69	0.707	0.0	******	******	****	****
192	5	2765	1.93	22.20	5.73	36.00	7	3	100	69	0.714	0.0	******	******	****	****
192	6	2766	1.93	22.20	5.73	36.00	3	2	100	68	0.690	0.0	******	******	****	****
192	7	2767	1.93	22.20	5.92	8.95	7	3	100	69	0.714	******	******	******	****	****
192	8	2768	1.93	22.20	18.33	3.15	5	3	100	70	0.739	******	******	******	****	****
192	9	2769	1.93	22.20	31.12	1.93	7	4	97	73	0.793	******	******	******	****	****
192	10	2770	1.93	22.20	44.14	1.43	8	5	95	76	0.860	******	******	******	****	****
192	11	2771	1.93	22.20	57.25	1.19	8	7	90	80	0.929	******	******	******	****	****
192	12	2772	1.93	22.20	70.20	1.06	8	7	80	83	0.910	******	******	******	****	****
192	13	2773	1.93	22.20	81.50	1.01	9	7	70	86	0.877	******	******	******	****	****
192	14	2774	1.93	22.20	79.20	1.02	9	7	60	90	0.853	******	******	******	****	****
192	15	2775	1.93	22.20	67.09	1.08	7	3	68	86	0.852	******	******	******	****	****
192	16	2776	1.93	22.20	54.06	1.23	7	3	64	86	0.802	******	******	******	****	****
192	17	2777	1.93	22.20	40.95	1.52	7	3	62	90	0.882	******	******	******	****	****
192	18	2778	1.93	22.20	27.98	2.12	6	2	62	90	0.882	******	******	******	****	****
192	19	2779	1.93	22.20	15.26	3.75	6	4	59	90	0.839	******	******	******	****	****
192	20	2780	1.93	22.20	5.73	15.30	5	2	59	90	0.839	******	******	******	****	****
192	21	2781	1.93	22.20	5.73	36.00	3	2	75	78	0.725	0.0	******	******	****	****
192	22	2782	1.93	22.20	5.73	36.00	0	0	85	75	0.744	0.0	******	******	****	****
192	23	2783	1.93	22.20	5.73	36.00	0	0	89	74	0.753	0.0	******	******	****	****
192	24	2784	1.93	22.20	5.73	36.00	0	0	92	74	0.778	0.0	******	******	****	****
193	1	2785	1.94	22.10	5.73	36.00	5	5	95	73	0.777	0.0	******	******	****	****
193	2	2786	1.94	22.10	5.73	36.00	5	5	94	73	0.769	0.0	******	******	****	****
193	3	2787	1.94	22.10	5.73	36.00	3	2	95	73	0.777	0.0	******	******	****	****
193	4	2788	1.94	22.10	5.73	36.00	3	2	94	72	0.744	0.0	******	******	****	****
193	5	2789	1.94	22.10	5.73	36.00	2	1	97	72	0.767	0.0	******	******	****	****
193	6	2790	1.94	22.10	5.73	36.00	6	4	98	72	0.775	0.0	******	******	****	****
193	7	2791	1.94	22.10	5.89	8.99	9	7	98	71	0.749	******	******	******	****	****
193	8	2792	1.94	22.10	18.31	3.15	10	8	98	72	0.775	******	******	******	****	****
193	9	2793	1.94	22.10	31.10	1.93	10	7	97	76	0.878	******	******	******	****	****
193	10	2794	1.94	22.10	44.13	1.43	10	9	93	79	0.929	******	******	******	****	****
193	11	2795	1.94	22.10	57.24	1.19	9	7	80	83	0.910	******	******	******	****	****
193	12	2796	1.94	22.10	70.18	1.06	9	7	79	83	0.899	******	******	******	****	****
193	13	2797	1.94	22.10	81.43	1.01	10	10	75	84	0.881	******	******	******	****	****
193	14	2798	1.94	22.10	79.11	1.02	10	10	78	84	0.916	******	******	******	****	****
193	15	2799	1.94	22.10	67.03	1.09	10	10	85	76	0.769	******	******	******	****	****
193	16	2800	1.94	22.10	54.00	1.23	10	10	92	72	0.728	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
193	17	2801	1.94	22.10	40.90	1.52	10	10	99	72	0.783	******	******	******	****	****
193	18	2802	1.94	22.10	27.92	2.13	10	10	99	72	0.783	******	******	******	****	****
193	19	2803	1.94	22.10	15.20	3.76	9	8	98	73	0.802	******	******	******	****	****
193	20	2804	1.94	22.10	5.73	15.55	7	6	98	72	0.775	******	******	******	****	****
193	21	2805	1.94	22.10	5.73	36.00	8	4	98	72	0.775	0.0	******	******	****	****
193	22	2806	1.94	22.10	5.73	36.00	0	0	99	72	0.783	0.0	******	******	****	****
193	23	2807	1.94	22.10	5.73	36.00	10	9	98	72	0.775	0.0	******	******	****	****
193	24	2808	1.94	22.10	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
194	1	2809	1.94	22.00	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
194	2	2810	1.94	22.00	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
194	3	2811	1.94	22.00	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
194	4	2812	1.94	22.00	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
194	5	2813	1.94	22.00	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
194	6	2814	1.94	22.00	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
194	7	2815	1.94	22.00	5.87	9.02	10	10	99	71	0.756	******	******	******	****	****
194	8	2816	1.94	22.00	18.29	3.16	10	9	99	72	0.783	******	******	******	****	****
194	9	2817	1.94	22.00	31.09	1.93	8	3	94	74	0.795	******	******	******	****	****
194	10	2818	1.94	22.00	44.12	1.43	9	4	83	78	0.803	******	******	******	****	****
194	11	2819	1.94	22.00	57.23	1.19	9	5	73	83	0.831	******	******	******	****	****
194	12	2820	1.94	22.00	70.16	1.06	10	8	68	85	0.826	******	******	******	****	****
194	13	2821	1.94	22.00	81.36	1.01	10	8	62	86	0.777	******	******	******	****	****
194	14	2822	1.94	22.00	79.03	1.02	10	8	60	87	0.776	******	******	******	****	****
194	15	2823	1.94	22.00	66.97	1.09	10	7	60	87	0.776	******	******	******	****	****
194	16	2824	1.94	22.00	53.95	1.24	10	9	60	88	0.801	******	******	******	****	****
194	17	2825	1.94	22.00	40.84	1.53	10	9	63	87	0.815	******	******	******	****	****
194	18	2826	1.94	22.00	27.86	2.13	10	9	66	84	0.775	******	******	******	****	****
194	19	2827	1.94	22.00	15.13	3.78	10	8	70	83	0.797	******	******	******	****	****
194	20	2828	1.94	22.00	5.73	15.81	10	7	71	82	0.782	******	******	******	****	****
194	21	2829	1.94	22.00	5.73	36.00	4	2	77	81	0.821	0.0	******	******	****	****
194	22	2830	1.94	22.00	5.73	36.00	10	9	86	79	0.859	0.0	******	******	****	****
194	23	2831	1.94	22.00	5.73	36.00	9	6	85	75	0.744	0.0	******	******	****	****
194	24	2832	1.94	22.00	5.73	36.00	10	8	94	73	0.769	0.0	******	******	****	****
195	1	2833	1.94	21.80	5.73	36.00	10	9	96	73	0.785	0.0	******	******	****	****
195	2	2834	1.94	21.80	5.73	36.00	10	10	84	74	0.711	0.0	******	******	****	****
195	3	2835	1.94	21.80	5.73	36.00	10	10	92	73	0.753	0.0	******	******	****	****
195	4	2836	1.94	21.80	5.73	36.00	10	10	94	72	0.744	0.0	******	******	****	****
195	5	2837	1.94	21.80	5.73	36.00	10	10	94	72	0.744	0.0	******	******	****	****
195	6	2838	1.94	21.80	5.73	36.00	10	10	93	72	0.736	0.0	******	******	****	****
195	7	2839	1.94	21.80	5.79	9.12	10	7	93	72	0.736	******	******	******	****	****
195	8	2840	1.94	21.80	18.23	3.17	9	8	91	74	0.770	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
195	9	2841	1.94	21.80	31.04	1.93	10	9	82	75	0.717	******	******	******	****	****
195	10	2842	1.94	21.80	44.07	1.44	10	7	75	80	0.774	******	******	******	****	****
195	11	2843	1.94	21.80	57.18	1.19	9	8	70	83	0.797	******	******	******	****	****
195	12	2844	1.94	21.80	70.09	1.06	9	7	70	86	0.877	******	******	******	****	****
195	13	2845	1.94	21.80	81.21	1.01	9	8	69	88	0.921	******	******	******	****	****
195	14	2846	1.94	21.80	78.88	1.02	9	8	64	90	0.910	******	******	******	****	****
195	15	2847	1.94	21.80	66.87	1.09	9	8	59	92	0.893	******	******	******	****	****
195	16	2848	1.94	21.80	53.86	1.24	9	8	58	92	0.878	******	******	******	****	****
195	17	2849	1.94	21.80	40.75	1.53	9	8	59	91	0.866	******	******	******	****	****
195	18	2850	1.94	21.80	27.76	2.14	9	8	60	82	0.661	******	******	******	****	****
195	19	2851	1.94	21.80	15.03	3.80	9	8	70	81	0.746	******	******	******	****	****
195	20	2852	1.94	21.80	5.73	16.27	7	7	78	79	0.779	******	******	******	****	****
195	21	2853	1.94	21.80	5.73	36.00	5	5	91	76	0.824	0.0	******	******	****	****
195	22	2854	1.94	21.80	5.73	36.00	5	3	92	76	0.833	0.0	******	******	****	****
195	23	2855	1.94	21.80	5.73	36.00	5	3	93	75	0.814	0.0	******	******	****	****
195	24	2856	1.94	21.80	5.73	36.00	0	0	94	74	0.795	0.0	******	******	****	****
196	1	1	1.94	21.70	5.73	36.00	0	0	88	74	0.744	0.0	******	******	****	****
196	2	2	1.94	21.70	5.73	36.00	0	0	94	73	0.769	0.0	******	******	****	****
196	3	3	1.94	21.70	5.73	36.00	0	0	95	73	0.777	0.0	******	******	****	****
196	4	4	1.94	21.70	5.73	36.00	0	0	96	72	0.759	0.0	******	******	****	****
196	5	5	1.94	21.70	5.73	36.00	0	0	97	72	0.767	0.0	******	******	****	****
196	6	6	1.94	21.70	5.73	36.00	0	0	97	72	0.767	0.0	******	******	****	****
196	7	7	1.94	21.70	5.78	9.14	0	0	97	72	0.767	79.97	******	******	****	****
196	8	8	1.94	21.70	18.22	3.17	0	0	97	74	0.821	79.97	******	******	****	****
196	9	9	1.94	21.70	31.04	1.93	6	2	88	80	0.908	79.97	******	******	****	****
196	10	10	1.94	21.70	44.08	1.44	7	2	78	84	0.916	79.97	******	******	****	****
196	11	11	1.94	21.70	57.19	1.19	9	3	70	86	0.877	79.97	******	******	****	****
196	12	12	1.94	21.70	70.09	1.06	9	4	60	90	0.853	79.97	******	******	****	****
196	13	13	1.94	21.70	81.15	1.01	9	4	56	91	0.822	79.97	******	******	****	****
196	14	14	1.94	21.70	78.78	1.02	8	3	53	92	0.802	79.97	******	******	****	****
196	15	15	1.94	21.70	66.79	1.09	8	5	50	94	0.805	79.97	******	******	****	****
196	16	16	1.94	21.70	53.78	1.24	8	5	48	94	0.773	79.97	******	******	****	****
196	17	17	1.94	21.70	40.68	1.53	9	7	55	85	0.668	79.97	******	******	****	****
196	18	18	1.94	21.70	27.68	2.14	10	8	57	84	0.670	79.97	******	******	****	****
196	19	19	1.94	21.70	14.94	3.82	10	7	60	85	0.728	79.97	******	******	****	****
196	20	20	1.94	21.70	5.73	16.62	5	4	62	83	0.706	79.97	******	******	****	****
196	21	21	1.94	21.70	5.73	36.00	3	2	77	80	0.795	0.0	******	******	****	****
196	22	22	1.94	21.70	5.73	36.00	2	1	82	78	0.793	0.0	******	******	****	****
196	23	23	1.94	21.70	5.73	36.00	2	1	87	77	0.813	0.0	******	******	****	****
196	24	24	1.94	21.70	5.73	36.00	2	1	93	76	0.842	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
197	1	25	1.94	21.50	5.73	36.00	5	4	93	76	0.842	0.0	******	******	****	****
197	2	26	1.94	21.50	5.73	36.00	5	4	96	74	0.812	0.0	******	******	****	****
197	3	27	1.94	21.50	5.73	36.00	8	4	97	74	0.821	0.0	******	******	****	****
197	4	28	1.94	21.50	5.73	36.00	8	7	97	74	0.821	0.0	******	******	****	****
197	5	29	1.94	21.50	5.73	36.00	7	6	98	74	0.829	0.0	******	******	****	****
197	6	30	1.94	21.50	5.73	36.00	6	3	98	74	0.829	0.0	******	******	****	****
197	7	31	1.94	21.50	5.73	9.24	6	3	98	74	0.829	79.97	******	******	****	****
197	8	32	1.94	21.50	18.16	3.18	7	2	98	76	0.887	79.97	******	******	****	****
197	9	33	1.94	21.50	30.99	1.94	7	2	80	80	0.826	79.97	******	******	****	****
197	10	34	1.94	21.50	44.03	1.44	6	2	71	83	0.808	79.97	******	******	****	****
197	11	35	1.94	21.50	57.14	1.19	7	3	65	86	0.814	79.97	******	******	****	****
197	12	36	1.94	21.50	70.02	1.06	8	3	56	88	0.748	79.97	******	******	****	****
197	13	37	1.94	21.50	81.00	1.01	10	4	50	90	0.711	79.97	******	******	****	****
197	14	38	1.94	21.50	78.63	1.02	10	4	51	90	0.725	79.97	******	******	****	****
197	15	39	1.94	21.50	66.69	1.09	9	4	50	91	0.733	79.97	******	******	****	****
197	16	40	1.94	21.50	53.69	1.24	8	3	49	92	0.742	79.97	******	******	****	****
197	17	41	1.94	21.50	40.58	1.53	7	3	52	92	0.787	79.97	******	******	****	****
197	18	42	1.94	21.50	27.58	2.15	7	2	54	90	0.768	79.97	******	******	****	****
197	19	43	1.94	21.50	14.84	3.85	7	2	60	85	0.728	79.97	******	******	****	****
197	20	44	1.94	21.50	5.73	17.12	3	2	70	84	0.822	79.97	******	******	****	****
197	21	45	1.94	21.50	5.73	36.00	3	1	75	82	0.826	0.0	******	******	****	****
197	22	46	1.94	21.50	5.73	36.00	3	1	82	80	0.846	0.0	******	******	****	****
197	23	47	1.94	21.50	5.73	36.00	3	1	88	79	0.879	0.0	******	******	****	****
197	24	48	1.94	21.50	5.73	36.00	6	2	92	79	0.919	0.0	******	******	****	****
198	1	49	1.94	21.40	5.73	36.00	3	2	93	78	0.899	0.0	******	******	****	****
198	2	50	1.94	21.40	5.73	36.00	0	0	93	77	0.870	0.0	******	******	****	****
198	3	51	1.94	21.40	5.73	36.00	0	0	95	76	0.860	0.0	******	******	****	****
198	4	52	1.94	21.40	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
198	5	53	1.94	21.40	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
198	6	54	1.94	21.40	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
198	7	55	1.94	21.40	5.73	9.28	1	0	98	74	0.829	79.97	******	******	****	****
198	8	56	1.94	21.40	18.14	3.18	3	1	92	75	0.805	79.97	******	******	****	****
198	9	57	1.94	21.40	30.97	1.94	6	2	85	78	0.822	79.97	******	******	****	****
198	10	58	1.94	21.40	44.02	1.44	3	1	78	80	0.805	79.97	******	******	****	****
198	11	59	1.94	21.40	57.13	1.19	4	1	70	84	0.822	79.97	******	******	****	****
198	12	60	1.94	21.40	70.00	1.06	7	3	60	87	0.776	79.97	******	******	****	****
198	13	61	1.94	21.40	80.93	1.01	8	5	59	89	0.813	79.97	******	******	****	****
198	14	62	1.94	21.40	78.54	1.02	8	3	56	89	0.772	79.97	******	******	****	****
198	15	63	1.94	21.40	66.62	1.09	7	4	53	91	0.778	79.97	******	******	****	****
198	16	64	1.94	21.40	53.64	1.24	10	9	54	92	0.818	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
198	17	65	1.94	21.40	40.53	1.54	10	8	57	90	0.811	79.97	******	******	****	****
198	18	66	1.94	21.40	27.52	2.15	9	8	62	89	0.854	79.97	******	******	****	****
198	19	67	1.94	21.40	14.77	3.86	8	6	61	85	0.741	79.97	******	******	****	****
198	20	68	1.94	21.40	5.73	17.43	9	9	65	84	0.764	79.97	******	******	****	****
198	21	69	1.94	21.40	5.73	36.00	8	6	90	76	0.814	0.0	******	******	****	****
198	22	70	1.94	21.40	5.73	36.00	7	5	96	73	0.785	0.0	******	******	****	****
198	23	71	1.94	21.40	5.73	36.00	7	4	97	72	0.767	0.0	******	******	****	****
198	24	72	1.94	21.40	5.73	36.00	7	4	98	72	0.775	0.0	******	******	****	****
199	1	73	1.94	21.20	5.73	36.00	**	**	98	72	0.775	0.0	******	******	****	****
199	2	74	1.94	21.20	5.73	36.00	**	**	98	72	0.775	0.0	******	******	****	****
199	3	75	1.94	21.20	5.73	36.00	**	**	98	71	0.749	0.0	******	******	****	****
199	4	76	1.94	21.20	5.73	36.00	**	**	99	70	0.732	0.0	******	******	****	****
199	5	77	1.94	21.20	5.73	36.00	**	**	99	70	0.732	0.0	******	******	****	****
199	6	78	1.94	21.20	5.73	36.00	**	**	99	70	0.732	0.0	******	******	****	****
199	7	79	1.94	21.20	5.73	9.42	**	**	98	71	0.749	79.97	******	******	****	****
199	8	80	1.94	21.20	18.05	3.19	**	**	92	72	0.728	79.97	******	******	****	****
199	9	81	1.94	21.20	30.90	1.94	**	**	85	76	0.769	79.97	******	******	****	****
199	10	82	1.94	21.20	43.95	1.44	**	**	75	79	0.749	79.97	******	******	****	****
199	11	83	1.94	21.20	57.06	1.19	**	**	70	82	0.771	79.97	******	******	****	****
199	12	84	1.94	21.20	69.91	1.06	**	**	60	84	0.705	79.97	******	******	****	****
199	13	85	1.94	21.20	80.76	1.01	**	**	52	88	0.694	79.97	******	******	****	****
199	14	86	1.94	21.20	78.40	1.02	**	**	50	90	0.711	79.97	******	******	****	****
199	15	87	1.94	21.20	66.54	1.09	**	**	48	92	0.727	79.97	******	******	****	****
199	16	88	1.94	21.20	53.57	1.24	**	**	49	92	0.742	79.97	******	******	****	****
199	17	89	1.94	21.20	40.46	1.54	**	**	55	92	0.833	79.97	******	******	****	****
199	18	90	1.94	21.20	27.45	2.16	**	**	65	90	0.924	79.97	******	******	****	****
199	19	91	1.94	21.20	14.68	3.89	**	**	72	81	0.768	79.97	******	******	****	****
199	20	92	1.94	21.20	5.73	17.88	**	**	73	81	0.778	79.97	******	******	****	****
199	21	93	1.94	21.20	5.73	36.00	**	**	77	80	0.795	0.0	******	******	****	****
199	22	94	1.94	21.20	5.73	36.00	**	**	86	78	0.832	0.0	******	******	****	****
199	23	95	1.94	21.20	5.73	36.00	**	**	86	78	0.832	0.0	******	******	****	****
199	24	96	1.94	21.20	5.73	36.00	**	**	85	78	0.822	0.0	******	******	****	****
200	1	97	1.94	21.00	5.73	36.00	6	2	92	77	0.860	0.0	******	******	****	****
200	2	98	1.94	21.00	5.73	36.00	0	0	96	76	0.869	0.0	******	******	****	****
200	3	99	1.94	21.00	5.73	36.00	0	0	97	75	0.849	0.0	******	******	****	****
200	4	100	1.94	21.00	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
200	5	101	1.94	21.00	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
200	6	102	1.94	21.00	5.73	36.00	5	2	99	73	0.810	0.0	******	******	****	****
200	7	103	1.94	21.00	5.73	9.53	3	2	99	73	0.810	79.97	******	******	****	****
200	8	104	1.94	21.00	17.99	3.21	0	0	99	74	0.838	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
200	9	105	1.94	21.00	30.84	1.94	4	4	92	78	0.890	79.97	******	******	****	****
200	10	106	1.94	21.00	43.90	1.44	3	3	80	81	0.853	79.97	******	******	****	****
200	11	107	1.94	21.00	57.01	1.19	4	4	70	85	0.850	79.97	******	******	****	****
200	12	108	1.94	21.00	69.84	1.06	5	4	60	88	0.801	79.97	******	******	****	****
200	13	109	1.94	21.00	80.60	1.01	5	4	50	90	0.711	79.97	******	******	****	****
200	14	110	1.94	21.00	78.25	1.02	5	4	50	91	0.733	79.97	******	******	****	****
200	15	111	1.94	21.00	66.44	1.09	5	4	48	93	0.749	79.97	******	******	****	****
200	16	112	1.94	21.00	53.48	1.24	5	4	46	94	0.741	79.97	******	******	****	****
200	17	113	1.94	21.00	40.36	1.54	8	6	46	95	0.764	79.97	******	******	****	****
200	18	114	1.94	21.00	27.35	2.17	8	6	50	91	0.733	79.97	******	******	****	****
200	19	115	1.94	21.00	14.58	3.91	8	6	72	83	0.819	79.97	******	******	****	****
200	20	116	1.94	21.00	5.73	18.45	5	3	80	82	0.882	79.97	******	******	****	****
200	21	117	1.94	21.00	5.73	36.00	4	2	83	81	0.885	0.0	******	******	****	****
200	22	118	1.94	21.00	5.73	36.00	4	2	86	80	0.888	0.0	******	******	****	****
200	23	119	1.94	21.00	5.73	36.00	0	0	90	78	0.870	0.0	******	******	****	****
200	24	120	1.94	21.00	5.73	36.00	0	0	92	77	0.860	0.0	******	******	****	****
201	1	121	1.94	20.80	5.73	36.00	3	1	95	75	0.831	0.0	******	******	****	****
201	2	122	1.94	20.80	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
201	3	123	1.94	20.80	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
201	4	124	1.94	20.80	5.73	36.00	0	0	98	73	0.802	0.0	******	******	****	****
201	5	125	1.94	20.80	5.73	36.00	4	1	98	73	0.802	0.0	******	******	****	****
201	6	126	1.94	20.80	5.73	36.00	0	0	99	73	0.810	0.0	******	******	****	****
201	7	127	1.94	20.80	5.73	9.68	3	1	***	73	0.0	79.97	******	******	****	****
201	8	128	1.94	20.80	17.91	3.22	2	1	95	73	0.777	79.97	******	******	****	****
201	9	129	1.94	20.80	30.77	1.95	5	4	86	80	0.888	79.97	******	******	****	****
201	10	130	1.94	20.80	43.83	1.44	8	7	76	83	0.865	79.97	******	******	****	****
201	11	131	1.94	20.80	56.93	1.19	8	6	64	86	0.802	79.97	******	******	****	****
201	12	132	1.94	20.80	69.74	1.07	10	8	60	89	0.827	79.97	******	******	****	****
201	13	133	1.94	20.80	80.42	1.01	10	10	70	76	0.633	79.97	******	******	****	****
201	14	134	1.94	20.80	78.10	1.02	10	10	94	74	0.795	79.97	******	******	****	****
201	15	135	1.94	20.80	66.35	1.09	10	9	90	79	0.899	79.97	******	******	****	****
201	16	136	1.94	20.80	53.40	1.24	10	9	72	82	0.793	79.97	******	******	****	****
201	17	137	1.94	20.80	40.29	1.54	10	10	70	84	0.822	79.97	******	******	****	****
201	18	138	1.94	20.80	27.27	2.17	10	10	98	73	0.802	79.97	******	******	****	****
201	19	139	1.94	20.80	14.49	3.94	9	8	98	75	0.857	79.97	******	******	****	****
201	20	140	1.94	20.80	5.73	18.96	9	8	98	74	0.829	79.97	******	******	****	****
201	21	141	1.94	20.80	5.73	36.00	9	8	97	73	0.793	0.0	******	******	****	****
201	22	142	1.94	20.80	5.73	36.00	9	8	98	73	0.802	0.0	******	******	****	****
201	23	143	1.94	20.80	5.73	36.00	6	5	98	72	0.775	0.0	******	******	****	****
201	24	144	1.94	20.80	5.73	36.00	5	4	98	72	0.775	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
202	1	145	1.94	20.60	5.73	36.00	4	4	98	71	0.749	0.0	******	******	****	****
202	2	146	1.94	20.60	5.73	36.00	6	6	98	71	0.749	0.0	******	******	****	****
202	3	147	1.94	20.60	5.73	36.00	8	8	98	70	0.724	0.0	******	******	****	****
202	4	148	1.94	20.60	5.73	36.00	10	10	98	70	0.724	0.0	******	******	****	****
202	5	149	1.94	20.60	5.73	36.00	10	10	98	70	0.724	0.0	******	******	****	****
202	6	150	1.94	20.60	5.73	36.00	10	10	98	71	0.749	0.0	******	******	****	****
202	7	151	1.94	20.60	5.73	9.79	10	10	98	72	0.775	79.97	******	******	****	****
202	8	152	1.94	20.60	17.84	3.23	9	6	98	73	0.802	79.97	******	******	****	****
202	9	153	1.94	20.60	30.71	1.95	9	8	85	77	0.795	79.97	******	******	****	****
202	10	154	1.94	20.60	43.78	1.44	7	6	70	82	0.771	79.97	******	******	****	****
202	11	155	1.94	20.60	56.88	1.19	8	7	70	84	0.822	79.97	******	******	****	****
202	12	156	1.94	20.60	69.67	1.07	7	3	70	87	0.905	79.97	******	******	****	****
202	13	157	1.94	20.60	80.26	1.01	10	9	60	88	0.801	79.97	******	******	****	****
202	14	158	1.94	20.60	77.94	1.02	10	9	59	88	0.788	79.97	******	******	****	****
202	15	159	1.94	20.60	66.25	1.09	10	10	63	85	0.765	79.97	******	******	****	****
202	16	160	1.94	20.60	53.31	1.25	10	10	97	70	0.717	79.97	******	******	****	****
202	17	161	1.94	20.60	40.20	1.55	10	10	98	71	0.749	79.97	******	******	****	****
202	18	162	1.94	20.60	27.17	2.18	10	10	98	72	0.775	79.97	******	******	****	****
202	19	163	1.94	20.60	14.38	3.96	10	10	98	72	0.775	79.97	******	******	****	****
202	20	164	1.94	20.60	5.73	19.59	10	10	98	72	0.775	79.97	******	******	****	****
202	21	165	1.94	20.60	5.73	36.00	10	10	98	71	0.749	0.0	******	******	****	****
202	22	166	1.94	20.60	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
202	23	167	1.94	20.60	5.73	36.00	10	9	98	71	0.749	0.0	******	******	****	****
202	24	168	1.94	20.60	5.73	36.00	8	6	98	71	0.749	0.0	******	******	****	****
203	1	169	1.94	20.40	5.73	36.00	8	6	98	70	0.724	0.0	******	******	****	****
203	2	170	1.94	20.40	5.73	36.00	7	3	98	70	0.724	0.0	******	******	****	****
203	3	171	1.94	20.40	5.73	36.00	10	10	98	71	0.749	0.0	******	******	****	****
203	4	172	1.94	20.40	5.73	36.00	10	10	97	71	0.741	0.0	******	******	****	****
203	5	173	1.94	20.40	5.73	36.00	10	10	97	72	0.767	0.0	******	******	****	****
203	6	174	1.94	20.40	5.73	36.00	10	10	97	73	0.793	0.0	******	******	****	****
203	7	175	1.94	20.40	5.73	9.95	10	10	97	74	0.821	79.97	******	******	****	****
203	8	176	1.94	20.40	17.76	3.24	10	9	96	76	0.869	79.97	******	******	****	****
203	9	177	1.94	20.40	30.64	1.96	10	9	95	77	0.888	79.97	******	******	****	****
203	10	178	1.94	20.40	43.71	1.44	10	9	93	78	0.899	79.97	******	******	****	****
203	11	179	1.94	20.40	56.81	1.19	10	9	88	80	0.908	79.97	******	******	****	****
203	12	180	1.94	20.40	69.57	1.07	10	8	79	84	0.928	79.97	******	******	****	****
203	13	181	1.94	20.40	80.09	1.01	9	8	72	86	0.902	79.97	******	******	****	****
203	14	182	1.94	20.40	77.80	1.02	9	8	85	76	0.769	79.97	******	******	****	****
203	15	183	1.94	20.40	66.16	1.09	9	8	83	80	0.857	79.97	******	******	****	****
203	16	184	1.94	20.40	53.24	1.25	10	8	89	78	0.861	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
203	17	185	1.94	20.40	40.13	1.55	10	8	88	79	0.879	79.97	******	******	****	****
203	18	186	1.94	20.40	27.09	2.19	10	7	77	80	0.795	79.97	******	******	****	****
203	19	187	1.94	20.40	14.29	3.99	10	7	82	77	0.767	79.97	******	******	****	****
203	20	188	1.94	20.40	5.73	20.14	9	4	89	76	0.805	79.97	******	******	****	****
203	21	189	1.94	20.40	5.73	36.00	8	3	92	75	0.805	0.0	******	******	****	****
203	22	190	1.94	20.40	5.73	36.00	6	2	94	74	0.795	0.0	******	******	****	****
203	23	191	1.94	20.40	5.73	36.00	3	1	96	74	0.812	0.0	******	******	****	****
203	24	192	1.94	20.40	5.73	36.00	3	1	97	73	0.793	0.0	******	******	****	****
204	1	193	1.94	20.20	5.73	36.00	3	1	97	72	0.767	0.0	******	******	****	****
204	2	194	1.94	20.20	5.73	36.00	5	2	98	72	0.775	0.0	******	******	****	****
204	3	195	1.94	20.20	5.73	36.00	5	2	98	72	0.775	0.0	******	******	****	****
204	4	196	1.94	20.20	5.73	36.00	5	2	98	72	0.775	0.0	******	******	****	****
204	5	197	1.94	20.20	5.73	36.00	8	6	98	72	0.775	0.0	******	******	****	****
204	6	198	1.94	20.20	5.73	36.00	8	6	98	72	0.775	0.0	******	******	****	****
204	7	199	1.94	20.20	5.73	10.07	9	7	98	73	0.802	79.97	******	******	****	****
204	8	200	1.94	20.20	17.70	3.26	10	9	96	74	0.812	79.97	******	******	****	****
204	9	201	1.94	20.20	30.58	1.96	9	8	90	78	0.870	79.97	******	******	****	****
204	10	202	1.94	20.20	43.66	1.45	9	8	87	79	0.869	79.97	******	******	****	****
204	11	203	1.94	20.20	56.75	1.19	9	9	80	82	0.882	79.97	******	******	****	****
204	12	204	1.94	20.20	69.50	1.07	5	5	70	85	0.850	79.97	******	******	****	****
204	13	205	1.94	20.20	79.92	1.02	7	6	63	88	0.841	79.97	******	******	****	****
204	14	206	1.94	20.20	77.64	1.02	10	8	67	87	0.866	79.97	******	******	****	****
204	15	207	1.94	20.20	66.05	1.09	10	7	70	85	0.850	79.97	******	******	****	****
204	16	208	1.94	20.20	53.14	1.25	10	6	78	80	0.805	79.97	******	******	****	****
204	17	209	1.94	20.20	40.03	1.55	9	5	80	81	0.853	79.97	******	******	****	****
204	18	210	1.94	20.20	26.99	2.19	9	5	79	82	0.871	79.97	******	******	****	****
204	19	211	1.94	20.20	14.18	4.02	10	6	79	81	0.842	79.97	******	******	****	****
204	20	212	1.94	20.20	5.73	20.84	9	5	89	78	0.861	79.97	******	******	****	****
204	21	213	1.94	20.20	5.73	36.00	8	5	92	77	0.860	0.0	******	******	****	****
204	22	214	1.94	20.20	5.73	36.00	5	3	92	76	0.833	0.0	******	******	****	****
204	23	215	1.94	20.20	5.73	36.00	8	7	93	75	0.814	0.0	******	******	****	****
204	24	216	1.94	20.20	5.73	36.00	9	8	95	74	0.804	0.0	******	******	****	****
205	1	217	1.94	20.00	5.73	36.00	10	9	95	74	0.804	0.0	******	******	****	****
205	2	218	1.94	20.00	5.73	36.00	6	5	95	74	0.804	0.0	******	******	****	****
205	3	219	1.94	20.00	5.73	36.00	10	9	97	74	0.821	0.0	******	******	****	****
205	4	220	1.94	20.00	5.73	36.00	10	10	98	74	0.829	0.0	******	******	****	****
205	5	221	1.94	20.00	5.73	36.00	8	7	97	74	0.821	0.0	******	******	****	****
205	6	222	1.94	20.00	5.73	36.00	5	3	97	74	0.821	0.0	******	******	****	****
205	7	223	1.94	20.00	5.73	10.20	5	3	97	74	0.821	79.97	******	******	****	****
205	8	224	1.94	20.00	17.63	3.27	8	6	98	75	0.857	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
205	9	225	1.94	20.00	30.53	1.96	5	4	90	79	0.899	79.97	******	******	****	****
205	10	226	1.94	20.00	43.61	1.45	5	5	81	82	0.893	79.97	******	******	****	****
205	11	227	1.94	20.00	56.70	1.20	5	5	70	85	0.850	79.97	******	******	****	****
205	12	228	1.94	20.00	69.42	1.07	5	5	65	88	0.868	79.97	******	******	****	****
205	13	229	1.94	20.00	79.76	1.02	5	5	60	90	0.853	79.97	******	******	****	****
205	14	230	1.94	20.00	77.47	1.02	5	5	56	92	0.848	79.97	******	******	****	****
205	15	231	1.94	20.00	65.94	1.09	4	3	53	92	0.802	79.97	******	******	****	****
205	16	232	1.94	20.00	53.05	1.25	7	4	52	94	0.837	79.97	******	******	****	****
205	17	233	1.94	20.00	39.94	1.55	7	5	55	92	0.833	79.97	******	******	****	****
205	18	234	1.94	20.00	26.89	2.20	7	5	60	90	0.853	79.97	******	******	****	****
205	19	235	1.94	20.00	14.07	4.05	8	5	66	85	0.801	79.97	******	******	****	****
205	20	236	1.94	20.00	5.73	21.58	6	2	72	83	0.819	79.97	******	******	****	****
205	21	237	1.94	20.00	5.73	36.00	6	2	79	82	0.871	0.0	******	******	****	****
205	22	238	1.94	20.00	5.73	36.00	4	1	84	80	0.867	0.0	******	******	****	****
205	23	239	1.94	20.00	5.73	36.00	3	1	88	78	0.851	0.0	******	******	****	****
205	24	240	1.94	20.00	5.73	36.00	0	0	91	78	0.880	0.0	******	******	****	****
206	1	241	1.94	19.80	5.73	36.00	0	0	94	76	0.851	0.0	******	******	****	****
206	2	242	1.94	19.80	5.73	36.00	0	0	96	76	0.869	0.0	******	******	****	****
206	3	243	1.94	19.80	5.73	36.00	0	0	97	75	0.849	0.0	******	******	****	****
206	4	244	1.94	19.80	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
206	5	245	1.94	19.80	5.73	36.00	0	0	98	74	0.829	0.0	******	******	****	****
206	6	246	1.94	19.80	5.73	36.00	10	2	98	74	0.829	0.0	******	******	****	****
206	7	247	1.94	19.80	5.73	10.36	10	9	98	74	0.829	79.97	******	******	****	****
206	8	248	1.94	19.80	17.55	3.28	7	7	98	74	0.829	79.97	******	******	****	****
206	9	249	1.94	19.80	30.45	1.97	7	7	95	77	0.888	79.97	******	******	****	****
206	10	250	1.94	19.80	43.54	1.45	8	3	80	84	0.940	79.97	******	******	****	****
206	11	251	1.94	19.80	56.62	1.20	8	5	70	84	0.822	79.97	******	******	****	****
206	12	252	1.94	19.80	69.32	1.07	5	3	60	87	0.776	79.97	******	******	****	****
206	13	253	1.94	19.80	79.58	1.02	5	3	55	90	0.782	79.97	******	******	****	****
206	14	254	1.94	19.80	77.33	1.02	4	3	50	90	0.711	79.97	******	******	****	****
206	15	255	1.94	19.80	65.85	1.10	4	3	50	92	0.757	79.97	******	******	****	****
206	16	256	1.94	19.80	52.97	1.25	4	3	50	92	0.757	79.97	******	******	****	****
206	17	257	1.94	19.80	39.86	1.56	4	3	50	92	0.757	79.97	******	******	****	****
206	18	258	1.94	19.80	26.81	2.21	4	3	50	92	0.757	79.97	******	******	****	****
206	19	259	1.94	19.80	13.99	4.07	3	2	53	90	0.754	79.97	******	******	****	****
206	20	260	1.94	19.80	5.73	22.23	0	0	65	86	0.814	79.97	******	******	****	****
206	21	261	1.94	19.80	5.73	36.00	0	0	75	82	0.826	0.0	******	******	****	****
206	22	262	1.94	19.80	5.73	36.00	0	0	81	81	0.863	0.0	******	******	****	****
206	23	263	1.94	19.80	5.73	36.00	0	0	84	80	0.867	0.0	******	******	****	****
206	24	264	1.94	19.80	5.73	36.00	0	0	87	78	0.841	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
207	1	265	1.94	19.60	5.73	36.00	0	0	91	76	0.824	0.0	******	******	****	****
207	2	266	1.94	19.60	5.73	36.00	0	0	94	76	0.851	0.0	******	******	****	****
207	3	267	1.94	19.60	5.73	36.00	0	0	96	75	0.840	0.0	******	******	****	****
207	4	268	1.94	19.60	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
207	5	269	1.94	19.60	5.73	36.00	0	0	96	74	0.812	0.0	******	******	****	****
207	6	270	1.94	19.60	5.73	36.00	7	7	96	74	0.812	0.0	******	******	****	****
207	7	271	1.94	19.60	5.73	10.53	7	6	96	74	0.812	79.97	******	******	****	****
207	8	272	1.94	19.60	17.46	3.30	7	6	96	74	0.812	79.97	******	******	****	****
207	9	273	1.94	19.60	30.38	1.97	8	8	95	76	0.860	79.97	******	******	****	****
207	10	274	1.94	19.60	43.46	1.45	10	10	93	78	0.899	79.97	******	******	****	****
207	11	275	1.94	19.60	56.54	1.20	10	10	91	80	0.939	79.97	******	******	****	****
207	12	276	1.94	19.60	69.22	1.07	10	10	92	76	0.833	79.97	******	******	****	****
207	13	277	1.94	19.60	79.40	1.02	10	10	97	72	0.767	79.97	******	******	****	****
207	14	278	1.94	19.60	77.17	1.02	10	10	98	70	0.724	79.97	******	******	****	****
207	15	279	1.94	19.60	65.76	1.10	10	10	98	70	0.724	79.97	******	******	****	****
207	16	280	1.94	19.60	52.89	1.25	10	9	99	74	0.838	79.97	******	******	****	****
207	17	281	1.94	19.60	39.79	1.56	10	9	90	79	0.899	79.97	******	******	****	****
207	18	282	1.94	19.60	26.73	2.21	10	10	86	80	0.888	79.97	******	******	****	****
207	19	283	1.94	19.60	13.90	4.09	10	9	88	79	0.879	79.97	******	******	****	****
207	20	284	1.94	19.60	5.73	22.92	10	9	90	78	0.870	79.97	******	******	****	****
207	21	285	1.94	19.60	5.73	36.00	10	10	94	76	0.851	0.0	******	******	****	****
207	22	286	1.94	19.60	5.73	36.00	10	8	95	76	0.860	0.0	******	******	****	****
207	23	287	1.94	19.60	5.73	36.00	5	4	95	75	0.831	0.0	******	******	****	****
207	24	288	1.94	19.60	5.73	36.00	5	4	95	75	0.831	0.0	******	******	****	****
208	1	289	1.94	19.40	5.73	36.00	7	5	96	74	0.812	0.0	******	******	****	****
208	2	290	1.94	19.40	5.73	36.00	9	7	98	73	0.802	0.0	******	******	****	****
208	3	291	1.94	19.40	5.73	36.00	8	6	98	73	0.802	0.0	******	******	****	****
208	4	292	1.94	19.40	5.73	36.00	3	2	98	72	0.775	0.0	******	******	****	****
208	5	293	1.94	19.40	5.73	36.00	7	5	99	72	0.783	0.0	******	******	****	****
208	6	294	1.94	19.40	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
208	7	295	1.94	19.40	5.73	10.70	10	10	99	72	0.783	79.97	******	******	****	****
208	8	296	1.94	19.40	17.38	3.31	10	10	99	73	0.810	79.97	******	******	****	****
208	9	297	1.94	19.40	30.30	1.98	9	7	92	78	0.890	79.97	******	******	****	****
208	10	298	1.94	19.40	43.39	1.45	9	7	90	79	0.899	79.97	******	******	****	****
208	11	299	1.94	19.40	56.46	1.20	8	6	80	80	0.826	79.97	******	******	****	****
208	12	300	1.94	19.40	69.11	1.07	8	6	70	84	0.822	79.97	******	******	****	****
208	13	301	1.94	19.40	79.22	1.02	9	7	60	88	0.801	79.97	******	******	****	****
208	14	302	1.94	19.40	77.02	1.03	8	6	64	88	0.854	79.97	******	******	****	****
208	15	303	1.94	19.40	65.66	1.10	8	6	57	90	0.811	79.97	******	******	****	****
208	16	304	1.94	19.40	52.82	1.25	8	6	62	90	0.882	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
208	17	305	1.94	19.40	39.71	1.56	9	7	64	90	0.910	79.97	******	******	****	****
208	18	306	1.94	19.40	26.65	2.22	9	9	70	85	0.850	79.97	******	******	****	****
208	19	307	1.94	19.40	13.81	4.12	7	7	80	81	0.853	79.97	******	******	****	****
208	20	308	1.94	19.40	5.73	23.64	7	7	84	79	0.839	79.97	******	******	****	****
208	21	309	1.94	19.40	5.73	36.00	5	5	87	78	0.841	0.0	******	******	****	****
208	22	310	1.94	19.40	5.73	36.00	3	3	90	77	0.841	0.0	******	******	****	****
208	23	311	1.94	19.40	5.73	36.00	3	1	96	76	0.869	0.0	******	******	****	****
208	24	312	1.94	19.40	5.73	36.00	8	3	96	76	0.869	0.0	******	******	****	****
209	1	313	1.94	19.20	5.73	36.00	8	3	96	75	0.840	0.0	******	******	****	****
209	2	314	1.94	19.20	5.73	36.00	8	3	97	74	0.821	0.0	******	******	****	****
209	3	315	1.94	19.20	5.73	36.00	8	3	98	74	0.829	0.0	******	******	****	****
209	4	316	1.94	19.20	5.73	36.00	4	1	98	74	0.829	0.0	******	******	****	****
209	5	317	1.94	19.20	5.73	36.00	3	1	98	74	0.829	0.0	******	******	****	****
209	6	318	1.94	19.20	5.73	36.00	4	3	98	73	0.802	0.0	******	******	****	****
209	7	319	1.94	19.20	5.73	10.88	4	1	98	74	0.829	79.97	******	******	****	****
209	8	320	1.94	19.20	17.29	3.33	3	1	95	75	0.831	79.97	******	******	****	****
209	9	321	1.94	19.20	30.22	1.98	1	0	85	79	0.849	79.97	******	******	****	****
209	10	322	1.94	19.20	43.31	1.46	1	1	75	82	0.826	79.97	******	******	****	****
209	11	323	1.94	19.20	56.38	1.20	3	2	70	85	0.850	79.97	******	******	****	****
209	12	324	1.94	19.20	69.01	1.07	6	4	65	88	0.868	79.97	******	******	****	****
209	13	325	1.94	19.20	79.04	1.02	7	4	60	90	0.853	79.97	******	******	****	****
209	14	326	1.94	19.20	76.87	1.03	8	5	59	90	0.839	79.97	******	******	****	****
209	15	327	1.94	19.20	65.57	1.10	8	6	55	92	0.833	79.97	******	******	****	****
209	16	328	1.94	19.20	52.74	1.26	7	6	65	91	0.954	79.97	******	******	****	****
209	17	329	1.94	19.20	39.64	1.56	7	7	84	85	1.020	79.97	******	******	****	****
209	18	330	1.94	19.20	26.57	2.23	9	8	81	80	0.836	79.97	******	******	****	****
209	19	331	1.94	19.20	13.72	4.14	10	9	80	80	0.826	79.97	******	******	****	****
209	20	332	1.94	19.20	5.73	24.38	10	8	89	78	0.861	79.97	******	******	****	****
209	21	333	1.94	19.20	5.73	36.00	10	4	92	76	0.833	0.0	******	******	****	****
209	22	334	1.94	19.20	5.73	36.00	7	2	93	76	0.842	0.0	******	******	****	****
209	23	335	1.94	19.20	5.73	36.00	5	2	93	76	0.842	0.0	******	******	****	****
209	24	336	1.94	19.20	5.73	36.00	5	2	95	75	0.831	0.0	******	******	****	****
210	1	337	1.94	19.00	5.73	36.00	6	2	97	75	0.849	0.0	******	******	****	****
210	2	338	1.94	19.00	5.73	36.00	7	4	98	74	0.829	0.0	******	******	****	****
210	3	339	1.94	19.00	5.73	36.00	6	4	98	74	0.829	0.0	******	******	****	****
210	4	340	1.94	19.00	5.73	36.00	8	5	98	74	0.829	0.0	******	******	****	****
210	5	341	1.94	19.00	5.73	36.00	4	3	98	74	0.829	0.0	******	******	****	****
210	6	342	1.94	19.00	5.73	36.00	5	2	98	73	0.802	0.0	******	******	****	****
210	7	343	1.94	19.00	5.73	11.07	5	2	98	74	0.829	79.97	******	******	****	****
210	8	344	1.94	19.00	17.21	3.34	0	0	95	76	0.860	79.97	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
210	9	345	1.94	19.00	30.14	1.98	0	0	87	81	0.927	79.97	******	******	****	****
210	10	346	1.94	19.00	43.24	1.46	0	0	73	84	0.858	79.97	******	******	****	****
210	11	347	1.94	19.00	56.30	1.20	3	2	68	86	0.852	79.97	******	******	****	****
210	12	348	1.94	19.00	68.90	1.07	5	4	52	90	0.739	79.97	******	******	****	****
210	13	349	1.94	19.00	78.86	1.02	6	4	58	90	0.825	79.97	******	******	****	****
210	14	350	1.94	19.00	76.72	1.03	4	3	56	91	0.822	79.97	******	******	****	****
210	15	351	1.94	19.00	65.47	1.10	5	4	54	94	0.869	79.97	******	******	****	****
210	16	352	1.94	19.00	52.66	1.26	3	3	53	92	0.802	79.97	******	******	****	****
210	17	353	1.94	19.00	39.56	1.57	0	0	52	94	0.837	79.97	******	******	****	****
210	18	354	1.94	19.00	26.49	2.23	3	1	52	92	0.787	79.97	******	******	****	****
210	19	355	1.94	19.00	13.63	4.17	2	1	60	90	0.853	79.97	******	******	****	****
210	20	356	1.94	19.00	5.73	25.17	2	1	70	86	0.877	79.97	******	******	****	****
210	21	357	1.94	19.00	5.73	36.00	2	2	77	84	0.905	0.0	******	******	****	****
210	22	358	1.94	19.00	5.73	36.00	6	5	82	82	0.904	0.0	******	******	****	****
210	23	359	1.94	19.00	5.73	36.00	7	6	85	81	0.906	0.0	******	******	****	****
210	24	360	1.94	19.00	5.73	36.00	7	6	87	80	0.898	0.0	******	******	****	****
211	1	361	1.94	18.70	5.73	36.00	10	10	88	80	0.908	0.0	******	******	****	****
211	2	362	1.94	18.70	5.73	36.00	10	10	93	79	0.929	0.0	******	******	****	****
211	3	363	1.94	18.70	5.73	36.00	10	9	95	78	0.919	0.0	******	******	****	****
211	4	364	1.94	18.70	5.73	36.00	10	10	96	77	0.898	0.0	******	******	****	****
211	5	365	1.94	18.70	5.73	36.00	10	8	96	77	0.898	0.0	******	******	****	****
211	6	366	1.94	18.70	5.73	36.00	7	5	96	77	0.898	0.0	******	******	****	****
211	7	367	1.94	18.70	5.73	11.36	5	4	96	76	0.869	0.0	******	******	****	****
211	8	368	1.94	18.70	17.08	3.37	1	1	94	79	0.939	3.12	******	******	****	****
211	9	369	1.94	18.70	30.02	1.99	0	0	88	83	1.001	17.94	******	******	0.55	****
211	10	370	1.94	18.70	43.12	1.46	2	2	79	85	0.959	37.44	******	******	****	****
211	11	371	1.94	18.70	56.18	1.20	6	6	70	88	0.934	53.82	******	******	****	****
211	12	372	1.94	18.70	68.74	1.07	7	6	65	90	0.924	73.32	******	******	****	****
211	13	373	1.94	18.70	78.59	1.02	6	5	63	90	0.896	******	******	******	****	****
211	14	374	1.94	18.70	76.48	1.03	4	3	62	90	0.882	******	******	******	****	****
211	15	375	1.94	18.70	65.33	1.10	5	4	60	94	0.966	******	******	******	****	****
211	16	376	1.94	18.70	52.54	1.26	9	7	73	86	0.915	73.32	******	******	****	****
211	17	377	1.94	18.70	39.45	1.57	10	9	65	92	0.984	59.28	******	******	****	****
211	18	378	1.94	18.70	26.37	2.24	10	10	88	80	0.908	******	******	******	****	****
211	19	379	1.94	18.70	13.50	4.21	10	9	97	78	0.938	******	******	******	****	****
211	20	380	1.94	18.70	5.73	26.41	10	9	99	76	0.896	******	******	******	****	****
211	21	381	1.94	18.70	5.73	36.00	8	3	99	76	0.896	0.0	******	******	****	****
211	22	382	1.94	18.70	5.73	36.00	7	2	99	76	0.896	0.0	******	******	****	****
211	23	383	1.94	18.70	5.73	36.00	6	2	99	76	0.896	0.0	******	******	****	****
211	24	384	1.94	18.70	5.73	36.00	5	1	99	76	0.896	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
212	1	385	1.94	18.50	5.73	36.00	5	1	99	76	0.896	0.0	******	******	****	****
212	2	386	1.94	18.50	5.73	36.00	0	0	99	75	0.866	0.0	******	******	****	****
212	3	387	1.94	18.50	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
212	4	388	1.94	18.50	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
212	5	389	1.94	18.50	5.73	36.00	0	0	99	74	0.838	0.0	******	******	****	****
212	6	390	1.94	18.50	5.73	36.00	3	1	99	74	0.838	0.0	******	******	****	****
212	7	391	1.94	18.50	5.73	11.60	7	2	99	75	0.866	0.0	******	******	****	****
212	8	392	1.94	18.50	16.97	3.39	5	2	98	76	0.887	7.02	******	******	****	****
212	9	393	1.94	18.50	29.93	2.00	4	1	95	80	0.980	22.62	******	******	****	****
212	10	394	1.94	18.50	43.03	1.46	5	2	89	82	0.981	42.90	******	******	****	****
212	11	395	1.94	18.50	56.08	1.20	5	4	75	85	0.910	60.84	******	******	****	****
212	12	396	1.94	18.50	68.62	1.07	7	5	65	90	0.924	57.72	******	******	****	****
212	13	397	1.94	18.50	78.40	1.02	6	5	60	93	0.937	******	******	******	****	****
212	14	398	1.94	18.50	76.34	1.03	6	3	55	94	0.885	******	******	******	****	****
212	15	399	1.94	18.50	65.25	1.10	7	3	53	94	0.853	******	******	******	****	****
212	16	400	1.94	18.50	52.48	1.26	8	3	50	94	0.805	******	******	******	****	****
212	17	401	1.94	18.50	39.39	1.57	7	3	60	90	0.853	49.92	******	******	****	****
212	18	402	1.94	18.50	26.31	2.25	7	2	63	88	0.841	42.12	******	******	****	****
212	19	403	1.94	18.50	13.43	4.23	8	2	70	85	0.850	23.40	******	******	****	****
212	20	404	1.94	18.50	5.73	27.13	8	2	75	83	0.853	3.90	******	******	****	****
212	21	405	1.94	18.50	5.73	36.00	9	3	80	80	0.826	0.0	******	******	****	****
212	22	406	1.94	18.50	5.73	36.00	9	3	88	80	0.908	0.0	******	******	****	****
212	23	407	1.94	18.50	5.73	36.00	8	5	90	79	0.899	0.0	******	******	****	****
212	24	408	1.94	18.50	5.73	36.00	10	10	90	79	0.899	0.0	******	******	****	****
213	1	409	1.94	18.20	5.73	36.00	10	10	95	78	0.919	0.0	******	******	****	****
213	2	410	1.94	18.20	5.73	36.00	10	10	96	78	0.928	0.0	******	******	****	****
213	3	411	1.94	18.20	5.73	36.00	9	4	96	78	0.928	0.0	******	******	****	****
213	4	412	1.94	18.20	5.73	36.00	3	1	96	77	0.898	0.0	******	******	****	****
213	5	413	1.94	18.20	5.73	36.00	0	0	97	76	0.878	0.0	******	******	****	****
213	6	414	1.94	18.20	5.73	36.00	2	2	97	76	0.878	0.0	******	******	****	****
213	7	415	1.94	18.20	5.73	11.92	7	3	97	76	0.878	******	******	******	****	****
213	8	416	1.94	18.20	16.84	3.41	9	4	96	76	0.869	******	******	******	****	****
213	9	417	1.94	18.20	29.81	2.00	8	3	89	81	0.949	******	******	******	****	****
213	10	418	1.94	18.20	42.91	1.47	8	3	70	84	0.822	******	******	******	****	****
213	11	419	1.94	18.20	55.95	1.21	8	3	60	87	0.776	******	******	******	****	****
213	12	420	1.94	18.20	68.45	1.07	8	3	56	90	0.796	******	******	******	****	****
213	13	421	1.94	18.20	78.12	1.02	8	3	50	92	0.757	******	******	******	****	****
213	14	422	1.94	18.20	76.10	1.03	8	4	48	94	0.773	******	******	******	****	****
213	15	423	1.94	18.20	65.10	1.10	6	3	48	94	0.773	******	******	******	****	****
213	16	424	1.94	18.20	52.36	1.26	3	2	47	94	0.757	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
213	17	425	1.94	18.20	39.27	1.58	3	2	46	94	0.741	******	******	******	****	****
213	18	426	1.94	18.20	26.19	2.26	2	2	45	94	0.724	******	******	******	****	****
213	19	427	1.94	18.20	13.29	4.27	4	3	55	90	0.782	******	******	******	****	****
213	20	428	1.94	18.20	5.73	28.51	2	2	59	87	0.763	******	******	******	****	****
213	21	429	1.94	18.20	5.73	36.00	2	2	62	85	0.753	0.0	******	******	****	****
213	22	430	1.94	18.20	5.73	36.00	2	2	74	82	0.815	0.0	******	******	****	****
213	23	431	1.94	18.20	5.73	36.00	7	6	80	82	0.882	0.0	******	******	****	****
213	24	432	1.94	18.20	5.73	36.00	0	0	87	80	0.898	0.0	******	******	****	****
214	1	433	1.94	17.90	5.73	36.00	0	0	87	78	0.841	0.0	******	******	****	****
214	2	434	1.94	17.90	5.73	36.00	0	0	87	78	0.841	0.0	******	******	****	****
214	3	435	1.94	17.90	5.73	36.00	0	0	93	76	0.842	0.0	******	******	****	****
214	4	436	1.94	17.90	5.73	36.00	0	0	95	75	0.831	0.0	******	******	****	****
214	5	437	1.94	17.90	5.73	36.00	0	0	97	74	0.821	0.0	******	******	****	****
214	6	438	1.94	17.90	5.73	36.00	2	1	98	74	0.829	0.0	******	******	****	****
214	7	439	1.94	17.90	5.73	12.30	9	3	97	74	0.821	0.0	******	******	****	****
214	8	440	1.94	17.90	16.69	3.44	7	2	97	76	0.878	5.46	******	******	****	****
214	9	441	1.94	17.90	29.66	2.01	3	1	90	80	0.929	22.62	******	******	****	****
214	10	442	1.94	17.90	42.77	1.47	3	3	80	84	0.940	37.44	******	******	****	****
214	11	443	1.94	17.90	55.80	1.21	3	3	70	86	0.877	54.60	******	******	****	****
214	12	444	1.94	17.90	68.26	1.08	4	3	60	90	0.853	72.54	******	******	****	****
214	13	445	1.94	17.90	77.84	1.02	5	4	57	92	0.863	******	******	******	****	****
214	14	446	1.94	17.90	75.88	1.03	4	3	55	92	0.833	******	******	******	****	****
214	15	447	1.94	17.90	64.97	1.10	5	4	55	92	0.833	******	******	******	****	****
214	16	448	1.94	17.90	52.26	1.26	5	4	58	92	0.878	81.12	******	******	****	****
214	17	449	1.94	17.90	39.18	1.58	5	4	70	86	0.877	45.24	******	******	****	****
214	18	450	1.94	17.90	26.09	2.26	4	3	72	84	0.846	43.68	******	******	****	****
214	19	451	1.94	17.90	13.18	4.31	3	2	73	85	0.886	25.74	******	******	****	****
214	20	452	1.94	17.90	5.73	29.76	2	2	79	83	0.899	3.12	******	******	****	****
214	21	453	1.94	17.90	5.73	36.00	1	1	86	82	0.948	0.0	******	******	****	****
214	22	454	1.94	17.90	5.73	36.00	1	1	86	81	0.917	0.0	******	******	****	****
214	23	455	1.94	17.90	5.73	36.00	1	1	89	80	0.918	0.0	******	******	****	****
214	24	456	1.94	17.90	5.73	36.00	0	0	90	79	0.899	0.0	******	******	****	****
215	1	457	1.94	17.70	5.73	36.00	0	0	95	78	0.919	0.0	******	******	****	****
215	2	458	1.94	17.70	5.73	36.00	0	0	97	77	0.907	0.0	******	******	****	****
215	3	459	1.94	17.70	5.73	36.00	0	0	97	76	0.878	0.0	******	******	****	****
215	4	460	1.94	17.70	5.73	36.00	0	0	98	76	0.887	0.0	******	******	****	****
215	5	461	1.94	17.70	5.73	36.00	0	0	98	75	0.857	0.0	******	******	****	****
215	6	462	1.94	17.70	5.73	36.00	0	0	99	75	0.866	0.0	******	******	****	****
215	7	463	1.94	17.70	5.73	12.59	0	0	99	75	0.866	0.0	******	******	****	****
215	8	464	1.94	17.70	16.58	3.46	2	1	99	75	0.866	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
215	9	465	1.94	17.70	29.56	2.02	4	3	93	80	0.960	******	******	******	****	****
215	10	466	1.94	17.70	42.67	1.47	6	4	80	82	0.882	******	******	******	****	****
215	11	467	1.94	17.70	55.69	1.21	5	4	70	86	0.877	52.26	******	******	****	****
215	12	468	1.94	17.70	68.13	1.08	5	5	60	89	0.827	70.98	******	******	****	****
215	13	469	1.94	17.70	77.64	1.02	5	5	55	92	0.833	******	******	******	****	****
215	14	470	1.94	17.70	75.73	1.03	5	5	51	94	0.821	******	******	******	****	****
215	15	471	1.94	17.70	64.88	1.10	5	4	49	95	0.814	******	******	******	****	****
215	16	472	1.94	17.70	52.20	1.26	5	4	47	96	0.805	70.98	******	******	****	****
215	17	473	1.94	17.70	39.12	1.58	4	3	50	96	0.856	******	******	******	****	****
215	18	474	1.94	17.70	26.03	2.27	4	3	48	96	0.822	******	******	******	****	****
215	19	475	1.94	17.70	13.11	4.33	5	4	50	93	0.780	******	******	******	****	****
215	20	476	1.94	17.70	5.73	30.57	4	3	66	85	0.801	******	******	******	****	****
215	21	477	1.94	17.70	5.73	36.00	3	2	63	82	0.694	0.0	******	******	****	****
215	22	478	1.94	17.70	5.73	36.00	3	2	75	81	0.799	0.0	******	******	****	****
215	23	479	1.94	17.70	5.73	36.00	0	0	88	80	0.908	0.0	******	******	****	****
215	24	480	1.94	17.70	5.73	36.00	0	0	90	79	0.899	0.0	******	******	****	****
216	1	481	1.94	17.40	5.73	36.00	0	0	90	79	0.899	0.0	******	******	****	****
216	2	482	1.94	17.40	5.73	36.00	0	0	93	78	0.899	0.0	******	******	****	****
216	3	483	1.94	17.40	5.73	36.00	0	0	96	76	0.869	0.0	******	******	****	****
216	4	484	1.94	17.40	5.73	36.00	0	0	97	76	0.878	0.0	******	******	****	****
216	5	485	1.94	17.40	5.73	36.00	0	0	98	75	0.857	0.0	******	******	****	****
216	6	486	1.94	17.40	5.73	36.00	6	2	98	74	0.829	0.0	******	******	****	****
216	7	487	1.94	17.40	5.73	12.96	8	3	98	74	0.829	0.0	******	******	****	****
216	8	488	1.94	17.40	16.45	3.49	9	2	98	76	0.887	1.56	******	******	****	****
216	9	489	1.94	17.40	29.44	2.03	9	2	90	80	0.929	9.36	******	******	****	****
216	10	490	1.94	17.40	42.55	1.48	9	2	80	83	0.910	******	******	******	****	****
216	11	491	1.94	17.40	55.56	1.21	5	2	63	87	0.815	******	******	******	****	****
216	12	492	1.94	17.40	67.96	1.08	5	2	60	90	0.853	56.94	******	******	****	****
216	13	493	1.94	17.40	77.37	1.02	3	1	56	92	0.848	60.06	******	******	****	****
216	14	494	1.94	17.40	75.49	1.03	3	1	51	94	0.821	******	******	******	****	****
216	15	495	1.94	17.40	64.73	1.10	3	1	49	96	0.839	******	******	******	****	****
216	16	496	1.94	17.40	52.07	1.27	3	1	49	96	0.839	******	******	******	****	****
216	17	497	1.94	17.40	39.00	1.59	7	3	49	96	0.839	35.88	******	******	****	****
216	18	498	1.94	17.40	25.91	2.28	8	3	49	94	0.789	******	******	******	****	****
216	19	499	1.94	17.40	12.98	4.37	9	3	56	90	0.796	******	******	******	****	****
216	20	500	1.94	17.40	5.73	32.15	9	2	63	85	0.765	******	******	******	****	****
216	21	501	1.94	17.40	5.73	36.00	5	2	70	82	0.771	0.0	******	******	****	****
216	22	502	1.94	17.40	5.73	36.00	4	1	79	81	0.842	0.0	******	******	****	****
216	23	503	1.94	17.40	5.73	36.00	3	1	84	80	0.867	0.0	******	******	****	****
216	24	504	1.94	17.40	5.73	36.00	3	1	86	80	0.888	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
217	1	505	1.94	17.20	5.73	36.00	6	4	87	80	0.898	0.0	******	******	****	****
217	2	506	1.94	17.20	5.73	36.00	6	4	87	80	0.898	0.0	******	******	****	****
217	3	507	1.94	17.20	5.73	36.00	6	4	91	79	0.909	0.0	******	******	****	****
217	4	508	1.94	17.20	5.73	36.00	6	4	92	79	0.919	0.0	******	******	****	****
217	5	509	1.94	17.20	5.73	36.00	6	4	94	78	0.909	0.0	******	******	****	****
217	6	510	1.94	17.20	5.73	36.00	5	2	95	78	0.919	0.0	******	******	****	****
217	7	511	1.94	17.20	5.73	13.28	4	2	96	78	0.928	******	******	******	****	****
217	8	512	1.94	17.20	16.34	3.51	4	1	96	80	0.991	******	******	******	****	****
217	9	513	1.94	17.20	29.33	2.03	7	3	90	84	1.057	******	******	******	****	****
217	10	514	1.94	17.20	42.45	1.48	5	4	74	86	0.927	******	******	******	****	****
217	11	515	1.94	17.20	55.45	1.21	5	4	66	88	0.881	******	******	******	****	****
217	12	516	1.94	17.20	67.82	1.08	5	4	60	92	0.908	******	******	******	****	****
217	13	517	1.94	17.20	77.17	1.02	5	4	58	92	0.878	******	******	******	****	****
217	14	518	1.94	17.20	75.34	1.03	8	6	54	94	0.869	******	******	******	****	****
217	15	519	1.94	17.20	64.64	1.11	10	7	60	95	0.997	******	******	******	****	****
217	16	520	1.94	17.20	52.01	1.27	10	8	70	90	0.995	******	******	******	****	****
217	17	521	1.94	17.20	38.94	1.59	10	10	80	84	0.940	******	******	******	****	****
217	18	522	1.94	17.20	25.85	2.28	10	10	91	80	0.939	******	******	******	****	****
217	19	523	1.94	17.20	12.91	4.39	10	10	95	78	0.919	******	******	******	****	****
217	20	524	1.94	17.20	5.73	33.01	10	10	96	80	0.991	******	******	******	****	****
217	21	525	1.94	17.20	5.73	36.00	9	8	95	77	0.888	0.0	******	******	****	****
217	22	526	1.94	17.20	5.73	36.00	9	7	94	78	0.909	0.0	******	******	****	****
217	23	527	1.94	17.20	5.73	36.00	10	10	94	78	0.909	0.0	******	******	****	****
217	24	528	1.94	17.20	5.73	36.00	10	10	96	77	0.898	0.0	******	******	****	****
218	1	529	1.95	16.90	5.73	36.00	10	10	98	76	0.887	0.0	******	******	****	****
218	2	530	1.95	16.90	5.73	36.00	10	8	98	76	0.887	0.0	******	******	****	****
218	3	531	1.95	16.90	5.73	36.00	10	9	99	75	0.866	0.0	******	******	****	****
218	4	532	1.95	16.90	5.73	36.00	10	9	99	74	0.838	0.0	******	******	****	****
218	5	533	1.95	16.90	5.73	36.00	8	6	99	74	0.838	0.0	******	******	****	****
218	6	534	1.95	16.90	5.73	36.00	7	2	99	74	0.838	0.0	******	******	****	****
218	7	535	1.95	16.90	5.73	13.75	6	2	99	74	0.838	******	******	******	****	****
218	8	536	1.95	16.90	16.19	3.54	6	3	98	76	0.887	******	******	******	****	****
218	9	537	1.95	16.90	29.19	2.04	6	3	91	80	0.939	******	******	******	****	****
218	10	538	1.95	16.90	42.30	1.48	8	3	80	83	0.910	******	******	******	****	****
218	11	539	1.95	16.90	55.29	1.22	8	7	64	87	0.828	******	******	******	****	****
218	12	540	1.95	16.90	67.62	1.08	10	9	58	88	0.774	******	******	******	****	****
218	13	541	1.95	16.90	76.89	1.03	9	8	55	90	0.782	******	******	******	****	****
218	14	542	1.95	16.90	75.10	1.03	9	8	55	90	0.782	******	******	******	****	****
218	15	543	1.95	16.90	64.50	1.11	10	8	53	92	0.802	******	******	******	****	****
218	16	544	1.95	16.90	51.90	1.27	10	8	54	91	0.792	******	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
218	17	545	1.95	16.90	38.84	1.59	9	4	55	91	0.807	41.73	******	******	****	****
218	18	546	1.95	16.90	25.74	2.29	8	3	56	90	0.796	25.35	******	******	****	****
218	19	547	1.95	16.90	12.80	4.43	8	3	60	90	0.853	14.43	******	******	****	****
218	20	548	1.95	16.90	5.73	34.46	7	2	65	86	0.814	******	******	******	****	****
218	21	549	1.95	16.90	5.73	36.00	6	2	73	83	0.831	0.0	******	******	****	****
218	22	550	1.95	16.90	5.73	36.00	6	2	73	81	0.778	0.0	******	******	****	****
218	23	551	1.95	16.90	5.73	36.00	5	2	74	80	0.764	0.0	******	******	****	****
218	24	552	1.95	16.90	5.73	36.00	10	7	79	79	0.789	0.0	******	******	****	****
219	1	553	1.95	16.70	5.73	36.00	10	7	85	78	0.822	0.0	******	******	****	****
219	2	554	1.95	16.70	5.73	36.00	10	6	85	77	0.795	0.0	******	******	****	****
219	3	555	1.95	16.70	5.73	36.00	10	7	87	77	0.813	0.0	******	******	****	****
219	4	556	1.95	16.70	5.73	36.00	10	6	90	76	0.814	0.0	******	******	****	****
219	5	557	1.95	16.70	5.73	36.00	10	7	93	76	0.842	0.0	******	******	****	****
219	6	558	1.95	16.70	5.73	36.00	8	3	94	75	0.822	0.0	******	******	****	****
219	7	559	1.95	16.70	5.73	14.10	9	3	95	75	0.831	1.56	******	******	****	****
219	8	560	1.95	16.70	16.08	3.57	7	3	95	76	0.860	10.14	******	******	****	****
219	9	561	1.95	16.70	29.09	2.05	7	3	85	79	0.849	******	******	******	****	****
219	10	562	1.95	16.70	42.20	1.49	6	3	76	82	0.838	******	******	******	****	****
219	11	563	1.95	16.70	55.18	1.22	7	5	73	88	0.975	63.96	******	******	****	****
219	12	564	1.95	16.70	67.49	1.08	6	4	65	90	0.924	******	******	******	****	****
219	13	565	1.95	16.70	76.69	1.03	5	4	58	92	0.878	******	******	******	****	****
219	14	566	1.95	16.70	74.95	1.03	6	4	54	93	0.843	******	******	******	****	****
219	15	567	1.95	16.70	64.41	1.11	8	7	58	91	0.851	23.40	******	******	****	****
219	16	568	1.95	16.70	51.83	1.27	10	9	89	80	0.918	10.92	******	******	****	****
219	17	569	1.95	16.70	38.78	1.59	10	10	93	77	0.870	6.24	******	******	****	****
219	18	570	1.95	16.70	25.68	2.30	10	8	93	76	0.842	8.58	******	******	****	****
219	19	571	1.95	16.70	12.73	4.45	10	10	87	80	0.898	10.14	******	******	****	****
219	20	572	1.95	16.70	5.73	35.37	10	8	84	80	0.867	1.56	******	******	****	****
219	21	573	1.95	16.70	5.73	36.00	10	10	89	79	0.889	0.0	******	******	****	****
219	22	574	1.95	16.70	5.73	36.00	10	10	93	78	0.899	0.0	******	******	****	****
219	23	575	1.95	16.70	5.73	36.00	10	10	94	78	0.909	0.0	******	******	****	****
219	24	576	1.95	16.70	5.73	36.00	9	8	94	78	0.909	0.0	******	******	****	****
220	1	577	1.95	16.40	5.73	36.00	8	6	96	76	0.869	0.0	******	******	****	****
220	2	578	1.95	16.40	5.73	36.00	7	6	96	76	0.869	0.0	******	******	****	****
220	3	579	1.95	16.40	5.73	36.00	5	4	96	75	0.840	0.0	******	******	****	****
220	4	580	1.95	16.40	5.73	36.00	5	4	97	74	0.821	0.0	******	******	****	****
220	5	581	1.95	16.40	5.73	36.00	4	3	97	74	0.821	0.0	******	******	****	****
220	6	582	1.95	16.40	5.73	36.00	4	3	98	74	0.829	0.0	******	******	****	****
220	7	583	1.95	16.40	5.73	14.69	7	3	98	74	0.829	0.78	******	******	****	****
220	8	584	1.95	16.40	15.90	3.60	8	3	98	74	0.829	9.36	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
220	9	585	1.95	16.40	28.92	2.06	8	3	93	79	0.929	28.08	******	******	****	****
220	10	586	1.95	16.40	42.03	1.49	10	6	83	83	0.945	46.80	******	******	****	****
220	11	587	1.95	16.40	55.00	1.22	10	7	73	85	0.886	46.80	******	******	****	****
220	12	588	1.95	16.40	67.27	1.08	9	8	65	89	0.896	63.18	******	******	****	****
220	13	589	1.95	16.40	76.40	1.03	10	10	57	91	0.836	66.30	******	******	****	****
220	14	590	1.95	16.40	74.72	1.04	10	10	73	84	0.858	24.18	******	******	****	****
220	15	591	1.95	16.40	64.29	1.11	10	10	76	85	0.923	23.40	******	******	****	****
220	16	592	1.95	16.40	51.74	1.27	10	10	76	85	0.923	20.28	******	******	****	****
220	17	593	1.95	16.40	38.70	1.60	10	10	76	85	0.923	35.10	******	******	****	****
220	18	594	1.95	16.40	25.60	2.30	10	10	81	82	0.893	14.82	******	******	****	****
220	19	595	1.95	16.40	12.63	4.48	10	10	84	80	0.867	3.90	******	******	****	****
220	20	596	1.95	16.40	5.73	36.37	10	10	87	78	0.841	0.78	******	******	****	****
220	21	597	1.95	16.40	5.73	36.00	10	10	97	76	0.878	0.0	******	******	****	****
220	22	598	1.95	16.40	5.73	36.00	10	10	99	76	0.896	0.0	******	******	****	****
220	23	599	1.95	16.40	5.73	36.00	10	10	99	76	0.896	0.0	******	******	****	****
220	24	600	1.95	16.40	5.73	36.00	10	10	99	75	0.866	0.0	******	******	****	****
221	1	601	1.95	16.10	5.73	36.00	10	9	98	75	0.857	0.0	******	******	****	****
221	2	602	1.95	16.10	5.73	36.00	10	9	98	74	0.829	0.0	******	******	****	****
221	3	603	1.95	16.10	5.73	36.00	10	9	98	74	0.829	0.0	******	******	****	****
221	4	604	1.95	16.10	5.73	36.00	10	10	98	74	0.829	0.0	******	******	****	****
221	5	605	1.95	16.10	5.73	36.00	8	7	98	74	0.829	0.0	******	******	****	****
221	6	606	1.95	16.10	5.73	36.00	9	8	98	74	0.829	0.0	******	******	****	****
221	7	607	1.95	16.10	5.73	15.26	10	7	98	74	0.829	0.78	******	******	****	****
221	8	608	1.95	16.10	15.75	3.64	10	8	98	74	0.829	8.58	******	******	****	****
221	9	609	1.95	16.10	28.77	2.07	10	10	97	79	0.969	21.84	******	******	****	****
221	10	610	1.95	16.10	41.88	1.50	10	10	90	80	0.929	24.18	******	******	****	****
221	11	611	1.95	16.10	54.84	1.22	10	10	83	80	0.857	23.40	******	******	****	****
221	12	612	1.95	16.10	67.07	1.09	9	9	80	82	0.882	46.80	******	******	****	****
221	13	613	1.95	16.10	76.11	1.03	9	9	72	84	0.846	56.94	******	******	****	****
221	14	614	1.95	16.10	74.48	1.04	10	10	70	84	0.822	42.90	******	******	****	****
221	15	615	1.95	16.10	64.14	1.11	10	10	97	78	0.938	12.48	******	******	****	****
221	16	616	1.95	16.10	51.63	1.27	10	10	99	77	0.926	10.92	******	******	****	****
221	17	617	1.95	16.10	38.60	1.60	10	10	98	78	0.948	9.36	******	******	****	****
221	18	618	1.95	16.10	25.49	2.31	10	10	97	78	0.938	7.02	******	******	****	****
221	19	619	1.95	16.10	12.52	4.52	10	10	96	78	0.928	6.24	******	******	****	****
221	20	620	1.95	16.10	5.73	34.88	10	9	99	73	0.810	0.78	******	******	****	****
221	21	621	1.95	16.10	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
221	22	622	1.95	16.10	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
221	23	623	1.95	16.10	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
221	24	624	1.95	16.10	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
222	1	625	1.95	15.80	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****
222	2	626	1.95	15.80	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****
222	3	627	1.95	15.80	5.73	36.00	9	9	99	72	0.783	0.0	******	******	****	****
222	4	628	1.95	15.80	5.73	36.00	10	10	99	72	0.783	0.0	******	******	****	****
222	5	629	1.95	15.80	5.73	36.00	10	10	99	73	0.810	0.0	******	******	****	****
222	6	630	1.95	15.80	5.73	36.00	10	10	99	74	0.838	0.0	******	******	****	****
222	7	631	1.95	15.80	5.73	15.87	10	10	99	74	0.838	0.78	******	******	****	****
222	8	632	1.95	15.80	15.59	3.67	10	10	99	74	0.838	4.68	******	******	****	****
222	9	633	1.95	15.80	28.62	2.08	10	10	96	74	0.812	5.46	******	******	****	****
222	10	634	1.95	15.80	41.73	1.50	10	10	96	72	0.759	9.36	******	******	****	****
222	11	635	1.95	15.80	54.68	1.22	10	10	98	72	0.775	12.48	******	******	****	****
222	12	636	1.95	15.80	66.86	1.09	10	9	90	72	0.712	24.96	******	******	****	****
222	13	637	1.95	15.80	75.82	1.03	10	9	73	78	0.706	45.24	******	******	****	****
222	14	638	1.95	15.80	74.24	1.04	10	10	77	78	0.745	37.44	******	******	****	****
222	15	639	1.95	15.80	63.99	1.11	10	9	80	77	0.748	12.48	******	******	****	****
222	16	640	1.95	15.80	51.52	1.28	10	10	95	76	0.860	9.36	******	******	****	****
222	17	641	1.95	15.80	38.50	1.60	10	10	92	75	0.805	21.84	******	******	****	****
222	18	642	1.95	15.80	25.39	2.32	10	10	93	75	0.814	9.36	******	******	****	****
222	19	643	1.95	15.80	12.41	4.56	10	10	95	75	0.831	5.46	******	******	****	****
222	20	644	1.95	15.80	5.73	33.42	10	10	95	75	0.831	0.78	******	******	****	****
222	21	645	1.95	15.80	5.73	36.00	10	10	96	75	0.840	0.0	******	******	****	****
222	22	646	1.95	15.80	5.73	36.00	10	9	92	73	0.753	0.0	******	******	****	****
222	23	647	1.95	15.80	5.73	36.00	10	10	94	72	0.744	0.0	******	******	****	****
222	24	648	1.95	15.80	5.73	36.00	10	10	96	73	0.785	0.0	******	******	****	****
223	1	649	1.95	15.50	5.73	36.00	10	10	97	73	0.793	0.0	******	******	****	****
223	2	650	1.95	15.50	5.73	36.00	10	10	97	74	0.821	0.0	******	******	****	****
223	3	651	1.95	15.50	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
223	4	652	1.95	15.50	5.73	36.00	10	10	98	71	0.749	0.0	******	******	****	****
223	5	653	1.95	15.50	5.73	36.00	10	10	98	72	0.775	0.0	******	******	****	****
223	6	654	1.95	15.50	5.73	36.00	10	10	98	73	0.802	0.0	******	******	****	****
223	7	655	1.95	15.50	5.73	16.61	10	10	98	72	0.775	0.78	******	******	****	****
223	8	656	1.95	15.50	15.41	3.71	10	10	98	72	0.775	1.56	******	******	****	****
223	9	657	1.95	15.50	28.45	2.09	10	10	98	73	0.802	3.90	******	******	****	****
223	10	658	1.95	15.50	41.56	1.50	10	10	98	74	0.829	8.58	******	******	****	****
223	11	659	1.95	15.50	54.49	1.23	10	10	92	74	0.778	21.84	******	******	****	****
223	12	660	1.95	15.50	66.64	1.09	10	10	86	74	0.728	33.54	******	******	****	****
223	13	661	1.95	15.50	75.52	1.03	9	8	80	76	0.724	46.80	******	******	****	****
223	14	662	1.95	15.50	74.01	1.04	10	9	80	80	0.826	46.02	******	******	****	****
223	15	663	1.95	15.50	63.86	1.11	10	9	80	78	0.774	24.96	******	******	****	****
223	16	664	1.95	15.50	51.42	1.28	10	10	72	78	0.696	24.18	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
223	17	665	1.95	15.50	38.42	1.61	10	10	88	77	0.823	13.26	******	******	****	****
223	18	666	1.95	15.50	25.31	2.33	10	10	92	76	0.833	8.58	******	******	****	****
223	19	667	1.95	15.50	12.31	4.59	10	10	94	76	0.851	3.90	******	******	****	****
223	20	668	1.95	15.50	5.73	32.24	10	10	92	76	0.833	0.78	******	******	****	****
223	21	669	1.95	15.50	5.73	36.00	10	10	92	76	0.833	0.0	******	******	****	****
223	22	670	1.95	15.50	5.73	36.00	10	10	92	76	0.833	0.0	******	******	****	****
223	23	671	1.95	15.50	5.73	36.00	10	10	95	75	0.831	0.0	******	******	****	****
223	24	672	1.95	15.50	5.73	36.00	10	10	96	75	0.840	0.0	******	******	****	****
224	1	673	1.95	15.20	5.73	36.00	10	10	96	75	0.840	0.0	******	******	****	****
224	2	674	1.95	15.20	5.73	36.00	10	10	96	75	0.840	0.0	******	******	****	****
224	3	675	1.95	15.20	5.73	36.00	10	10	97	75	0.849	0.0	******	******	****	****
224	4	676	1.95	15.20	5.73	36.00	10	10	97	75	0.849	0.0	******	******	****	****
224	5	677	1.95	15.20	5.73	36.00	10	10	97	75	0.849	0.0	******	******	****	****
224	6	678	1.95	15.20	5.73	36.00	10	8	97	75	0.849	0.0	******	******	****	****
224	7	679	1.95	15.20	5.73	17.30	10	9	97	75	0.849	0.78	******	******	****	****
224	8	680	1.95	15.20	15.26	3.75	10	10	97	74	0.821	7.80	******	******	****	****
224	9	681	1.95	15.20	28.31	2.10	10	10	98	74	0.829	1.56	******	******	****	****
224	10	682	1.95	15.20	41.41	1.51	10	10	98	74	0.829	6.24	******	******	****	****
224	11	683	1.95	15.20	54.33	1.23	10	10	98	72	0.775	3.90	******	******	****	****
224	12	684	1.95	15.20	66.43	1.09	10	10	98	73	0.802	7.02	******	******	****	****
224	13	685	1.95	15.20	75.23	1.03	10	10	98	76	0.887	16.38	******	******	****	****
224	14	686	1.95	15.20	73.76	1.04	10	10	98	76	0.887	35.10	******	******	****	****
224	15	687	1.95	15.20	63.70	1.11	10	10	95	77	0.888	29.64	******	******	****	****
224	16	688	1.95	15.20	51.30	1.28	10	10	94	78	0.909	19.50	******	******	****	****
224	17	689	1.95	15.20	38.31	1.61	10	10	94	79	0.939	19.50	******	******	****	****
224	18	690	1.95	15.20	25.20	2.34	10	10	94	79	0.939	16.38	******	******	****	****
224	19	691	1.95	15.20	12.20	4.63	10	10	93	78	0.899	6.24	******	******	****	****
224	20	692	1.95	15.20	5.73	30.84	10	10	93	77	0.870	1.56	******	******	****	****
224	21	693	1.95	15.20	5.73	36.00	10	9	95	77	0.888	0.0	******	******	****	****
224	22	694	1.95	15.20	5.73	36.00	10	8	96	76	0.869	0.0	******	******	****	****
224	23	695	1.95	15.20	5.73	36.00	10	6	97	76	0.878	0.0	******	******	****	****
224	24	696	1.95	15.20	5.73	36.00	10	10	98	76	0.887	0.0	******	******	****	****
225	1	697	1.95	14.90	5.73	36.00	10	10	97	75	0.849	0.0	******	******	****	****
225	2	698	1.95	14.90	5.73	36.00	10	10	97	74	0.821	0.0	******	******	****	****
225	3	699	1.95	14.90	5.73	36.00	10	10	98	74	0.829	0.0	******	******	****	****
225	4	700	1.95	14.90	5.73	36.00	10	10	98	75	0.857	0.0	******	******	****	****
225	5	701	1.95	14.90	5.73	36.00	10	10	98	75	0.857	0.0	******	******	****	****
225	6	702	1.95	14.90	5.73	36.00	10	10	98	74	0.829	0.0	******	******	****	****
225	7	703	1.95	14.90	5.73	18.07	10	10	97	74	0.821	0.0	******	******	****	****
225	8	704	1.95	14.90	15.11	3.78	10	9	98	75	0.857	5.46	******	******	****	****

DAY	HR	SEQN	SOLC	DECLN	HRANG	AIRMS	CL *	OP *	RHM *	TEM *	VPRES	SWRADT *	TLRADT *	LWRADT	TRAN	EMSV
			LY/M	DEG	DEG					F	IN-HG	LY/HR	LY/HR	LY/HR		
225	9	705	1.95	14.90	28.16	2.11	10	10	96	75	0.840	10.92	******	******	****	****
225	10	706	1.95	14.90	41.26	1.51	10	10	97	74	0.821	5.46	******	******	****	****
225	11	707	1.95	14.90	54.16	1.23	10	10	96	75	0.840	7.02	******	******	****	****
225	12	708	1.95	14.90	66.22	1.09	10	10	96	76	0.869	21.06	******	******	****	****
225	13	709	1.95	14.90	74.94	1.03	10	10	97	74	0.821	8.58	******	******	****	****
225	14	710	1.95	14.90	73.52	1.04	10	10	97	74	0.821	8.58	******	******	****	****
225	15	711	1.95	14.90	63.55	1.12	10	10	97	75	0.849	11.70	******	******	****	****
225	16	712	1.95	14.90	51.19	1.28	10	8	97	77	0.907	20.28	******	******	****	****
225	17	713	1.95	14.90	38.20	1.61	10	9	93	78	0.899	22.62	******	******	****	****
225	18	714	1.95	14.90	25.09	2.35	10	9	94	78	0.909	9.36	******	******	****	****
225	19	715	1.95	14.90	12.08	4.67	10	9	94	77	0.879	6.24	******	******	****	****
225	20	716	1.95	14.90	5.73	29.54	10	9	95	76	0.860	0.78	******	******	****	****
225	21	717	1.95	14.90	5.73	36.00	9	8	95	76	0.860	0.0	******	******	****	****
225	22	718	1.95	14.90	5.73	36.00	8	6	96	76	0.869	0.0	******	******	****	****
225	23	719	1.95	14.90	5.73	36.00	4	3	96	75	0.840	0.0	******	******	****	****
225	24	720	1.95	14.90	5.73	36.00	3	2	97	74	0.821	0.0	******	******	****	****